

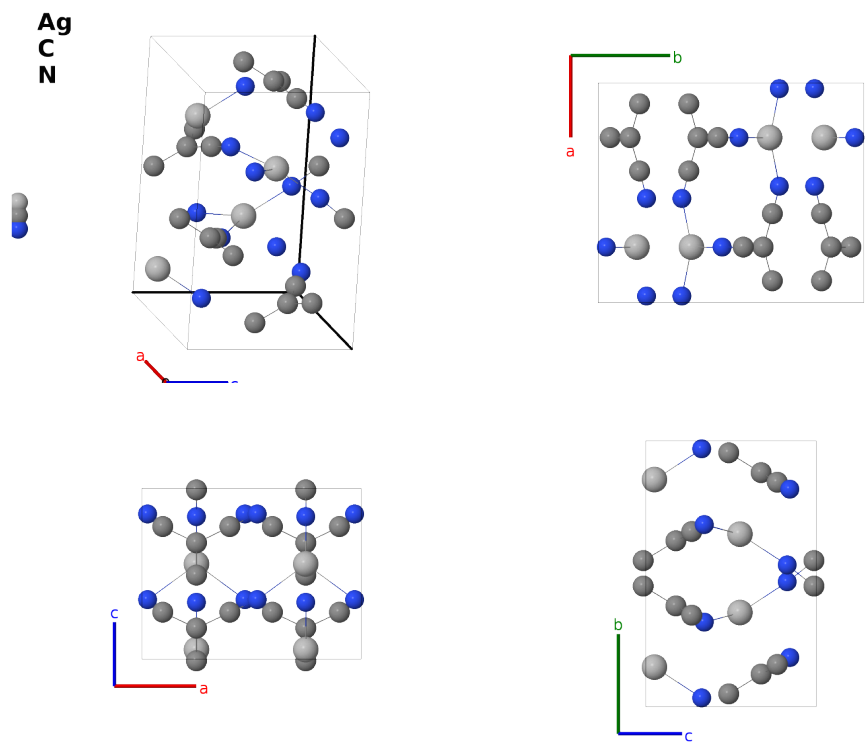
Low Temperature AgC_4N_3 Structure: AB4C3_oI32_46_b_2bc_bc-002

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<https://aflow.org/prototype-encyclopedia/AS99>

https://aflow.org/prototype-encyclopedia/AB4C3_oI32_46_b_2bc_bc-002



Prototype	AgC_4N_3
AFLOW prototype label	AB4C3_oI32_46_b_2bc_bc-002
CCDC	961476
Pearson symbol	oI32
Space group number	46
Space group symbol	$Ima2$
AFLOW prototype command	<pre>aflow --proto=AB4C3_oI32_46_b_2bc_bc-002 --params=a, b/a, c/a, y1, z1, y2, z2, y3, z3, y4, z4, x5, y5, z5, x6, y6, z6</pre>

- This is the structure obtained by (Hodgson, 2014) on cooling to 100K. There is a considerable difference in the structure compared to the room temperature structure even though the space group and Wyckoff positions do not change.

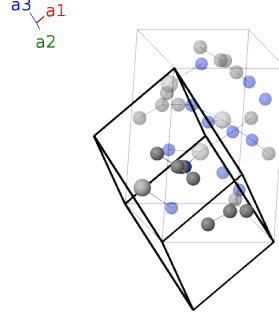
- In chemical literature this is often referred to as Ag(tcm), where tcm is an abbreviation for tricyanomethanide.
- We use the ambient pressure structural data taken at 100K after heating.

Body-centered Orthorhombic primitive vectors

$$\mathbf{a}_1 = -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$$

$$\mathbf{a}_2 = \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$$

$$\mathbf{a}_3 = \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= (y_1 + z_1) \mathbf{a}_1 + (z_1 + \frac{1}{4}) \mathbf{a}_2 + (y_1 + \frac{1}{4}) \mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + by_1\hat{\mathbf{y}} + cz_1\hat{\mathbf{z}}$	(4b)	Ag I
$\mathbf{B}_2$	$= -(y_1 - z_1) \mathbf{a}_1 + (z_1 + \frac{3}{4}) \mathbf{a}_2 - (y_1 - \frac{3}{4}) \mathbf{a}_3$	$=$	$\frac{3}{4}a\hat{\mathbf{x}} - by_1\hat{\mathbf{y}} + cz_1\hat{\mathbf{z}}$	(4b)	Ag I
$\mathbf{B}_3$	$= (y_2 + z_2) \mathbf{a}_1 + (z_2 + \frac{1}{4}) \mathbf{a}_2 + (y_2 + \frac{1}{4}) \mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + by_2\hat{\mathbf{y}} + cz_2\hat{\mathbf{z}}$	(4b)	C I
$\mathbf{B}_4$	$= -(y_2 - z_2) \mathbf{a}_1 + (z_2 + \frac{3}{4}) \mathbf{a}_2 - (y_2 - \frac{3}{4}) \mathbf{a}_3$	$=$	$\frac{3}{4}a\hat{\mathbf{x}} - by_2\hat{\mathbf{y}} + cz_2\hat{\mathbf{z}}$	(4b)	C I
$\mathbf{B}_5$	$= (y_3 + z_3) \mathbf{a}_1 + (z_3 + \frac{1}{4}) \mathbf{a}_2 + (y_3 + \frac{1}{4}) \mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(4b)	C II
$\mathbf{B}_6$	$= -(y_3 - z_3) \mathbf{a}_1 + (z_3 + \frac{3}{4}) \mathbf{a}_2 - (y_3 - \frac{3}{4}) \mathbf{a}_3$	$=$	$\frac{3}{4}a\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(4b)	C II
$\mathbf{B}_7$	$= (y_4 + z_4) \mathbf{a}_1 + (z_4 + \frac{1}{4}) \mathbf{a}_2 + (y_4 + \frac{1}{4}) \mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(4b)	N I
$\mathbf{B}_8$	$= -(y_4 - z_4) \mathbf{a}_1 + (z_4 + \frac{3}{4}) \mathbf{a}_2 - (y_4 - \frac{3}{4}) \mathbf{a}_3$	$=$	$\frac{3}{4}a\hat{\mathbf{x}} - by_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(4b)	N I
$\mathbf{B}_9$	$= (y_5 + z_5) \mathbf{a}_1 + (x_5 + z_5) \mathbf{a}_2 + (x_5 + y_5) \mathbf{a}_3$	$=$	$ax_5\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8c)	C III
$\mathbf{B}_{10}$	$= -(y_5 - z_5) \mathbf{a}_1 - (x_5 - z_5) \mathbf{a}_2 - (x_5 + y_5) \mathbf{a}_3$	$=$	$-ax_5\hat{\mathbf{x}} - by_5\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8c)	C III
$\mathbf{B}_{11}$	$= -(y_5 - z_5) \mathbf{a}_1 + (x_5 + z_5 + \frac{1}{2}) \mathbf{a}_2 + (x_5 - y_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$a(x_5 + \frac{1}{2})\hat{\mathbf{x}} - by_5\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8c)	C III
$\mathbf{B}_{12}$	$= (y_5 + z_5) \mathbf{a}_1 + (-x_5 + z_5 + \frac{1}{2}) \mathbf{a}_2 + (-x_5 + y_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_5 - \frac{1}{2})\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8c)	C III
$\mathbf{B}_{13}$	$= (y_6 + z_6) \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + (x_6 + y_6) \mathbf{a}_3$	$=$	$ax_6\hat{\mathbf{x}} + by_6\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8c)	N II
$\mathbf{B}_{14}$	$= -(y_6 - z_6) \mathbf{a}_1 - (x_6 - z_6) \mathbf{a}_2 - (x_6 + y_6) \mathbf{a}_3$	$=$	$-ax_6\hat{\mathbf{x}} - by_6\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8c)	N II

$$\mathbf{B}_{15} = \begin{matrix} -(y_6 - z_6) \mathbf{a}_1 + \\ (x_6 + z_6 + \frac{1}{2}) \mathbf{a}_2 + \\ (x_6 - y_6 + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = a \left(x_6 + \frac{1}{2} \right) \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (8c) \quad \text{N II}$$

$$\mathbf{B}_{16} = \begin{matrix} (y_6 + z_6) \mathbf{a}_1 + \\ (-x_6 + z_6 + \frac{1}{2}) \mathbf{a}_2 + \\ (-x_6 + y_6 + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = -a \left(x_6 - \frac{1}{2} \right) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (8c) \quad \text{N II}$$

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