

α -PdSn₂ Structure:

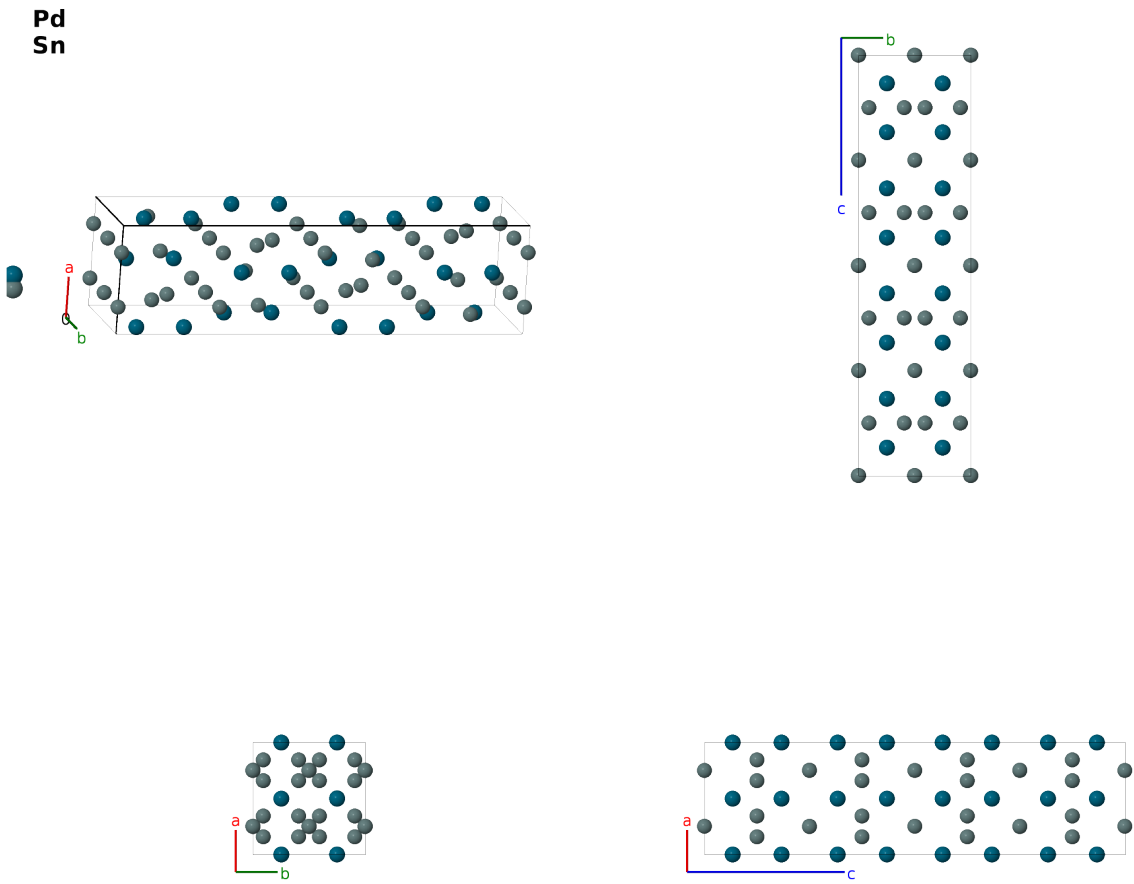
AB2_tI48_142_d_ef-001

Cite this page as:

- H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettl, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.
- D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/FUUU>

https://aflow.org/prototype-encyclopedia/AB2_tI48_142_d_ef-001



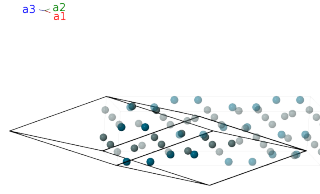
Prototype	PdSn ₂
AFLOW prototype label	AB2_tI48_142_d_ef-001
ICSD	30235
CCDC	1604605
Pearson symbol	tI48

Space group number	142
Space group symbol	$I4_1/acd$
AFLOW prototype command	<code>aflow --proto=AB2_tI48_142_d_ef-001</code> <code>--params=a, c/a, z₁, x₂, x₃</code>

- This structure is stable up to 600°C. (Villars, 2016)
- PdSn₂ has also been found in the orthorhombic C_e structure.
- The ICSD entry is from (Hellner, 1956), but we use the refined data from (Künnen, 2000), which has no ICSD or CCDC listing, for this presentation.

Body-centered Tetragonal primitive vectors

$$\begin{aligned}
\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\
\mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\
\mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}
\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$(z_1 + \frac{1}{4}) \mathbf{a}_1 + z_1 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(16d)	Pd I
$\mathbf{B}_2$	$z_1 \mathbf{a}_1 + (z_1 + \frac{1}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + c(z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Pd I
$\mathbf{B}_3$	$-(z_1 - \frac{1}{4}) \mathbf{a}_1 - (z_1 - \frac{1}{2}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16d)	Pd I
$\mathbf{B}_4$	$-(z_1 - \frac{1}{2}) \mathbf{a}_1 - (z_1 - \frac{1}{4}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{y}} - c(z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Pd I
$\mathbf{B}_5$	$-(z_1 - \frac{3}{4}) \mathbf{a}_1 - z_1 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	=	$\frac{3}{4}a \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16d)	Pd I
$\mathbf{B}_6$	$-z_1 \mathbf{a}_1 - (z_1 - \frac{3}{4}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{4}a \hat{\mathbf{y}} - c(z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Pd I
$\mathbf{B}_7$	$(z_1 + \frac{3}{4}) \mathbf{a}_1 + (z_1 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{y}} + c(z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(16d)	Pd I
$\mathbf{B}_8$	$(z_1 + \frac{1}{2}) \mathbf{a}_1 + (z_1 + \frac{3}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + c(z_1 + \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Pd I
$\mathbf{B}_9$	$\frac{1}{4} \mathbf{a}_1 + (x_2 + \frac{1}{4}) \mathbf{a}_2 + x_2 \mathbf{a}_3$	=	$ax_2 \hat{\mathbf{x}} + \frac{1}{4}c \hat{\mathbf{z}}$	(16e)	Sn I
$\mathbf{B}_{10}$	$\frac{3}{4} \mathbf{a}_1 - (x_2 - \frac{1}{4}) \mathbf{a}_2 - (x_2 - \frac{1}{2}) \mathbf{a}_3$	=	$-ax_2 \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(16e)	Sn I
$\mathbf{B}_{11}$	$(x_2 + \frac{1}{4}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + x_2 \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{x}} + a(x_2 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(16e)	Sn I
$\mathbf{B}_{12}$	$-(x_2 - \frac{1}{4}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - (x_2 - \frac{1}{2}) \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{x}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{y}}$	(16e)	Sn I
$\mathbf{B}_{13}$	$\frac{3}{4} \mathbf{a}_1 - (x_2 - \frac{3}{4}) \mathbf{a}_2 - x_2 \mathbf{a}_3$	=	$-ax_2 \hat{\mathbf{x}} + \frac{3}{4}c \hat{\mathbf{z}}$	(16e)	Sn I
$\mathbf{B}_{14}$	$\frac{1}{4} \mathbf{a}_1 + (x_2 + \frac{3}{4}) \mathbf{a}_2 + (x_2 + \frac{1}{2}) \mathbf{a}_3$	=	$a(x_2 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{4}c \hat{\mathbf{z}}$	(16e)	Sn I
$\mathbf{B}_{15}$	$-(x_2 - \frac{3}{4}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - x_2 \mathbf{a}_3$	=	$-\frac{1}{4}a \hat{\mathbf{x}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(16e)	Sn I
$\mathbf{B}_{16}$	$(x_2 + \frac{3}{4}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + (x_2 + \frac{1}{2}) \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{x}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(16e)	Sn I

$$\begin{aligned}
\mathbf{B}_{17} &= \begin{pmatrix} (x_3 + \frac{3}{8}) \mathbf{a}_1 + (x_3 + \frac{1}{8}) \mathbf{a}_2 + \\ (2x_3 + \frac{1}{4}) \mathbf{a}_3 \end{pmatrix} = ax_3 \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}} & (16f) & \text{Sn II} \\
\mathbf{B}_{18} &= \begin{pmatrix} -(x_3 - \frac{3}{8}) \mathbf{a}_1 - (x_3 - \frac{1}{8}) \mathbf{a}_2 - \\ (2x_3 - \frac{1}{4}) \mathbf{a}_3 \end{pmatrix} = -ax_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}} & (16f) & \text{Sn II} \\
\mathbf{B}_{19} &= \begin{pmatrix} (x_3 + \frac{1}{8}) \mathbf{a}_1 - (x_3 - \frac{3}{8}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 \end{pmatrix} = -a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{8}c \hat{\mathbf{z}} & (16f) & \text{Sn II} \\
\mathbf{B}_{20} &= \begin{pmatrix} -(x_3 - \frac{1}{8}) \mathbf{a}_1 + (x_3 + \frac{3}{8}) \mathbf{a}_2 + \\ \frac{3}{4} \mathbf{a}_3 \end{pmatrix} = a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{8}c \hat{\mathbf{z}} & (16f) & \text{Sn II} \\
\mathbf{B}_{21} &= \begin{pmatrix} -(x_3 - \frac{5}{8}) \mathbf{a}_1 - (x_3 - \frac{7}{8}) \mathbf{a}_2 - \\ (2x_3 - \frac{3}{4}) \mathbf{a}_3 \end{pmatrix} = -a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}} & (16f) & \text{Sn II} \\
\mathbf{B}_{22} &= \begin{pmatrix} (x_3 + \frac{5}{8}) \mathbf{a}_1 + (x_3 + \frac{7}{8}) \mathbf{a}_2 + \\ (2x_3 + \frac{3}{4}) \mathbf{a}_3 \end{pmatrix} = a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}} & (16f) & \text{Sn II} \\
\mathbf{B}_{23} &= \begin{pmatrix} -(x_3 - \frac{7}{8}) \mathbf{a}_1 + (x_3 + \frac{5}{8}) \mathbf{a}_2 + \\ \frac{1}{4} \mathbf{a}_3 \end{pmatrix} = ax_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{5}{8}c \hat{\mathbf{z}} & (16f) & \text{Sn II} \\
\mathbf{B}_{24} &= \begin{pmatrix} (x_3 + \frac{7}{8}) \mathbf{a}_1 - (x_3 - \frac{5}{8}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3 \end{pmatrix} = -ax_3 \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{5}{8}c \hat{\mathbf{z}} & (16f) & \text{Sn II}
\end{aligned}$$

References

- [1] E. Hellner, *Flu-Misch-Typen*, Zeitschrift für Kristallographie **107**, 99–123 (1956), doi:10.1524/zkri.1956.107.16.99.
- [2] P. Villars, ed., *PAULING FILE* (Springer, 2016), chap. Pd-Sn Binary Phase Diagram 0-100 at.% Sn.

Found in

- [1] B. Künnen, D. Niepmann, and W. Jeitschko, *Structure refinements and some properties of the transition metal stannides Os_3Sn_7 , Ir_5Sn_7 , $Ni_{0.402(4)}Pd_{0.598}Sn_4$, α - $PdSn_2$ and $PtSn_4$* , J. Alloys Compd. **309**, 1–9 (2000), doi:10.1016/S0925-8388(00)01042-2.

First cited in

H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettl, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.