

Nb₆Sn₅ Structure:

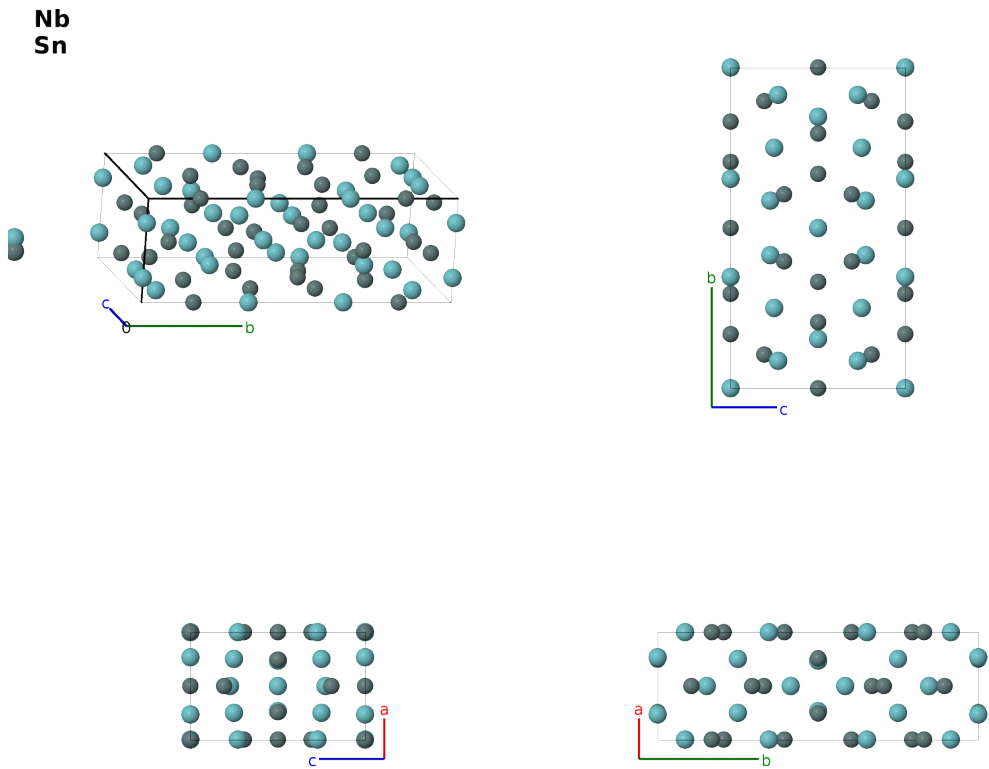
A6B5_oI44_71_egkl_fghl-001

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<https://aflow.org/prototype-encyclopedia/Q45R>

https://aflow.org/prototype-encyclopedia/A6B5_oI44_71_egkl_fghl-001



Prototype	Nb ₆ Sn ₅
AFLOW prototype label	A6B5_oI44_71_egkl_fghl-001
ICSD	105232
CCDC	1663122
Pearson symbol	oI44
Space group number	71
Space group symbol	<i>Immm</i>
AFLOW prototype command	<code>aflow --proto=A6B5_oI44_71_egkl_fghl-001</code> <code>--params=a, b/a, c/a, x₁, x₂, y₃, y₄, y₅, y₇, z₇, y₈, z₈</code>

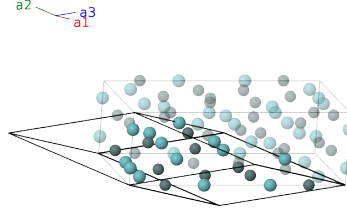
Other compounds with this structure

Ti₆Sn₅

- (Ogren, 1965) state that what we have labeled the Sn-II (4g) site is only occupied 92% of the time.
- (Villars, 2018) and others use Ti₆Sn₅ as the prototype for this structure. We follow (Pearson, 1967) and use Nb₆Sn₅ as the prototype.

Body-centered Orthorhombic primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}}$	(4e)	Nb I
$\mathbf{B}_2$	$= -x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}}$	(4e)	Nb I
$\mathbf{B}_3$	$= \frac{1}{2} \mathbf{a}_1 + x_2 \mathbf{a}_2 + \left(x_2 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}}$	(4f)	Sn I
$\mathbf{B}_4$	$= \frac{1}{2} \mathbf{a}_1 - x_2 \mathbf{a}_2 - \left(x_2 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}}$	(4f)	Sn I
$\mathbf{B}_5$	$= y_3 \mathbf{a}_1 + y_3 \mathbf{a}_3$	$=$	$by_3 \hat{\mathbf{y}}$	(4g)	Nb II
$\mathbf{B}_6$	$= -y_3 \mathbf{a}_1 - y_3 \mathbf{a}_3$	$=$	$-by_3 \hat{\mathbf{y}}$	(4g)	Nb II
$\mathbf{B}_7$	$= y_4 \mathbf{a}_1 + y_4 \mathbf{a}_3$	$=$	$by_4 \hat{\mathbf{y}}$	(4g)	Sn II
$\mathbf{B}_8$	$= -y_4 \mathbf{a}_1 - y_4 \mathbf{a}_3$	$=$	$-by_4 \hat{\mathbf{y}}$	(4g)	Sn II
$\mathbf{B}_9$	$= \left(y_5 + \frac{1}{2}\right) \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + y_5 \mathbf{a}_3$	$=$	$by_5 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4h)	Sn III
$\mathbf{B}_{10}$	$= -\left(y_5 - \frac{1}{2}\right) \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - y_5 \mathbf{a}_3$	$=$	$-by_5 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4h)	Sn III
$\mathbf{B}_{11}$	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8k)	Nb III
$\mathbf{B}_{12}$	$= \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} - \frac{1}{4}c \hat{\mathbf{z}}$	(8k)	Nb III
$\mathbf{B}_{13}$	$= \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - \frac{1}{4}b \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8k)	Nb III
$\mathbf{B}_{14}$	$= \frac{1}{2} \mathbf{a}_1$	$=$	$-\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8k)	Nb III
$\mathbf{B}_{15}$	$= (y_7 + z_7) \mathbf{a}_1 + z_7 \mathbf{a}_2 + y_7 \mathbf{a}_3$	$=$	$by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(8l)	Nb IV
$\mathbf{B}_{16}$	$= -(y_7 - z_7) \mathbf{a}_1 + z_7 \mathbf{a}_2 - y_7 \mathbf{a}_3$	$=$	$-by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(8l)	Nb IV
$\mathbf{B}_{17}$	$= (y_7 - z_7) \mathbf{a}_1 - z_7 \mathbf{a}_2 + y_7 \mathbf{a}_3$	$=$	$by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(8l)	Nb IV
$\mathbf{B}_{18}$	$= -(y_7 + z_7) \mathbf{a}_1 - z_7 \mathbf{a}_2 - y_7 \mathbf{a}_3$	$=$	$-by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(8l)	Nb IV
$\mathbf{B}_{19}$	$= (y_8 + z_8) \mathbf{a}_1 + z_8 \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(8l)	Sn IV
$\mathbf{B}_{20}$	$= -(y_8 - z_8) \mathbf{a}_1 + z_8 \mathbf{a}_2 - y_8 \mathbf{a}_3$	$=$	$-by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(8l)	Sn IV
$\mathbf{B}_{21}$	$= (y_8 - z_8) \mathbf{a}_1 - z_8 \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(8l)	Sn IV

$$\mathbf{B}_{22} = -(y_8 + z_8) \mathbf{a}_1 - z_8 \mathbf{a}_2 - y_8 \mathbf{a}_3 = -by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} \quad (81) \quad \text{Sn IV}$$

References

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Found in

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