

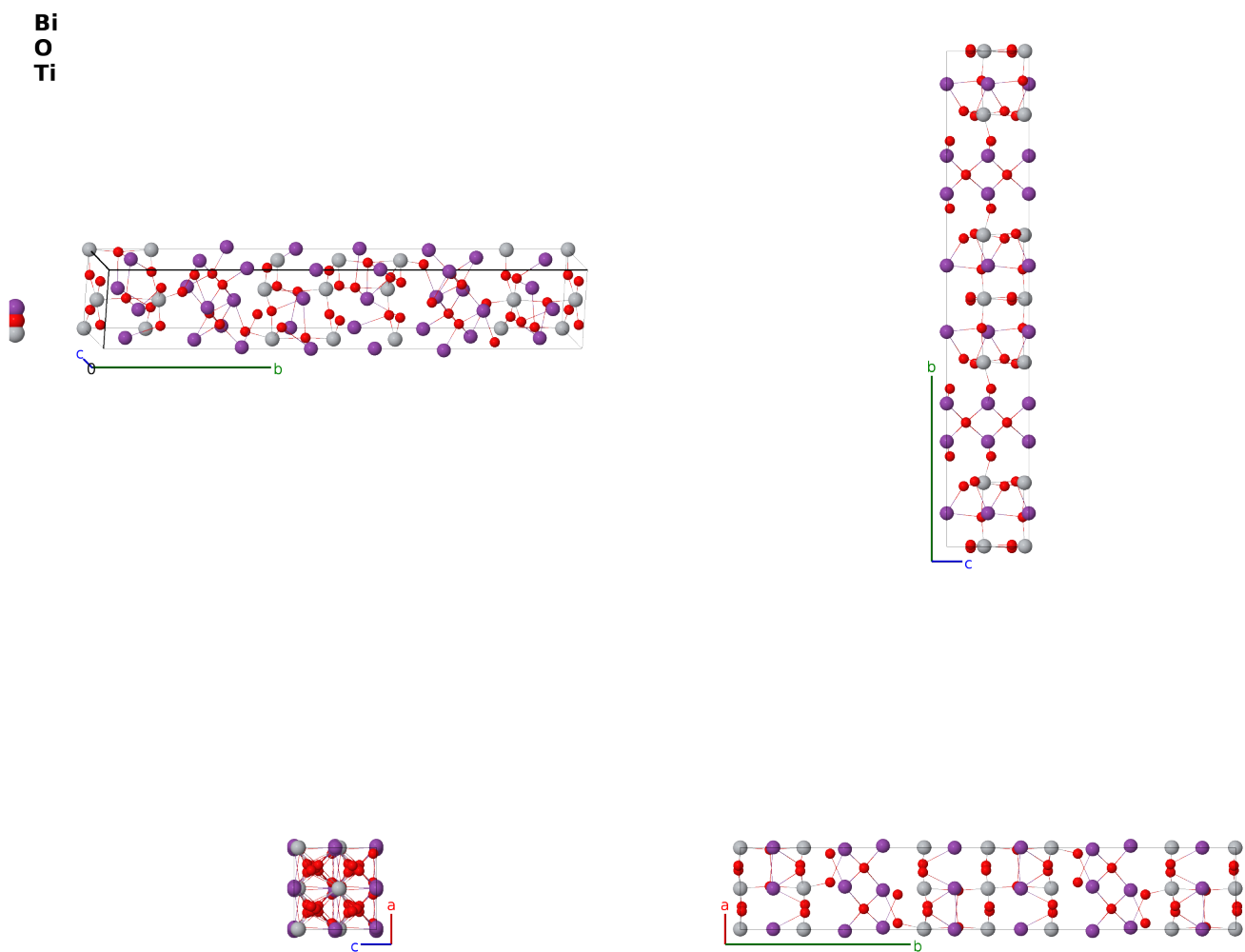
Orthorhombic $\text{Bi}_4\text{Ti}_3\text{O}_{12}$ $m = 3$ Aurivillius Structure (*Obsolete*): A4B12C3_oC76_41_2b_6b_ab-001

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<https://aflow.org/prototype-encyclopedia/5TXE>

https://aflow.org/prototype-encyclopedia/A4B12C3_oC76_41_2b_6b_ab-001



Prototype

$\text{Bi}_4\text{O}_{12}\text{Ti}_3$

AFLOW prototype label

A4B12C3_oC76_41_2b_6b_ab-001

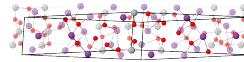
ICSD	16488
CCDC	1597063
Pearson symbol	oC76
Space group number	41
Space group symbol	<i>Aea</i> 2
AFLOW prototype command	aflow --proto=A4B12C3_oC76_41_2b_6b_ab-001 --params= <i>a, b/a, c/a, z₁, x₂, y₂, z₂, x₃, y₃, z₃, x₄, y₄, z₄, x₅, y₅, z₅, x₆, y₆, z₆, x₇, y₇, z₇, x₈, y₈, z₈, x₉, y₉, z₉, x₁₀, y₁₀, z₁₀</i>

- Aurivillius phases are layered tetragonal materials with composition $(\text{Me}'_2\text{O}_2)^{2+}(\text{Me}_{m-1}\text{R}_m\text{O}_{3m+1})^{2-}$ ($\text{Me}_{m-1}\text{Me}'_2\text{R}_m\text{O}_{3(m+1)}$), where Me and Me' are metals and R is a transition metal with a charge of +4 or +5. (Subbaro, 1962)
- (Dorrian, 1971) give this structure in what they call the *B2cb* (or *B2ab*) setting of space group #41. We used FINDSYM to transform this to the standard *Aba*2 setting.
- (Dorrian, 1971) notes that the physical properties of this structure indicate monoclinic symmetry, but that the structure is consistent with orthorhombic symmetry. Various authors have shown that the structure is actually in monoclinic, with space group *Pc* #7, as described by (Guo, 2019).

Base-centered Orthorhombic primitive vectors

$$\begin{aligned}
\mathbf{a}_1 &= a \hat{\mathbf{x}} \\
\mathbf{a}_2 &= \frac{1}{2}b \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}} \\
\mathbf{a}_3 &= \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}
\end{aligned}$$

$\mathbf{a}_1$
 $\mathbf{a}_2$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= -z_1 \mathbf{a}_2 + z_1 \mathbf{a}_3$	$=$	$cz_1 \hat{\mathbf{z}}$	(4a)	Ti I
$\mathbf{B}_2$	$= \frac{1}{2} \mathbf{a}_1 - (z_1 - \frac{1}{2}) \mathbf{a}_2 + (z_1 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(4a)	Ti I
$\mathbf{B}_3$	$= x_2 \mathbf{a}_1 + (y_2 - z_2) \mathbf{a}_2 + (y_2 + z_2) \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(8b)	Bi I
$\mathbf{B}_4$	$= -x_2 \mathbf{a}_1 - (y_2 + z_2) \mathbf{a}_2 - (y_2 - z_2) \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(8b)	Bi I
$\mathbf{B}_5$	$= (x_2 + \frac{1}{2}) \mathbf{a}_1 - (y_2 + z_2 - \frac{1}{2}) \mathbf{a}_2 + (-y_2 + z_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$a(x_2 + \frac{1}{2}) \hat{\mathbf{x}} - b(y_2 - \frac{1}{2}) \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(8b)	Bi I
$\mathbf{B}_6$	$= -(x_2 - \frac{1}{2}) \mathbf{a}_1 + (y_2 - z_2 + \frac{1}{2}) \mathbf{a}_2 + (y_2 + z_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_2 - \frac{1}{2}) \hat{\mathbf{x}} + b(y_2 + \frac{1}{2}) \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(8b)	Bi I
$\mathbf{B}_7$	$= x_3 \mathbf{a}_1 + (y_3 - z_3) \mathbf{a}_2 + (y_3 + z_3) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(8b)	Bi II

$$\begin{aligned}
\mathbf{B}_8 &= -x_3 \mathbf{a}_1 - (y_3 + z_3) \mathbf{a}_2 - (y_3 - z_3) \mathbf{a}_3 = -ax_3 \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}} & (8b) & \text{Bi II} \\
\mathbf{B}_9 &= (x_3 + \frac{1}{2}) \mathbf{a}_1 - (y_3 + z_3 - \frac{1}{2}) \mathbf{a}_2 + (-y_3 + z_3 + \frac{1}{2}) \mathbf{a}_3 = a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} - b(y_3 - \frac{1}{2}) \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}} & (8b) & \text{Bi II} \\
\mathbf{B}_{10} &= -(x_3 - \frac{1}{2}) \mathbf{a}_1 + (y_3 - z_3 + \frac{1}{2}) \mathbf{a}_2 + (y_3 + z_3 + \frac{1}{2}) \mathbf{a}_3 = -a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} + b(y_3 + \frac{1}{2}) \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}} & (8b) & \text{Bi II} \\
\mathbf{B}_{11} &= x_4 \mathbf{a}_1 + (y_4 - z_4) \mathbf{a}_2 + (y_4 + z_4) \mathbf{a}_3 = ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}} & (8b) & \text{O I} \\
\mathbf{B}_{12} &= -x_4 \mathbf{a}_1 - (y_4 + z_4) \mathbf{a}_2 - (y_4 - z_4) \mathbf{a}_3 = -ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}} & (8b) & \text{O I} \\
\mathbf{B}_{13} &= (x_4 + \frac{1}{2}) \mathbf{a}_1 - (y_4 + z_4 - \frac{1}{2}) \mathbf{a}_2 + (-y_4 + z_4 + \frac{1}{2}) \mathbf{a}_3 = a(x_4 + \frac{1}{2}) \hat{\mathbf{x}} - b(y_4 - \frac{1}{2}) \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}} & (8b) & \text{O I} \\
\mathbf{B}_{14} &= -(x_4 - \frac{1}{2}) \mathbf{a}_1 + (y_4 - z_4 + \frac{1}{2}) \mathbf{a}_2 + (y_4 + z_4 + \frac{1}{2}) \mathbf{a}_3 = -a(x_4 - \frac{1}{2}) \hat{\mathbf{x}} + b(y_4 + \frac{1}{2}) \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}} & (8b) & \text{O I} \\
\mathbf{B}_{15} &= x_5 \mathbf{a}_1 + (y_5 - z_5) \mathbf{a}_2 + (y_5 + z_5) \mathbf{a}_3 = ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} & (8b) & \text{O II} \\
\mathbf{B}_{16} &= -x_5 \mathbf{a}_1 - (y_5 + z_5) \mathbf{a}_2 - (y_5 - z_5) \mathbf{a}_3 = -ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} & (8b) & \text{O II} \\
\mathbf{B}_{17} &= (x_5 + \frac{1}{2}) \mathbf{a}_1 - (y_5 + z_5 - \frac{1}{2}) \mathbf{a}_2 + (-y_5 + z_5 + \frac{1}{2}) \mathbf{a}_3 = a(x_5 + \frac{1}{2}) \hat{\mathbf{x}} - b(y_5 - \frac{1}{2}) \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} & (8b) & \text{O II} \\
\mathbf{B}_{18} &= -(x_5 - \frac{1}{2}) \mathbf{a}_1 + (y_5 - z_5 + \frac{1}{2}) \mathbf{a}_2 + (y_5 + z_5 + \frac{1}{2}) \mathbf{a}_3 = -a(x_5 - \frac{1}{2}) \hat{\mathbf{x}} + b(y_5 + \frac{1}{2}) \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} & (8b) & \text{O II} \\
\mathbf{B}_{19} &= x_6 \mathbf{a}_1 + (y_6 - z_6) \mathbf{a}_2 + (y_6 + z_6) \mathbf{a}_3 = ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (8b) & \text{O III} \\
\mathbf{B}_{20} &= -x_6 \mathbf{a}_1 - (y_6 + z_6) \mathbf{a}_2 - (y_6 - z_6) \mathbf{a}_3 = -ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (8b) & \text{O III} \\
\mathbf{B}_{21} &= (x_6 + \frac{1}{2}) \mathbf{a}_1 - (y_6 + z_6 - \frac{1}{2}) \mathbf{a}_2 + (-y_6 + z_6 + \frac{1}{2}) \mathbf{a}_3 = a(x_6 + \frac{1}{2}) \hat{\mathbf{x}} - b(y_6 - \frac{1}{2}) \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (8b) & \text{O III} \\
\mathbf{B}_{22} &= -(x_6 - \frac{1}{2}) \mathbf{a}_1 + (y_6 - z_6 + \frac{1}{2}) \mathbf{a}_2 + (y_6 + z_6 + \frac{1}{2}) \mathbf{a}_3 = -a(x_6 - \frac{1}{2}) \hat{\mathbf{x}} + b(y_6 + \frac{1}{2}) \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (8b) & \text{O III} \\
\mathbf{B}_{23} &= x_7 \mathbf{a}_1 + (y_7 - z_7) \mathbf{a}_2 + (y_7 + z_7) \mathbf{a}_3 = ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (8b) & \text{O IV} \\
\mathbf{B}_{24} &= -x_7 \mathbf{a}_1 - (y_7 + z_7) \mathbf{a}_2 - (y_7 - z_7) \mathbf{a}_3 = -ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (8b) & \text{O IV} \\
\mathbf{B}_{25} &= (x_7 + \frac{1}{2}) \mathbf{a}_1 - (y_7 + z_7 - \frac{1}{2}) \mathbf{a}_2 + (-y_7 + z_7 + \frac{1}{2}) \mathbf{a}_3 = a(x_7 + \frac{1}{2}) \hat{\mathbf{x}} - b(y_7 - \frac{1}{2}) \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (8b) & \text{O IV} \\
\mathbf{B}_{26} &= -(x_7 - \frac{1}{2}) \mathbf{a}_1 + (y_7 - z_7 + \frac{1}{2}) \mathbf{a}_2 + (y_7 + z_7 + \frac{1}{2}) \mathbf{a}_3 = -a(x_7 - \frac{1}{2}) \hat{\mathbf{x}} + b(y_7 + \frac{1}{2}) \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (8b) & \text{O IV} \\
\mathbf{B}_{27} &= x_8 \mathbf{a}_1 + (y_8 - z_8) \mathbf{a}_2 + (y_8 + z_8) \mathbf{a}_3 = ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (8b) & \text{O V} \\
\mathbf{B}_{28} &= -x_8 \mathbf{a}_1 - (y_8 + z_8) \mathbf{a}_2 - (y_8 - z_8) \mathbf{a}_3 = -ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (8b) & \text{O V} \\
\mathbf{B}_{29} &= (x_8 + \frac{1}{2}) \mathbf{a}_1 - (y_8 + z_8 - \frac{1}{2}) \mathbf{a}_2 + (-y_8 + z_8 + \frac{1}{2}) \mathbf{a}_3 = a(x_8 + \frac{1}{2}) \hat{\mathbf{x}} - b(y_8 - \frac{1}{2}) \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (8b) & \text{O V} \\
\mathbf{B}_{30} &= -(x_8 - \frac{1}{2}) \mathbf{a}_1 + (y_8 - z_8 + \frac{1}{2}) \mathbf{a}_2 + (y_8 + z_8 + \frac{1}{2}) \mathbf{a}_3 = -a(x_8 - \frac{1}{2}) \hat{\mathbf{x}} + b(y_8 + \frac{1}{2}) \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (8b) & \text{O V}
\end{aligned}$$

$$\begin{aligned}
\mathbf{B}_{31} &= x_9 \mathbf{a}_1 + (y_9 - z_9) \mathbf{a}_2 + (y_9 + z_9) \mathbf{a}_3 = ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (8b) & \quad \text{O VI} \\
\mathbf{B}_{32} &= -x_9 \mathbf{a}_1 - (y_9 + z_9) \mathbf{a}_2 - (y_9 - z_9) \mathbf{a}_3 = -ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (8b) & \quad \text{O VI} \\
\mathbf{B}_{33} &= (x_9 + \frac{1}{2}) \mathbf{a}_1 - (y_9 + z_9 - \frac{1}{2}) \mathbf{a}_2 + (-y_9 + z_9 + \frac{1}{2}) \mathbf{a}_3 = a(x_9 + \frac{1}{2}) \hat{\mathbf{x}} - b(y_9 - \frac{1}{2}) \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (8b) & \quad \text{O VI} \\
\mathbf{B}_{34} &= -(x_9 - \frac{1}{2}) \mathbf{a}_1 + (y_9 - z_9 + \frac{1}{2}) \mathbf{a}_2 + (y_9 + z_9 + \frac{1}{2}) \mathbf{a}_3 = -a(x_9 - \frac{1}{2}) \hat{\mathbf{x}} + b(y_9 + \frac{1}{2}) \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (8b) & \quad \text{O VI} \\
\mathbf{B}_{35} &= x_{10} \mathbf{a}_1 + (y_{10} - z_{10}) \mathbf{a}_2 + (y_{10} + z_{10}) \mathbf{a}_3 = ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (8b) & \quad \text{Ti II} \\
\mathbf{B}_{36} &= -x_{10} \mathbf{a}_1 - (y_{10} + z_{10}) \mathbf{a}_2 - (y_{10} - z_{10}) \mathbf{a}_3 = -ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (8b) & \quad \text{Ti II} \\
\mathbf{B}_{37} &= (x_{10} + \frac{1}{2}) \mathbf{a}_1 - (y_{10} + z_{10} - \frac{1}{2}) \mathbf{a}_2 + (-y_{10} + z_{10} + \frac{1}{2}) \mathbf{a}_3 = a(x_{10} + \frac{1}{2}) \hat{\mathbf{x}} - b(y_{10} - \frac{1}{2}) \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (8b) & \quad \text{Ti II} \\
\mathbf{B}_{38} &= -(x_{10} - \frac{1}{2}) \mathbf{a}_1 + (y_{10} - z_{10} + \frac{1}{2}) \mathbf{a}_2 + (y_{10} + z_{10} + \frac{1}{2}) \mathbf{a}_3 = -a(x_{10} - \frac{1}{2}) \hat{\mathbf{x}} + b(y_{10} + \frac{1}{2}) \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (8b) & \quad \text{Ti II}
\end{aligned}$$

References

- [1] J. F. Dorrian, R. E. Newnham, D. K. Smith, and M. I. Kay, *Crystal Structure of $\text{Bi}_4\text{Ti}_3\text{O}_{12}$* , *Ferroelectrics* **3**, 17–27 (1972), doi:10.1080/00150197108237680.
- [2] E. C. Subbarao, *A family of ferroelectric bismuth compounds*, *J. Phys.: Conf. Ser.* **23**, 665–676 (1962), doi:10.1016/0022-3697(62)90526-7.
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