

# Si<sub>34</sub> Clathrate Structure: A\_cF136\_227\_aeg-001

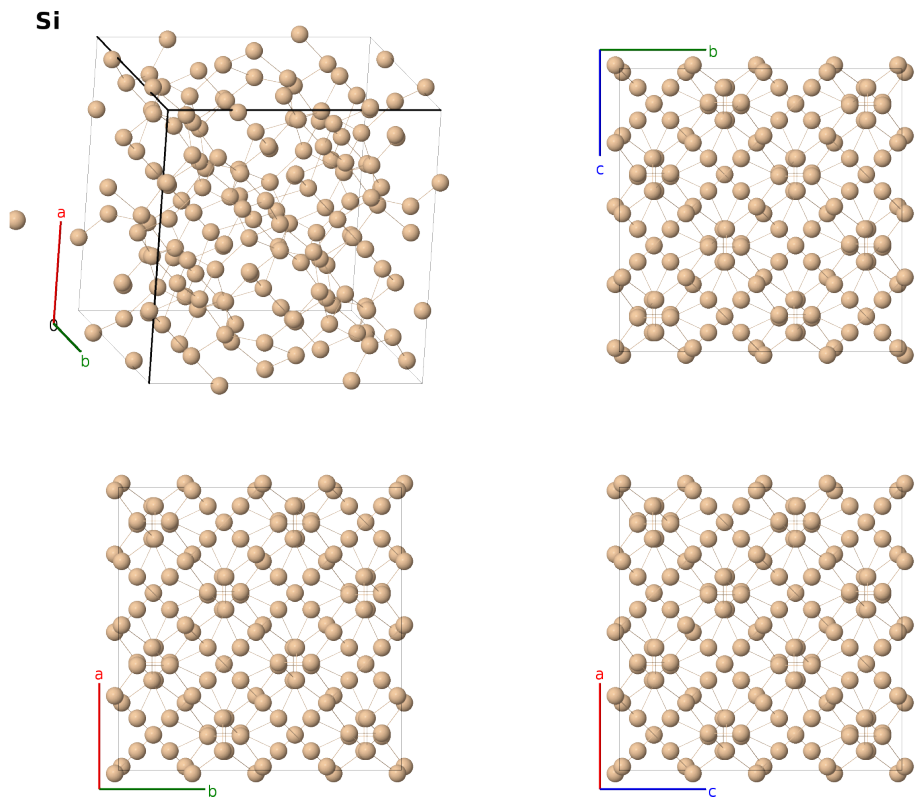
This structure previously used the label(s) **A\_cF136\_227\_aeg**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/U115>

[https://aflow.org/prototype-encyclopedia/A\\_cF136\\_227\\_aeg-001](https://aflow.org/prototype-encyclopedia/A_cF136_227_aeg-001)



|                         |                                                                                                                        |
|-------------------------|------------------------------------------------------------------------------------------------------------------------|
| Prototype               | Si                                                                                                                     |
| AFLOW prototype label   | A_cF136_227_aeg-001                                                                                                    |
| Pearson symbol          | cF136                                                                                                                  |
| Space group number      | 227                                                                                                                    |
| Space group symbol      | $Fd\bar{3}m$                                                                                                           |
| AFLOW prototype command | <code>aflow --proto=A_cF136_227_aeg-001</code><br><code>--params=a, x<sub>2</sub>, x<sub>3</sub>, z<sub>3</sub></code> |

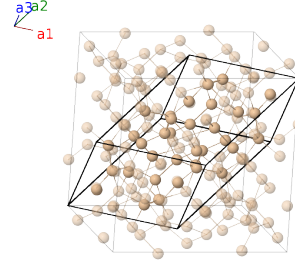
Other compounds with this structure  
Ge (high pressure)

- Silicon clathrates are open structures of pentagonal dodecahedra connected so that all of the silicon atoms have sp<sup>3</sup> bonding. In nature these structures are stabilized by alkali impurity atoms.
- This structure and the Si<sub>46</sub> structure are proposed “pure” silicon clathrate structures.
- For more information about these structures and their possible stability, see (Adams, 1994).
- See (Gryko, 2000) for a possible experimental realization of this structure (Si<sub>34</sub>Na<sub>x</sub>, where x is very small).
- We have used the fact that all vectors of the form  $(0, \pm a/2, \pm a/2)$ ,  $(\pm a/2, 0, \pm a/2)$ , and  $(\pm a/2, \pm a/2, 0)$  are primitive vectors of the face-centered cubic lattice to simplify the positions of some atoms in both lattice and Cartesian coordinates.
- (Dong, 1999) study a similar, but not identical structure (ICSD 56271), and (Schwarz, 2008) find a similar high-pressure phase of germanium (ICSD 245948).

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### Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}}\end{aligned}$$




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### Basis vectors

|                   | Lattice<br>coordinates                                                                      |     | Cartesian<br>coordinates                                                                                 | Wyckoff<br>position | Atom<br>type |
|-------------------|---------------------------------------------------------------------------------------------|-----|----------------------------------------------------------------------------------------------------------|---------------------|--------------|
| $\mathbf{B}_1$    | $= \frac{1}{8} \mathbf{a}_1 + \frac{1}{8} \mathbf{a}_2 + \frac{1}{8} \mathbf{a}_3$          | $=$ | $\frac{1}{8}a \hat{\mathbf{x}} + \frac{1}{8}a \hat{\mathbf{y}} + \frac{1}{8}a \hat{\mathbf{z}}$          | (8a)                | Si I         |
| $\mathbf{B}_2$    | $= \frac{7}{8} \mathbf{a}_1 + \frac{7}{8} \mathbf{a}_2 + \frac{7}{8} \mathbf{a}_3$          | $=$ | $\frac{7}{8}a \hat{\mathbf{x}} + \frac{7}{8}a \hat{\mathbf{y}} + \frac{7}{8}a \hat{\mathbf{z}}$          | (8a)                | Si I         |
| $\mathbf{B}_3$    | $= x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$                                  | $=$ | $ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$                                  | (32e)               | Si II        |
| $\mathbf{B}_4$    | $= x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - (3x_2 - \frac{1}{2}) \mathbf{a}_3$                 | $=$ | $-a(x_2 - \frac{1}{4}) \hat{\mathbf{x}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$ | (32e)               | Si II        |
| $\mathbf{B}_5$    | $= x_2 \mathbf{a}_1 - (3x_2 - \frac{1}{2}) \mathbf{a}_2 + x_2 \mathbf{a}_3$                 | $=$ | $-a(x_2 - \frac{1}{4}) \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{z}}$ | (32e)               | Si II        |
| $\mathbf{B}_6$    | $= -(3x_2 - \frac{1}{2}) \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$                | $=$ | $ax_2 \hat{\mathbf{x}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{y}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{z}}$  | (32e)               | Si II        |
| $\mathbf{B}_7$    | $= -x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 + (3x_2 + \frac{1}{2}) \mathbf{a}_3$                | $=$ | $a(x_2 + \frac{1}{4}) \hat{\mathbf{x}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$  | (32e)               | Si II        |
| $\mathbf{B}_8$    | $= -x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$                                 | $=$ | $-ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$                                 | (32e)               | Si II        |
| $\mathbf{B}_9$    | $= -x_2 \mathbf{a}_1 + (3x_2 + \frac{1}{2}) \mathbf{a}_2 - x_2 \mathbf{a}_3$                | $=$ | $a(x_2 + \frac{1}{4}) \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{z}}$  | (32e)               | Si II        |
| $\mathbf{B}_{10}$ | $= (3x_2 + \frac{1}{2}) \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$                 | $=$ | $-ax_2 \hat{\mathbf{x}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{y}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{z}}$ | (32e)               | Si II        |
| $\mathbf{B}_{11}$ | $= z_3 \mathbf{a}_1 + z_3 \mathbf{a}_2 + (2x_3 - z_3) \mathbf{a}_3$                         | $=$ | $ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + az_3 \hat{\mathbf{z}}$                                  | (96g)               | Si III       |
| $\mathbf{B}_{12}$ | $= z_3 \mathbf{a}_1 + z_3 \mathbf{a}_2 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_3$           | $=$ | $-a(x_3 - \frac{1}{4}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} + az_3 \hat{\mathbf{z}}$ | (96g)               | Si III       |
| $\mathbf{B}_{13}$ | $= (2x_3 - z_3) \mathbf{a}_1 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_2 + z_3 \mathbf{a}_3$  | $=$ | $-a(x_3 - \frac{1}{4}) \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - a(z_3 - \frac{1}{4}) \hat{\mathbf{z}}$ | (96g)               | Si III       |
| $\mathbf{B}_{14}$ | $= -(2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_1 + (2x_3 - z_3) \mathbf{a}_2 + z_3 \mathbf{a}_3$ | $=$ | $ax_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} - a(z_3 - \frac{1}{4}) \hat{\mathbf{z}}$  | (96g)               | Si III       |
| $\mathbf{B}_{15}$ | $= (2x_3 - z_3) \mathbf{a}_1 + z_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$                         | $=$ | $az_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$                                  | (96g)               | Si III       |
| $\mathbf{B}_{16}$ | $= -(2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_1 + z_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$          | $=$ | $az_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{z}}$  | (96g)               | Si III       |

$$\begin{aligned}
\mathbf{B}_{17} &= z_3 \mathbf{a}_1 + (2x_3 - z_3) \mathbf{a}_2 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_3 = -a(z_3 - \frac{1}{4}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{18} &= z_3 \mathbf{a}_1 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_2 + (2x_3 - z_3) \mathbf{a}_3 = -a(z_3 - \frac{1}{4}) \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{19} &= z_3 \mathbf{a}_1 + (2x_3 - z_3) \mathbf{a}_2 + z_3 \mathbf{a}_3 = ax_3 \hat{\mathbf{x}} + az_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{20} &= z_3 \mathbf{a}_1 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_2 + z_3 \mathbf{a}_3 = -a(x_3 - \frac{1}{4}) \hat{\mathbf{x}} + az_3 \hat{\mathbf{y}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{21} &= -(2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_1 + z_3 \mathbf{a}_2 + (2x_3 - z_3) \mathbf{a}_3 = ax_3 \hat{\mathbf{x}} - a(z_3 - \frac{1}{4}) \hat{\mathbf{y}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{22} &= (2x_3 - z_3) \mathbf{a}_1 + z_3 \mathbf{a}_2 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_3 = -a(x_3 - \frac{1}{4}) \hat{\mathbf{x}} - a(z_3 - \frac{1}{4}) \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{23} &= -z_3 \mathbf{a}_1 - z_3 \mathbf{a}_2 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_3 = a(x_3 + \frac{1}{4}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} - az_3 \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{24} &= -z_3 \mathbf{a}_1 - z_3 \mathbf{a}_2 - (2x_3 - z_3) \mathbf{a}_3 = -ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - az_3 \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{25} &= -(2x_3 - z_3) \mathbf{a}_1 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 - z_3 \mathbf{a}_3 = a(x_3 + \frac{1}{4}) \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + a(z_3 + \frac{1}{4}) \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{26} &= (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 - (2x_3 - z_3) \mathbf{a}_2 - z_3 \mathbf{a}_3 = -ax_3 \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} + a(z_3 + \frac{1}{4}) \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{27} &= -(2x_3 - z_3) \mathbf{a}_1 - z_3 \mathbf{a}_2 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_3 = a(x_3 + \frac{1}{4}) \hat{\mathbf{x}} + a(z_3 + \frac{1}{4}) \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{28} &= (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 - z_3 \mathbf{a}_2 - (2x_3 - z_3) \mathbf{a}_3 = -ax_3 \hat{\mathbf{x}} + a(z_3 + \frac{1}{4}) \hat{\mathbf{y}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{29} &= -z_3 \mathbf{a}_1 - (2x_3 - z_3) \mathbf{a}_2 - z_3 \mathbf{a}_3 = -ax_3 \hat{\mathbf{x}} - az_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{30} &= -z_3 \mathbf{a}_1 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 - z_3 \mathbf{a}_3 = a(x_3 + \frac{1}{4}) \hat{\mathbf{x}} - az_3 \hat{\mathbf{y}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{31} &= -z_3 \mathbf{a}_1 - (2x_3 - z_3) \mathbf{a}_2 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_3 = a(z_3 + \frac{1}{4}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{32} &= -z_3 \mathbf{a}_1 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 - (2x_3 - z_3) \mathbf{a}_3 = a(z_3 + \frac{1}{4}) \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{33} &= (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 - z_3 \mathbf{a}_2 - z_3 \mathbf{a}_3 = -az_3 \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{z}} & (96g) & \text{Si III} \\
\mathbf{B}_{34} &= -(2x_3 - z_3) \mathbf{a}_1 - z_3 \mathbf{a}_2 - z_3 \mathbf{a}_3 = -az_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} & (96g) & \text{Si III}
\end{aligned}$$

## References

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