

Copper (I) Azide (CuN₃) Structure: AB3_tI32_88_c_df-001

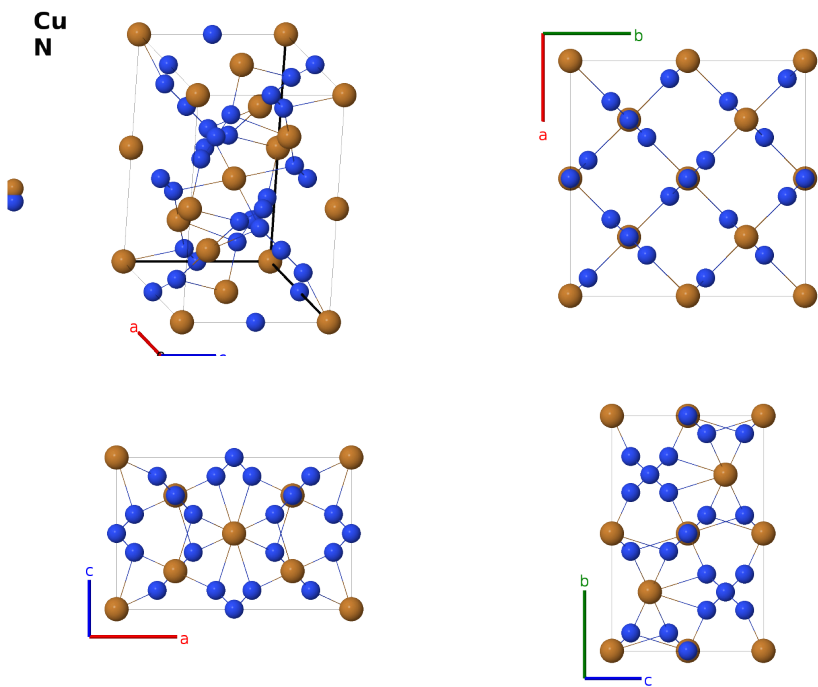
This structure previously used the label(s) **AB3-tI32_88_d_cf**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/L0WX>

https://aflow.org/prototype-encyclopedia/AB3_tI32_88_c_df-001



Prototype	CuN ₃
AFLOW prototype label	AB3_tI32_88_c_df-001
Mineral name	copper (I) azide
ICSD	30633
CCDC	1604878
Pearson symbol	tI32
Space group number	88
Space group symbol	<i>I</i> 4 ₁ / <i>a</i>
AFLOW prototype command	<code>aflow --proto=AB3_tI32_88_c_df-001</code> <code>--params=<i>a</i>, <i>c/a</i>, <i>x</i>₃, <i>y</i>₃, <i>z</i>₃</code>

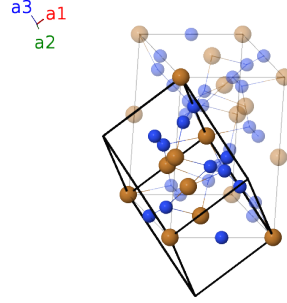
Other compounds with this structure

AgN₃, TiN₃

- Not to be confused with Copper (II) Azide, Cu(N₃)₂, an explosive.
- (Wilsdorf, 1948) gave the Wyckoff positions in setting 1 of space group $P4_1/a$ #88. We used findsym to translate this to the standard setting 2.

Body-centered Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	0	$=$	0	(8c)	Cu I
$\mathbf{B}_2$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{y}}$	(8c)	Cu I
$\mathbf{B}_3$	$\frac{1}{2} \mathbf{a}_1$	$=$	$-\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8c)	Cu I
$\mathbf{B}_4$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8c)	Cu I
$\mathbf{B}_5$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2}c \hat{\mathbf{z}}$	(8d)	N I
$\mathbf{B}_6$	$\frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}}$	(8d)	N I
$\mathbf{B}_7$	$\frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - \frac{1}{4}a \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8d)	N I
$\mathbf{B}_8$	$\frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} - \frac{1}{4}c \hat{\mathbf{z}}$	(8d)	N I
$\mathbf{B}_9$	$(y_3 + z_3) \mathbf{a}_1 + (x_3 + z_3) \mathbf{a}_2 + (x_3 + y_3) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(16f)	N II
$\mathbf{B}_{10}$	$(-y_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 - (x_3 - z_3) \mathbf{a}_2 - (x_3 + y_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - a(y_3 - \frac{1}{2}) \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(16f)	N II
$\mathbf{B}_{11}$	$(x_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 - (y_3 - z_3) \mathbf{a}_2 + (x_3 - y_3) \mathbf{a}_3$	$=$	$-a(y_3 + \frac{1}{4}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} + c(z_3 + \frac{1}{4}) \hat{\mathbf{z}}$	(16f)	N II
$\mathbf{B}_{12}$	$(-x_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 + (y_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 + (-x_3 + y_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$a(y_3 + \frac{1}{4}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} + c(z_3 + \frac{1}{4}) \hat{\mathbf{z}}$	(16f)	N II
$\mathbf{B}_{13}$	$-(y_3 + z_3) \mathbf{a}_1 - (x_3 + z_3) \mathbf{a}_2 - (x_3 + y_3) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(16f)	N II
$\mathbf{B}_{14}$	$(y_3 - z_3 + \frac{1}{2}) \mathbf{a}_1 + (x_3 - z_3) \mathbf{a}_2 + (x_3 + y_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + a(y_3 + \frac{1}{2}) \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(16f)	N II
$\mathbf{B}_{15}$	$-(x_3 + z_3 - \frac{1}{2}) \mathbf{a}_1 + (y_3 - z_3) \mathbf{a}_2 - (x_3 - y_3) \mathbf{a}_3$	$=$	$a(y_3 - \frac{1}{4}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} - c(z_3 - \frac{1}{4}) \hat{\mathbf{z}}$	(16f)	N II

$$\mathbf{B}_{16} = \begin{pmatrix} x_3 - z_3 + \frac{1}{2} \\ y_3 + z_3 - \frac{1}{2} \\ x_3 - y_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} -a(y_3 - \frac{1}{4})\hat{\mathbf{x}} + a(x_3 + \frac{1}{4})\hat{\mathbf{y}} - c(z_3 - \frac{1}{4})\hat{\mathbf{z}} \end{pmatrix} \quad (16f) \quad \text{N II}$$

References

- [1] H. Wilsdorf, *Die Kristallstruktur des einwertigen Kupferazids, CuN_3* , Acta Cryst. **1**, 115–118 (1948), doi:10.1107/S0365110X48000314.

Found in

- [1] W. Zhu and H. Xiao, *Ab initio study of electronic structure and optical properties of heavy-metal azides: TlN_3 , AgN_3 , and CuN_3* , J. Comput. Chem. **29**, 176–184 (2008), doi:10.1002/jcc.20682.

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