

Modern $C26$ (NO_2) Structure: AB2_cI36_204_d_g-001

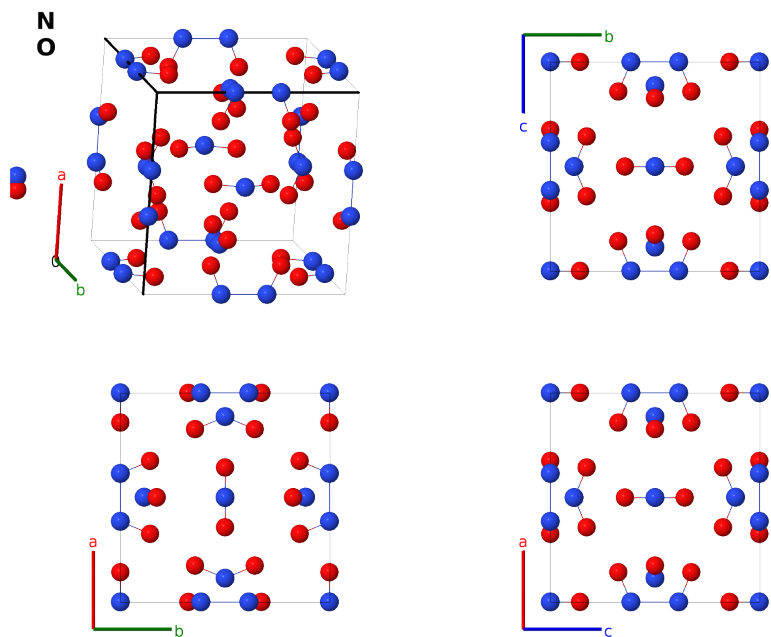
This structure previously used the label(s) **AB2_cI36_204_d_g**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/XJC7>

https://aflow.org/prototype-encyclopedia/AB2_cI36_204_d_g-001

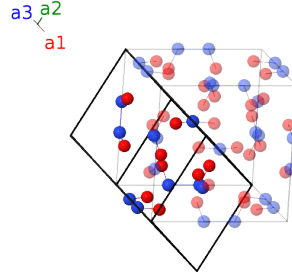


Prototype	NO_2
AFLOW prototype label	AB2_cI36_204_d_g-001
<i>Strukturbericht</i> designation	$C26$
ICSD	201140
CCDC	1705882
Pearson symbol	cI36
Space group number	204
Space group symbol	$Im\bar{3}$
AFLOW prototype command	<code>aflow --proto=AB2_cI36_204_d_g-001</code> <code>--params=a, x_1, y_2, z_2</code>

- (Hermann, 1937) listed two possible structures for the low temperature solid cubic phase of NO₂, which were given *Strukturbericht* designations *C26_a* and *C26_b*, the only structures with Roman subscripts in the original series.
- *C26_a* (AB2_cI36_199_b_c) was set in space group *I2₁3* #199. Hermann noted that this structure has a very short distance (1.88Å) between oxygen atoms on different NO₂ molecules, and that this structure does not form the (NO₂)₂ aggregate molecule found in the *C26_b* structure, making “making this proposed structure very unlikely.”
- Recognizing this, (Hendricks, 1931) suggested that NO₂ was actually in space group *I23* #197. (Hermann, 1997) gave this structure the *C26_b* designation, but noted that based on Hendricks’s atomic positions the space group was actually *Im* $\bar{3}$ #204.
- The modern accepted structure for No₂, AB2_cI36_204_d_g, is set in space group *Im* $\bar{3}$, confirming Hendricks. We follow (Villars, 2005) and give this the *C26* designation, depreciating the *C26_b* label.
- We used the experimental data for this phase collected at 20K.

Body-centered Cubic primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}a \hat{\mathbf{z}} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	=	$ax_1 \hat{\mathbf{x}}$	(12d)	N I
$\mathbf{B}_2$	$-x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	=	$-ax_1 \hat{\mathbf{x}}$	(12d)	N I
$\mathbf{B}_3$	$x_1 \mathbf{a}_1 + x_1 \mathbf{a}_3$	=	$ax_1 \hat{\mathbf{y}}$	(12d)	N I
$\mathbf{B}_4$	$-x_1 \mathbf{a}_1 - x_1 \mathbf{a}_3$	=	$-ax_1 \hat{\mathbf{y}}$	(12d)	N I
$\mathbf{B}_5$	$x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2$	=	$ax_1 \hat{\mathbf{z}}$	(12d)	N I
$\mathbf{B}_6$	$-x_1 \mathbf{a}_1 - x_1 \mathbf{a}_2$	=	$-ax_1 \hat{\mathbf{z}}$	(12d)	N I
$\mathbf{B}_7$	$(y_2 + z_2) \mathbf{a}_1 + z_2 \mathbf{a}_2 + y_2 \mathbf{a}_3$	=	$ay_2 \hat{\mathbf{y}} + az_2 \hat{\mathbf{z}}$	(24g)	O I
$\mathbf{B}_8$	$-(y_2 - z_2) \mathbf{a}_1 + z_2 \mathbf{a}_2 - y_2 \mathbf{a}_3$	=	$-ay_2 \hat{\mathbf{y}} + az_2 \hat{\mathbf{z}}$	(24g)	O I
$\mathbf{B}_9$	$(y_2 - z_2) \mathbf{a}_1 - z_2 \mathbf{a}_2 + y_2 \mathbf{a}_3$	=	$ay_2 \hat{\mathbf{y}} - az_2 \hat{\mathbf{z}}$	(24g)	O I
$\mathbf{B}_{10}$	$-(y_2 + z_2) \mathbf{a}_1 - z_2 \mathbf{a}_2 - y_2 \mathbf{a}_3$	=	$-ay_2 \hat{\mathbf{y}} - az_2 \hat{\mathbf{z}}$	(24g)	O I
$\mathbf{B}_{11}$	$y_2 \mathbf{a}_1 + (y_2 + z_2) \mathbf{a}_2 + z_2 \mathbf{a}_3$	=	$az_2 \hat{\mathbf{x}} + ay_2 \hat{\mathbf{z}}$	(24g)	O I
$\mathbf{B}_{12}$	$-y_2 \mathbf{a}_1 - (y_2 - z_2) \mathbf{a}_2 + z_2 \mathbf{a}_3$	=	$az_2 \hat{\mathbf{x}} - ay_2 \hat{\mathbf{z}}$	(24g)	O I
$\mathbf{B}_{13}$	$y_2 \mathbf{a}_1 + (y_2 - z_2) \mathbf{a}_2 - z_2 \mathbf{a}_3$	=	$-az_2 \hat{\mathbf{x}} + ay_2 \hat{\mathbf{z}}$	(24g)	O I
$\mathbf{B}_{14}$	$-y_2 \mathbf{a}_1 - (y_2 + z_2) \mathbf{a}_2 - z_2 \mathbf{a}_3$	=	$-az_2 \hat{\mathbf{x}} - ay_2 \hat{\mathbf{z}}$	(24g)	O I
$\mathbf{B}_{15}$	$z_2 \mathbf{a}_1 + y_2 \mathbf{a}_2 + (y_2 + z_2) \mathbf{a}_3$	=	$ay_2 \hat{\mathbf{x}} + az_2 \hat{\mathbf{y}}$	(24g)	O I
$\mathbf{B}_{16}$	$z_2 \mathbf{a}_1 - y_2 \mathbf{a}_2 - (y_2 - z_2) \mathbf{a}_3$	=	$-ay_2 \hat{\mathbf{x}} + az_2 \hat{\mathbf{y}}$	(24g)	O I
$\mathbf{B}_{17}$	$-z_2 \mathbf{a}_1 + y_2 \mathbf{a}_2 + (y_2 - z_2) \mathbf{a}_3$	=	$ay_2 \hat{\mathbf{x}} - az_2 \hat{\mathbf{y}}$	(24g)	O I
$\mathbf{B}_{18}$	$-z_2 \mathbf{a}_1 - y_2 \mathbf{a}_2 - (y_2 + z_2) \mathbf{a}_3$	=	$-ay_2 \hat{\mathbf{x}} - az_2 \hat{\mathbf{y}}$	(24g)	O I

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Found in

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