

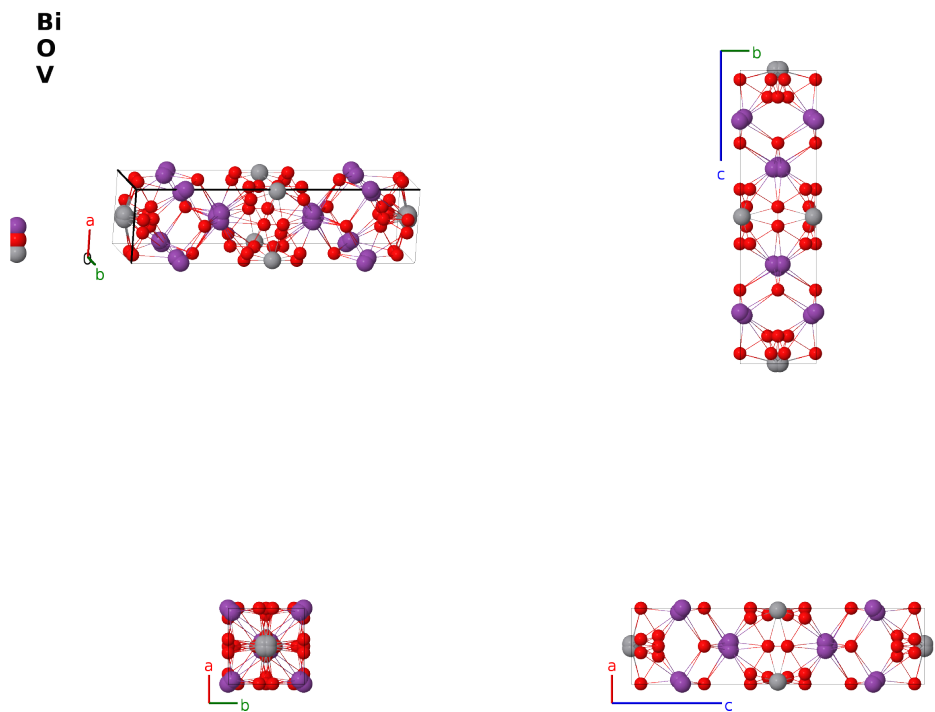
γ -Bi₄V₂O₁₁ Structure: A5B9C2_tI64_139_em_d2n_h-001

Cite this page as:

- H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettl, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.
- D. Hicks, M. J. Mehl, M. Esters, C. Osos, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/0N6E>

https://aflow.org/prototype-encyclopedia/A5B9C2_tI64_139_em_d2n_h-001



Prototype	Bi ₄ O ₁₁ V ₂
AFLOW prototype label	A5B9C2_tI64_139_em_d2n_h-001
ICSD	98587
CCDC	1657851
Pearson symbol	tI64
Space group number	139
Space group symbol	<i>I4</i> / <i>mmm</i>
AFLOW prototype command	<code>aflow --proto=A5B9C2_tI64_139_em_d2n_h-001</code> <code>--params=a, c/a, z₂, x₃, x₄, z₄, y₅, z₅, y₆, z₆</code>

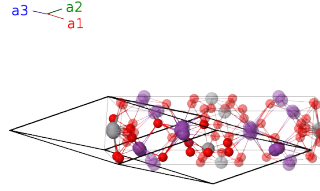
Other compounds with this structure

Bi₂WO₆

- There are three known varieties of Bi₄V₂O₁₁ (Villars, 2018):
 - α , the ground state structure, stable up to 450°C,
 - β , stable between 450°C and 555°C, and
 - γ , stable from 555°C up to the melting point at 880°C (this structure).
- The data for this structure was taken at 550°C.
- Most of the Wyckoff positions here are only partially occupied: Bi-I 50%, Bi-II 25%, O-II 23.8%, O-III 19.8%, and V 25%, giving a stoichiometry of Bi₄V₂O_{10.976}. This structure is also sometimes described as Bi₂VO_{5.5}.

Body-centered Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{3}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(4d)	O I
$\mathbf{B}_2$	$= \frac{1}{4}\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{4}c\hat{\mathbf{z}}$	(4d)	O I
$\mathbf{B}_3$	$= z_2\mathbf{a}_1 + z_2\mathbf{a}_2$	$=$	$cz_2\hat{\mathbf{z}}$	(4e)	Bi I
$\mathbf{B}_4$	$= -z_2\mathbf{a}_1 - z_2\mathbf{a}_2$	$=$	$-cz_2\hat{\mathbf{z}}$	(4e)	Bi I
$\mathbf{B}_5$	$= x_3\mathbf{a}_1 + x_3\mathbf{a}_2 + 2x_3\mathbf{a}_3$	$=$	$ax_3\hat{\mathbf{x}} + ax_3\hat{\mathbf{y}}$	(8h)	V I
$\mathbf{B}_6$	$= -x_3\mathbf{a}_1 - x_3\mathbf{a}_2 - 2x_3\mathbf{a}_3$	$=$	$-ax_3\hat{\mathbf{x}} - ax_3\hat{\mathbf{y}}$	(8h)	V I
$\mathbf{B}_7$	$= x_3\mathbf{a}_1 - x_3\mathbf{a}_2$	$=$	$-ax_3\hat{\mathbf{x}} + ax_3\hat{\mathbf{y}}$	(8h)	V I
$\mathbf{B}_8$	$= -x_3\mathbf{a}_1 + x_3\mathbf{a}_2$	$=$	$ax_3\hat{\mathbf{x}} - ax_3\hat{\mathbf{y}}$	(8h)	V I
$\mathbf{B}_9$	$= (x_4 + z_4)\mathbf{a}_1 + (x_4 + z_4)\mathbf{a}_2 + 2x_4\mathbf{a}_3$	$=$	$ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(16m)	Bi II
$\mathbf{B}_{10}$	$= -(x_4 - z_4)\mathbf{a}_1 - (x_4 - z_4)\mathbf{a}_2 - 2x_4\mathbf{a}_3$	$=$	$-ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(16m)	Bi II
$\mathbf{B}_{11}$	$= (x_4 + z_4)\mathbf{a}_1 - (x_4 - z_4)\mathbf{a}_2$	$=$	$-ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(16m)	Bi II
$\mathbf{B}_{12}$	$= -(x_4 - z_4)\mathbf{a}_1 + (x_4 + z_4)\mathbf{a}_2$	$=$	$ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(16m)	Bi II
$\mathbf{B}_{13}$	$= (x_4 - z_4)\mathbf{a}_1 - (x_4 + z_4)\mathbf{a}_2$	$=$	$-ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(16m)	Bi II
$\mathbf{B}_{14}$	$= -(x_4 + z_4)\mathbf{a}_1 + (x_4 - z_4)\mathbf{a}_2$	$=$	$ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(16m)	Bi II
$\mathbf{B}_{15}$	$= (x_4 - z_4)\mathbf{a}_1 + (x_4 - z_4)\mathbf{a}_2 + 2x_4\mathbf{a}_3$	$=$	$ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(16m)	Bi II

$\mathbf{B}_{16}$	$=$	$-(x_4 + z_4) \mathbf{a}_1 - (x_4 + z_4) \mathbf{a}_2 -$	$=$	$-ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(16m)	Bi II
		$2x_4 \mathbf{a}_3$				
$\mathbf{B}_{17}$	$=$	$(y_5 + z_5) \mathbf{a}_1 + z_5 \mathbf{a}_2 + y_5 \mathbf{a}_3$	$=$	$ay_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(16n)	O II
$\mathbf{B}_{18}$	$=$	$-(y_5 - z_5) \mathbf{a}_1 + z_5 \mathbf{a}_2 - y_5 \mathbf{a}_3$	$=$	$-ay_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(16n)	O II
$\mathbf{B}_{19}$	$=$	$z_5 \mathbf{a}_1 - (y_5 - z_5) \mathbf{a}_2 - y_5 \mathbf{a}_3$	$=$	$-ay_5 \hat{\mathbf{x}} + cz_5 \hat{\mathbf{z}}$	(16n)	O II
$\mathbf{B}_{20}$	$=$	$z_5 \mathbf{a}_1 + (y_5 + z_5) \mathbf{a}_2 + y_5 \mathbf{a}_3$	$=$	$ay_5 \hat{\mathbf{x}} + cz_5 \hat{\mathbf{z}}$	(16n)	O II
$\mathbf{B}_{21}$	$=$	$(y_5 - z_5) \mathbf{a}_1 - z_5 \mathbf{a}_2 + y_5 \mathbf{a}_3$	$=$	$ay_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(16n)	O II
$\mathbf{B}_{22}$	$=$	$-(y_5 + z_5) \mathbf{a}_1 - z_5 \mathbf{a}_2 - y_5 \mathbf{a}_3$	$=$	$-ay_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(16n)	O II
$\mathbf{B}_{23}$	$=$	$-z_5 \mathbf{a}_1 + (y_5 - z_5) \mathbf{a}_2 + y_5 \mathbf{a}_3$	$=$	$ay_5 \hat{\mathbf{x}} - cz_5 \hat{\mathbf{z}}$	(16n)	O II
$\mathbf{B}_{24}$	$=$	$-z_5 \mathbf{a}_1 - (y_5 + z_5) \mathbf{a}_2 - y_5 \mathbf{a}_3$	$=$	$-ay_5 \hat{\mathbf{x}} - cz_5 \hat{\mathbf{z}}$	(16n)	O II
$\mathbf{B}_{25}$	$=$	$(y_6 + z_6) \mathbf{a}_1 + z_6 \mathbf{a}_2 + y_6 \mathbf{a}_3$	$=$	$ay_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(16n)	O III
$\mathbf{B}_{26}$	$=$	$-(y_6 - z_6) \mathbf{a}_1 + z_6 \mathbf{a}_2 - y_6 \mathbf{a}_3$	$=$	$-ay_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(16n)	O III
$\mathbf{B}_{27}$	$=$	$z_6 \mathbf{a}_1 - (y_6 - z_6) \mathbf{a}_2 - y_6 \mathbf{a}_3$	$=$	$-ay_6 \hat{\mathbf{x}} + cz_6 \hat{\mathbf{z}}$	(16n)	O III
$\mathbf{B}_{28}$	$=$	$z_6 \mathbf{a}_1 + (y_6 + z_6) \mathbf{a}_2 + y_6 \mathbf{a}_3$	$=$	$ay_6 \hat{\mathbf{x}} + cz_6 \hat{\mathbf{z}}$	(16n)	O III
$\mathbf{B}_{29}$	$=$	$(y_6 - z_6) \mathbf{a}_1 - z_6 \mathbf{a}_2 + y_6 \mathbf{a}_3$	$=$	$ay_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(16n)	O III
$\mathbf{B}_{30}$	$=$	$-(y_6 + z_6) \mathbf{a}_1 - z_6 \mathbf{a}_2 - y_6 \mathbf{a}_3$	$=$	$-ay_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(16n)	O III
$\mathbf{B}_{31}$	$=$	$-z_6 \mathbf{a}_1 + (y_6 - z_6) \mathbf{a}_2 + y_6 \mathbf{a}_3$	$=$	$ay_6 \hat{\mathbf{x}} - cz_6 \hat{\mathbf{z}}$	(16n)	O III
$\mathbf{B}_{32}$	$=$	$-z_6 \mathbf{a}_1 - (y_6 + z_6) \mathbf{a}_2 - y_6 \mathbf{a}_3$	$=$	$-ay_6 \hat{\mathbf{x}} - cz_6 \hat{\mathbf{z}}$	(16n)	O III

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First cited in

H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettel, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.