

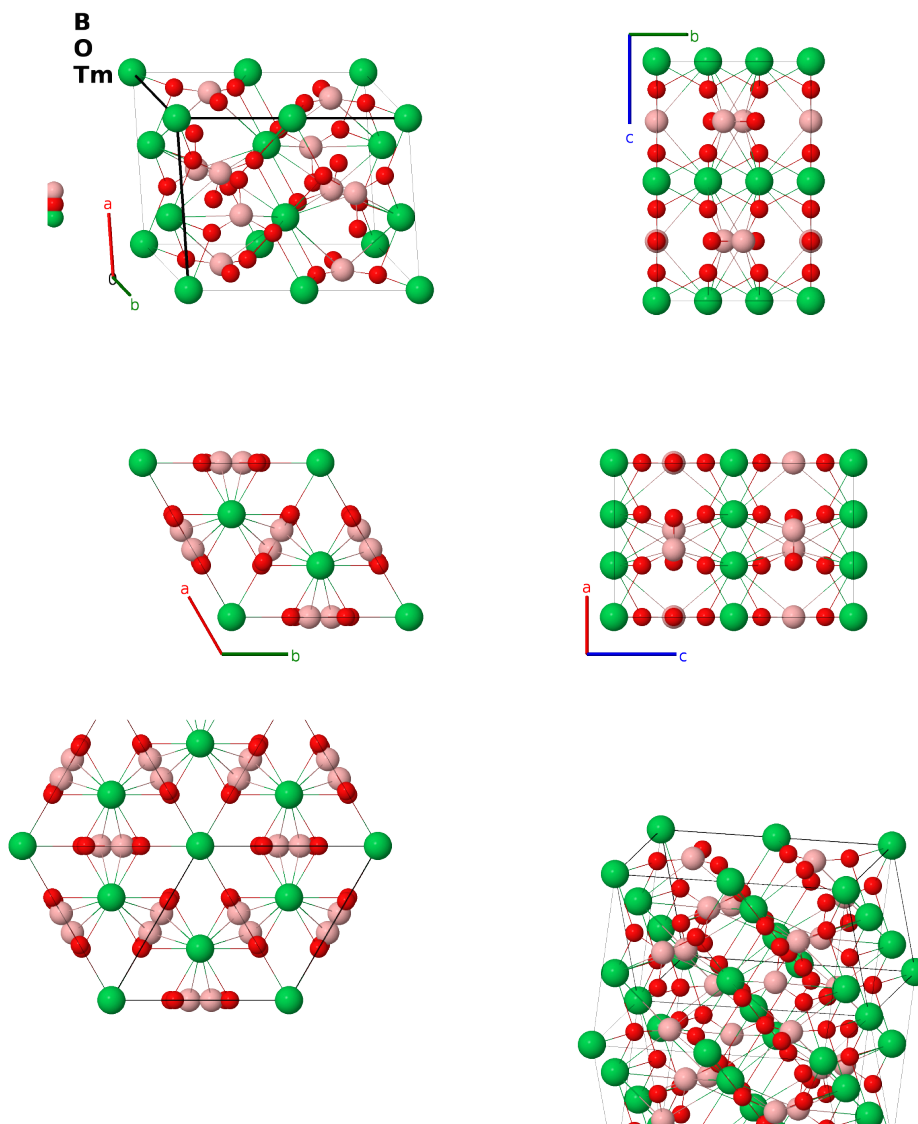
Ordered TmBO₃ Structure: AB3C_hP30_193_g_gk_bd-001

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<https://aflow.org/prototype-encyclopedia/AE3Q>

https://aflow.org/prototype-encyclopedia/AB3C_hP30_193_g_gk_bd-001



Prototype	BO ₃ Tm
AFLOW prototype label	AB3C_hP30_193_g_gk_bd-001
ICSD	27942
CCDC	1603102

Pearson symbol	hP30
Space group number	193
Space group symbol	$P6_3/mcm$
AFLOW prototype command	<code>aflow --proto=AB3C_hP30_193_g_gk_bd-001</code> <code>--params=a,c/a,x₃,x₄,x₅,z₅</code>

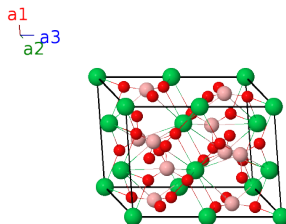
Other compounds with this structure

DyBO₃, ErBO₃, EuBO₃, GdBO₃, HoBO₃, LuBO₃, SmBO₃, YBO₃, YbBO₃

- (Newnham, 1963) found two possible structures for TmBO₃ and YBO₃:
 - A compact hexagonal cell with partially disordered boron and oxygen atoms, and
 - this structure, which has a larger hexagonal cell but completely ordered atoms.
- There are several problems with this structure:
 - The ICSD entry 27942 places this structure in space group $P\bar{6}c2$ #188 even though the positions are such that the structure can be resolved in the higher symmetry $P6_3/mcm$ space group, and
 - the positions of the O I atoms are such that the O-O distance is less than 1 Å.
 - The ICSD entry gives what seem to be reasonable O-O distances, so we use those coordinates, using AFLOW to transform the structure into space group $P6_3/mcm$.

Hexagonal primitive vectors

$$\begin{aligned}
 \mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}a \hat{\mathbf{y}} \\
 \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}a \hat{\mathbf{y}} \\
 \mathbf{a}_3 &= c \hat{\mathbf{z}}
 \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	0	$=$	0	(2b) Tm I
$\mathbf{B}_2$	$=$	$\frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} c \hat{\mathbf{z}}$	(2b) Tm I
$\mathbf{B}_3$	$=$	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}}$	(4d) Tm II
$\mathbf{B}_4$	$=$	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4d) Tm II
$\mathbf{B}_5$	$=$	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a \hat{\mathbf{y}}$	(4d) Tm II
$\mathbf{B}_6$	$=$	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4d) Tm II
$\mathbf{B}_7$	$=$	$x_3 \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a x_3 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2} a x_3 \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(6g) B I
$\mathbf{B}_8$	$=$	$x_3 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a x_3 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2} a x_3 \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(6g) B I
$\mathbf{B}_9$	$=$	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$-a x_3 \hat{\mathbf{x}} + \frac{1}{4} c \hat{\mathbf{z}}$	(6g) B I

$\mathbf{B}_{10} =$	$-x_3 \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_3$	$=$	$-\frac{1}{2}ax_3 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_3 \hat{\mathbf{y}} + \frac{3}{4}c \hat{\mathbf{z}}$	(6g)	B I
$\mathbf{B}_{11} =$	$-x_3 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-\frac{1}{2}ax_3 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_3 \hat{\mathbf{y}} + \frac{3}{4}c \hat{\mathbf{z}}$	(6g)	B I
$\mathbf{B}_{12} =$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + \frac{3}{4}c \hat{\mathbf{z}}$	(6g)	B I
$\mathbf{B}_{13} =$	$x_4 \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2}ax_4 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_4 \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(6g)	O I
$\mathbf{B}_{14} =$	$x_4 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2}ax_4 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_4 \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(6g)	O I
$\mathbf{B}_{15} =$	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + \frac{1}{4}c \hat{\mathbf{z}}$	(6g)	O I
$\mathbf{B}_{16} =$	$-x_4 \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_3$	$=$	$-\frac{1}{2}ax_4 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_4 \hat{\mathbf{y}} + \frac{3}{4}c \hat{\mathbf{z}}$	(6g)	O I
$\mathbf{B}_{17} =$	$-x_4 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-\frac{1}{2}ax_4 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_4 \hat{\mathbf{y}} + \frac{3}{4}c \hat{\mathbf{z}}$	(6g)	O I
$\mathbf{B}_{18} =$	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + \frac{3}{4}c \hat{\mathbf{z}}$	(6g)	O I
$\mathbf{B}_{19} =$	$x_5 \mathbf{a}_1 + z_5 \mathbf{a}_3$	$=$	$\frac{1}{2}ax_5 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{20} =$	$x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$\frac{1}{2}ax_5 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{21} =$	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + cz_5 \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{22} =$	$-x_5 \mathbf{a}_1 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-\frac{1}{2}ax_5 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{23} =$	$-x_5 \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-\frac{1}{2}ax_5 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{24} =$	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + c(z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{25} =$	$x_5 \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}ax_5 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} - c(z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{26} =$	$x_5 \mathbf{a}_1 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}ax_5 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} - c(z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{27} =$	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - c(z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{28} =$	$-x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$-\frac{1}{2}ax_5 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{29} =$	$-x_5 \mathbf{a}_1 - z_5 \mathbf{a}_3$	$=$	$-\frac{1}{2}ax_5 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(12k)	O II
$\mathbf{B}_{30} =$	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} - cz_5 \hat{\mathbf{z}}$	(12k)	O II

References

- [1] R. E. Newnham, M. J. Redman, and R. P. Santoro, *Crystal Structure of Yttrium and Other Rare-Earth Borates*, J. Am. Ceram. Soc. **46**, 253–256 (1963), doi:10.1111/j.1151-2916.1963.tb11721.x.

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