

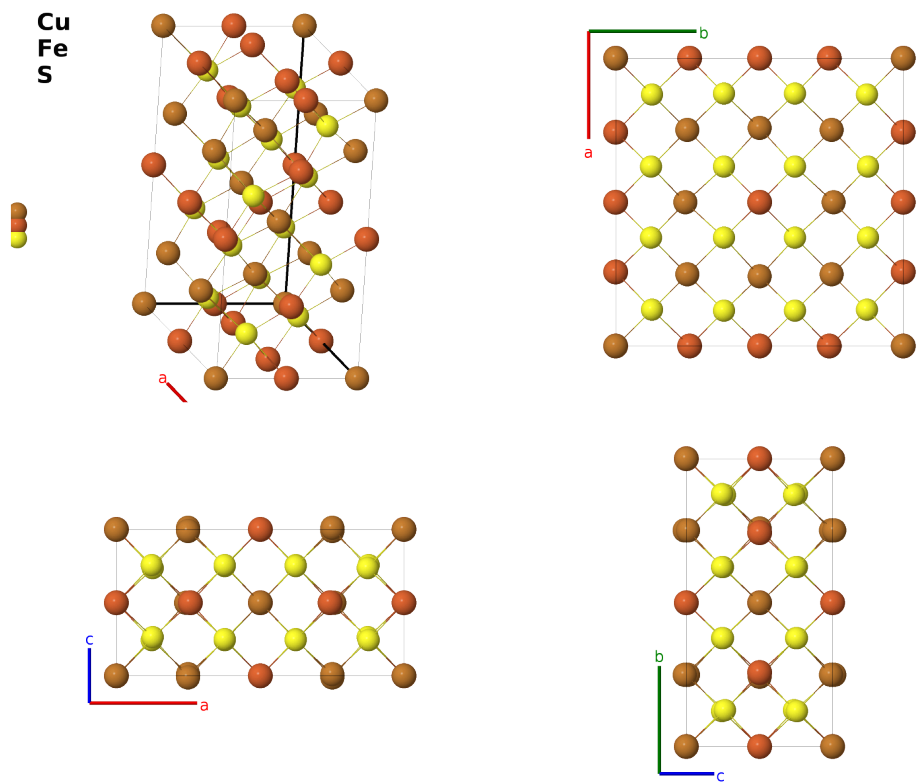
Mooihoekite (Cu₉Fe₉S₁₆) Structure: A9B9C16_tP34_111_ajn_bcdek_2no-001

Cite this page as:

- H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettl, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.
- D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/2KD6>

https://aflow.org/prototype-encyclopedia/A9B9C16_tP34_111_ajn_bcdek_2no-001



Prototype	Cu ₉ Fe ₉ S ₁₆
AFLOW prototype label	A9B9C16_tP34_111_ajn_bcdek_2no-001
Mineral name	mooihoekite
ICSD	2649
CCDC	1592517
Pearson symbol	tP34
Space group number	111
Space group symbol	$P\bar{4}2m$
AFLOW prototype command	<code>aflow --proto=A9B9C16_tP34_111_ajn_bcdek_2no-001</code> <code>--params=a, c/a, x₆, x₇, x₈, z₈, x₉, z₉, x₁₀, z₁₀, x₁₁, y₁₁, z₁₁</code>

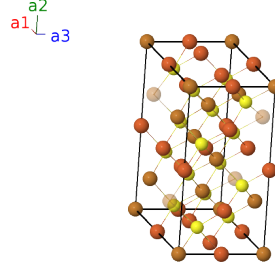
- We have shifted the origin by $a/2(\hat{x} + \hat{y})$ from that used by (Hall, 1973).

Simple Tetragonal primitive vectors

$$\mathbf{a}_1 = a \hat{\mathbf{x}}$$

$$\mathbf{a}_2 = a \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = c \hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	0	$=$	0	(1a) Cu I
$\mathbf{B}_2$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(1b) Fe I
$\mathbf{B}_3$	$=$	$\frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} c \hat{\mathbf{z}}$	(1c) Fe II
$\mathbf{B}_4$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(1d) Fe III
$\mathbf{B}_5$	$=$	$\frac{1}{2} \mathbf{a}_1$	$=$	$\frac{1}{2} a \hat{\mathbf{x}}$	(2e) Fe IV
$\mathbf{B}_6$	$=$	$\frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{y}}$	(2e) Fe IV
$\mathbf{B}_7$	$=$	$x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4j) Cu II
$\mathbf{B}_8$	$=$	$-x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4j) Cu II
$\mathbf{B}_9$	$=$	$\frac{1}{2} \mathbf{a}_1 - x_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4j) Cu II
$\mathbf{B}_{10}$	$=$	$\frac{1}{2} \mathbf{a}_1 + x_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4j) Cu II
$\mathbf{B}_{11}$	$=$	$x_7 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4k) Fe V
$\mathbf{B}_{12}$	$=$	$-x_7 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4k) Fe V
$\mathbf{B}_{13}$	$=$	$-x_7 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4k) Fe V
$\mathbf{B}_{14}$	$=$	$x_7 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4k) Fe V
$\mathbf{B}_{15}$	$=$	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(4n) Cu III
$\mathbf{B}_{16}$	$=$	$-x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(4n) Cu III
$\mathbf{B}_{17}$	$=$	$x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(4n) Cu III
$\mathbf{B}_{18}$	$=$	$-x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(4n) Cu III
$\mathbf{B}_{19}$	$=$	$x_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} + ax_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(4n) S I
$\mathbf{B}_{20}$	$=$	$-x_9 \mathbf{a}_1 - x_9 \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} - ax_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(4n) S I
$\mathbf{B}_{21}$	$=$	$x_9 \mathbf{a}_1 - x_9 \mathbf{a}_2 - z_9 \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} - ax_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(4n) S I
$\mathbf{B}_{22}$	$=$	$-x_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 - z_9 \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} + ax_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(4n) S I
$\mathbf{B}_{23}$	$=$	$x_{10} \mathbf{a}_1 + x_{10} \mathbf{a}_2 + z_{10} \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{x}} + ax_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}}$	(4n) S II
$\mathbf{B}_{24}$	$=$	$-x_{10} \mathbf{a}_1 - x_{10} \mathbf{a}_2 + z_{10} \mathbf{a}_3$	$=$	$-ax_{10} \hat{\mathbf{x}} - ax_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}}$	(4n) S II
$\mathbf{B}_{25}$	$=$	$x_{10} \mathbf{a}_1 - x_{10} \mathbf{a}_2 - z_{10} \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{x}} - ax_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}}$	(4n) S II
$\mathbf{B}_{26}$	$=$	$-x_{10} \mathbf{a}_1 + x_{10} \mathbf{a}_2 - z_{10} \mathbf{a}_3$	$=$	$-ax_{10} \hat{\mathbf{x}} + ax_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}}$	(4n) S II

$$\begin{aligned}
\mathbf{B}_{27} &= x_{11} \mathbf{a}_1 + y_{11} \mathbf{a}_2 + z_{11} \mathbf{a}_3 &= ax_{11} \hat{\mathbf{x}} + ay_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} &(8o) &\text{S III} \\
\mathbf{B}_{28} &= -x_{11} \mathbf{a}_1 - y_{11} \mathbf{a}_2 + z_{11} \mathbf{a}_3 &= -ax_{11} \hat{\mathbf{x}} - ay_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} &(8o) &\text{S III} \\
\mathbf{B}_{29} &= y_{11} \mathbf{a}_1 - x_{11} \mathbf{a}_2 - z_{11} \mathbf{a}_3 &= ay_{11} \hat{\mathbf{x}} - ax_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} &(8o) &\text{S III} \\
\mathbf{B}_{30} &= -y_{11} \mathbf{a}_1 + x_{11} \mathbf{a}_2 - z_{11} \mathbf{a}_3 &= -ay_{11} \hat{\mathbf{x}} + ax_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} &(8o) &\text{S III} \\
\mathbf{B}_{31} &= -x_{11} \mathbf{a}_1 + y_{11} \mathbf{a}_2 - z_{11} \mathbf{a}_3 &= -ax_{11} \hat{\mathbf{x}} + ay_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} &(8o) &\text{S III} \\
\mathbf{B}_{32} &= x_{11} \mathbf{a}_1 - y_{11} \mathbf{a}_2 - z_{11} \mathbf{a}_3 &= ax_{11} \hat{\mathbf{x}} - ay_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} &(8o) &\text{S III} \\
\mathbf{B}_{33} &= -y_{11} \mathbf{a}_1 - x_{11} \mathbf{a}_2 + z_{11} \mathbf{a}_3 &= -ay_{11} \hat{\mathbf{x}} - ax_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} &(8o) &\text{S III} \\
\mathbf{B}_{34} &= y_{11} \mathbf{a}_1 + x_{11} \mathbf{a}_2 + z_{11} \mathbf{a}_3 &= ay_{11} \hat{\mathbf{x}} + ax_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} &(8o) &\text{S III}
\end{aligned}$$

References

- [1] S. R. Hall and J. F. Rowland, *The crystal structure of synthetic mooihoekite $\text{Cu}_9\text{Fe}_9\text{S}_{16}$* , Acta Crystallogr. Sect. B **29**, 2365–2372 (1973), doi:10.1107/S0567740873006710.

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First cited in

H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettel, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.