

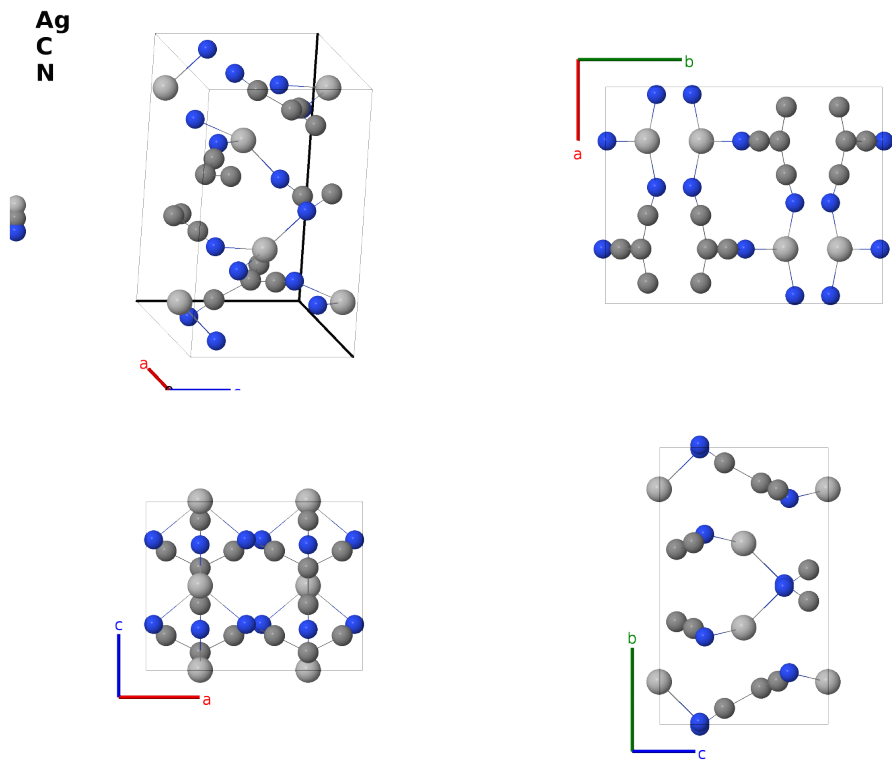
Room Temperature AgC₄N₃ Structure: AB4C3_oI32_46_b_2bc_bc-001

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<https://aflow.org/prototype-encyclopedia/77VH>

https://aflow.org/prototype-encyclopedia/AB4C3_oI32_46_b_2bc_bc-001

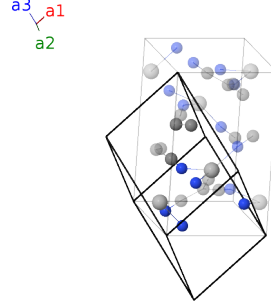


Prototype	AgC ₄ N ₃
AFLOW prototype label	AB4C3_oI32_46_b_2bc_bc-001
ICSD	43823
CCDC	1613281
Pearson symbol	oI32
Space group number	46
Space group symbol	<i>Ima</i> 2
AFLOW prototype command	<code>aflow --proto=AB4C3_oI32_46_b_2bc_bc-001</code> <code>--params=a, b/a, c/a, y₁, z₁, y₂, z₂, y₃, z₃, y₄, z₄, x₅, y₅, z₅, x₆, y₆, z₆</code>

- This is the room temperature structure of AgC_4N_3 . Around 100K it undergoes a significant change in structure which does not change the space group or Wyckoff positions. (Hodgson, 2014). This can be found on the low temperature AgC_4N_3 structure page.
- In chemical literature this is often referred to as $\text{Ag}(\text{tcm})$, where tcm is an abbreviation for tricyanomethanide.
- (Konnert, 2014) swapped the x - and z -axes compared to the standard setting of space group $Ima2$ #46. We used AFLOW to transform this to the standard orientation.

Body-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= (y_1 + z_1) \mathbf{a}_1 + (z_1 + \frac{1}{4}) \mathbf{a}_2 + (y_1 + \frac{1}{4}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + by_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(4b)	Ag I
$\mathbf{B}_2$	$= -(y_1 - z_1) \mathbf{a}_1 + (z_1 + \frac{3}{4}) \mathbf{a}_2 - (y_1 - \frac{3}{4}) \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{\mathbf{x}} - by_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(4b)	Ag I
$\mathbf{B}_3$	$= (y_2 + z_2) \mathbf{a}_1 + (z_2 + \frac{1}{4}) \mathbf{a}_2 + (y_2 + \frac{1}{4}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(4b)	C I
$\mathbf{B}_4$	$= -(y_2 - z_2) \mathbf{a}_1 + (z_2 + \frac{3}{4}) \mathbf{a}_2 - (y_2 - \frac{3}{4}) \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(4b)	C I
$\mathbf{B}_5$	$= (y_3 + z_3) \mathbf{a}_1 + (z_3 + \frac{1}{4}) \mathbf{a}_2 + (y_3 + \frac{1}{4}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(4b)	C II
$\mathbf{B}_6$	$= -(y_3 - z_3) \mathbf{a}_1 + (z_3 + \frac{3}{4}) \mathbf{a}_2 - (y_3 - \frac{3}{4}) \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(4b)	C II
$\mathbf{B}_7$	$= (y_4 + z_4) \mathbf{a}_1 + (z_4 + \frac{1}{4}) \mathbf{a}_2 + (y_4 + \frac{1}{4}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(4b)	N I
$\mathbf{B}_8$	$= -(y_4 - z_4) \mathbf{a}_1 + (z_4 + \frac{3}{4}) \mathbf{a}_2 - (y_4 - \frac{3}{4}) \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(4b)	N I
$\mathbf{B}_9$	$= (y_5 + z_5) \mathbf{a}_1 + (x_5 + z_5) \mathbf{a}_2 + (x_5 + y_5) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8c)	C III
$\mathbf{B}_{10}$	$= -(y_5 - z_5) \mathbf{a}_1 - (x_5 - z_5) \mathbf{a}_2 - (x_5 + y_5) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8c)	C III
$\mathbf{B}_{11}$	$= -(y_5 - z_5) \mathbf{a}_1 + (x_5 + z_5 + \frac{1}{2}) \mathbf{a}_2 + (x_5 - y_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$a(x_5 + \frac{1}{2}) \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8c)	C III
$\mathbf{B}_{12}$	$= (y_5 + z_5) \mathbf{a}_1 + (-x_5 + z_5 + \frac{1}{2}) \mathbf{a}_2 + (-x_5 + y_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_5 - \frac{1}{2}) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8c)	C III

$$\mathbf{B}_{13} = \begin{pmatrix} (y_6 + z_6) \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + \\ (x_6 + y_6) \mathbf{a}_3 \end{pmatrix} = ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (8c) \quad \text{N II}$$

$$\mathbf{B}_{14} = -\begin{pmatrix} (y_6 - z_6) \mathbf{a}_1 - (x_6 - z_6) \mathbf{a}_2 - \\ (x_6 + y_6) \mathbf{a}_3 \end{pmatrix} = -ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (8c) \quad \text{N II}$$

$$\mathbf{B}_{15} = \begin{pmatrix} -(y_6 - z_6) \mathbf{a}_1 + \\ (x_6 + z_6 + \frac{1}{2}) \mathbf{a}_2 + \\ (x_6 - y_6 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a \left(x_6 + \frac{1}{2}\right) \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (8c) \quad \text{N II}$$

$$\mathbf{B}_{16} = \begin{pmatrix} (y_6 + z_6) \mathbf{a}_1 + \\ (-x_6 + z_6 + \frac{1}{2}) \mathbf{a}_2 + \\ (-x_6 + y_6 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a \left(x_6 - \frac{1}{2}\right) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (8c) \quad \text{N II}$$

References

- [1] J. Konnert and D. Britton, *The Crystal Structure of AgC(CN)₃*, Inorg. Chem. **5**, 1191–1196 (1966), doi:10.1021/ic50041a026.
- [2] S. A. Hodgson, J. Adamson, S. J. Hunt, M. J. Cliffe, A. B. Cairns, A. L. Thompson, M. G. Tucker, N. P. Funnell, and A. L. Goodwin, *Negative area compressibility in silver(I) tricyanomethanide*, Chem. Commun. **50**, 5264–5266 (2014), doi:10.1039/C3CC47032F.

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