

γ -brass (Cu_9Al_4 , $D8_3$) Structure: A4B9_cP52_215_ei_3efgi-001

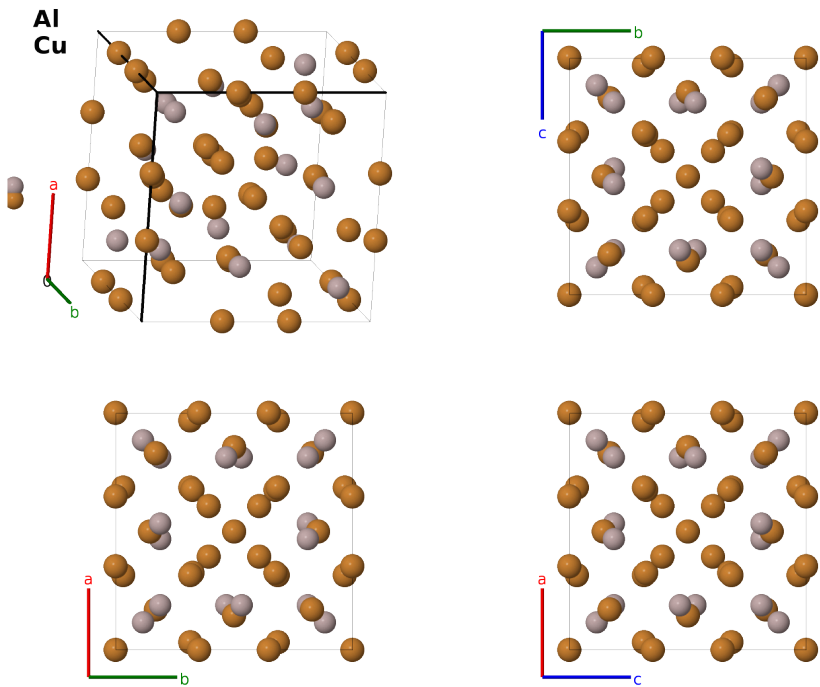
This structure previously used the label(s) **A4B9_cP52_215_ei_3efgi**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/TRNX>

https://aflow.org/prototype-encyclopedia/A4B9_cP52_215_ei_3efgi-001



Prototype	Al_4Cu_9
AFLOW prototype label	A4B9_cP52_215_ei_3efgi-001
<i>Strukturbericht</i> designation	$D8_3$
Mineral name	γ -brass
ICSD	1625
CCDC	1591705
Pearson symbol	cP52
Space group number	215
Space group symbol	$P\bar{4}3m$
AFLOW prototype command	<code>aflow --proto=A4B9_cP52_215_ei_3efgi-001</code> <code>--params=$a, x_1, x_2, x_3, x_4, x_5, x_6, x_7, z_7, x_8, z_8$</code>

Other compounds with this structure

Cu_9Ga_4 , InMn_3

- (Arnberg, 1978) give the Wyckoff positions of the Cu-IV and Cu-V atoms as (6g) $(x, 1/2, 1/2)$, but give the coordinates in the form $(x, 0, 0)$ corresponding to the (6f) site.
- (Stokhuyzen, 1974) used (6f) for both types of atoms in the isostructural system Ga_9Al_4 .
- (Pearson, 1958) places the Cu-IV atoms on a (6f) site and Cu-V on (6g), but does not give explicit coordinates.
- Placing the Cu-V atoms on (6f) sites yields an interatomic distance of $1.8\text{\AA}$. This contradicts (Arnberg, 1978), who say that the minimum interatomic distance between the Cu-IV and Cu-V atoms is $2.48\text{\AA}$. Placing the Cu-V atoms on (6g) sites gives this distance, in agreement with (Pearson, 1958), so we make this choice for the crystal structure.
- This is a variety of γ -brass comparable to the $D8_2$ structure. In fact, if we
 - Replace the Al and Cu-III atoms by Zn, while setting $x_4 = x_1 + 1/2$,
 - Replace the Al II and Cu-VI atoms by Zn, with $x_8 = x_7 + 1/2$ and $z_8 = z_7 + 1/2$,
 - Set $x_3 = x_2 + 1/2$ and
 - Set $x_6 = x_5 + 1/2$,

then this structure is identical to $D8_2$ γ -brass.

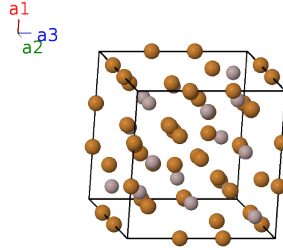
- (Pearson, 1958), pp. 252, gives a list of compounds which can take on the $D8_1$, $D8_2$, or $D8_3$ structure, depending on the exact composition.
 - (Mizutani, 2010) classifies this as a “P-cell” γ -brass.
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Simple Cubic primitive vectors

$$\mathbf{a}_1 = a \hat{\mathbf{x}}$$

$$\mathbf{a}_2 = a \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = a \hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}} + ax_1 \hat{\mathbf{y}} + ax_1 \hat{\mathbf{z}}$	(4e)	Al I
$\mathbf{B}_2$	$= -x_1 \mathbf{a}_1 - x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}} - ax_1 \hat{\mathbf{y}} + ax_1 \hat{\mathbf{z}}$	(4e)	Al I
$\mathbf{B}_3$	$= -x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}} + ax_1 \hat{\mathbf{y}} - ax_1 \hat{\mathbf{z}}$	(4e)	Al I
$\mathbf{B}_4$	$= x_1 \mathbf{a}_1 - x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}} - ax_1 \hat{\mathbf{y}} - ax_1 \hat{\mathbf{z}}$	(4e)	Al I
$\mathbf{B}_5$	$= x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(4e)	Cu I
$\mathbf{B}_6$	$= -x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(4e)	Cu I
$\mathbf{B}_7$	$= -x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(4e)	Cu I
$\mathbf{B}_8$	$= x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(4e)	Cu I

B_9	$=$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(4e)	Cu II
B_{10}	$=$	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(4e)	Cu II
B_{11}	$=$	$-x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(4e)	Cu II
B_{12}	$=$	$x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(4e)	Cu II
B_{13}	$=$	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(4e)	Cu III
B_{14}	$=$	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(4e)	Cu III
B_{15}	$=$	$-x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(4e)	Cu III
B_{16}	$=$	$x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(4e)	Cu III
B_{17}	$=$	$x_5 \mathbf{a}_1$	$=$	$ax_5 \hat{\mathbf{x}}$	(6f)	Cu IV
B_{18}	$=$	$-x_5 \mathbf{a}_1$	$=$	$-ax_5 \hat{\mathbf{x}}$	(6f)	Cu IV
B_{19}	$=$	$x_5 \mathbf{a}_2$	$=$	$ax_5 \hat{\mathbf{y}}$	(6f)	Cu IV
B_{20}	$=$	$-x_5 \mathbf{a}_2$	$=$	$-ax_5 \hat{\mathbf{y}}$	(6f)	Cu IV
B_{21}	$=$	$x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{z}}$	(6f)	Cu IV
B_{22}	$=$	$-x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{z}}$	(6f)	Cu IV
B_{23}	$=$	$x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Cu V
B_{24}	$=$	$-x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Cu V
B_{25}	$=$	$\frac{1}{2} \mathbf{a}_1 + x_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Cu V
B_{26}	$=$	$\frac{1}{2} \mathbf{a}_1 - x_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Cu V
B_{27}	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}}$	(6g)	Cu V
B_{28}	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - x_6 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}}$	(6g)	Cu V
B_{29}	$=$	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + az_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{30}	$=$	$-x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + az_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{31}	$=$	$-x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - az_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{32}	$=$	$x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - az_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{33}	$=$	$z_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$az_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{34}	$=$	$z_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$az_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{35}	$=$	$-z_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$-az_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{36}	$=$	$-z_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$-az_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{37}	$=$	$x_7 \mathbf{a}_1 + z_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + az_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{38}	$=$	$-x_7 \mathbf{a}_1 + z_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + az_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{39}	$=$	$x_7 \mathbf{a}_1 - z_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - az_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{40}	$=$	$-x_7 \mathbf{a}_1 - z_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - az_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Al II
B_{41}	$=$	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} + az_8 \hat{\mathbf{z}}$	(12i)	Cu VI
B_{42}	$=$	$-x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} + az_8 \hat{\mathbf{z}}$	(12i)	Cu VI
B_{43}	$=$	$-x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - az_8 \hat{\mathbf{z}}$	(12i)	Cu VI
B_{44}	$=$	$x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - az_8 \hat{\mathbf{z}}$	(12i)	Cu VI
B_{45}	$=$	$z_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$az_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
B_{46}	$=$	$z_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$az_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
B_{47}	$=$	$-z_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$-az_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
B_{48}	$=$	$-z_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$-az_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
B_{49}	$=$	$x_8 \mathbf{a}_1 + z_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + az_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI

$$\begin{aligned}
\mathbf{B}_{50} &= -x_8 \mathbf{a}_1 + z_8 \mathbf{a}_2 - x_8 \mathbf{a}_3 &= -ax_8 \hat{\mathbf{x}} + az_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}} & (12i) & \text{Cu VI} \\
\mathbf{B}_{51} &= x_8 \mathbf{a}_1 - z_8 \mathbf{a}_2 - x_8 \mathbf{a}_3 &= ax_8 \hat{\mathbf{x}} - az_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}} & (12i) & \text{Cu VI} \\
\mathbf{B}_{52} &= -x_8 \mathbf{a}_1 - z_8 \mathbf{a}_2 + x_8 \mathbf{a}_3 &= -ax_8 \hat{\mathbf{x}} - az_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}} & (12i) & \text{Cu VI}
\end{aligned}$$

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