

# $\alpha$ -WO<sub>3</sub> Structure:

## A3B\_tP16\_130\_cf\_c-001

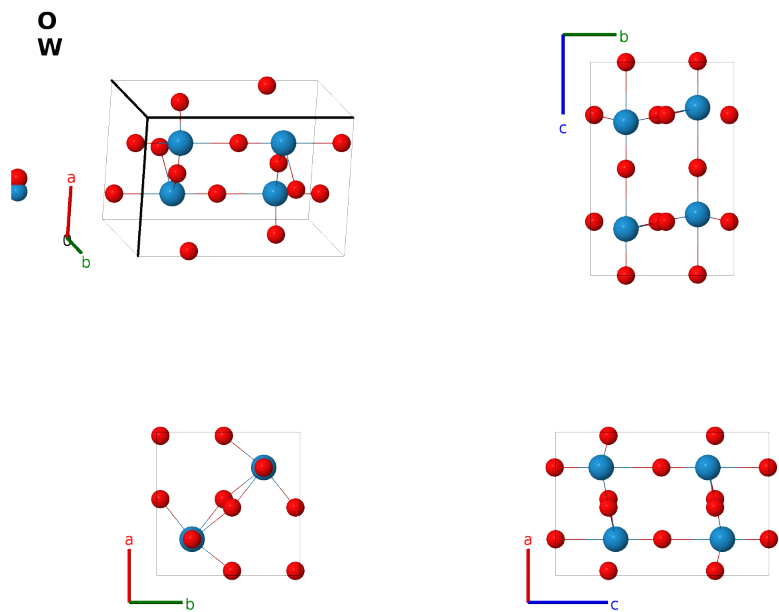
This structure previously used the label(s) **A3B\_tP16\_130\_cf\_c**. Calls to these addresses will be redirected here.

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|                         |                                                                                                                               |
|-------------------------|-------------------------------------------------------------------------------------------------------------------------------|
| Prototype               | O <sub>3</sub> W                                                                                                              |
| AFLOW prototype label   | A3B_tP16_130_cf_c-001                                                                                                         |
| ICSD                    | 50732                                                                                                                         |
| CCDC                    | 1615636                                                                                                                       |
| Pearson symbol          | tP16                                                                                                                          |
| Space group number      | 130                                                                                                                           |
| Space group symbol      | <i>P4/ncc</i>                                                                                                                 |
| AFLOW prototype command | <code>aflow --proto=A3B_tP16_130_cf_c-001</code><br><code>--params=a, c/a, z<sub>1</sub>, z<sub>2</sub>, x<sub>3</sub></code> |

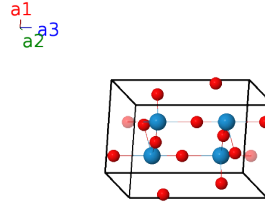
- All stable phases of WO<sub>3</sub> are distortions of the cubic  $\alpha$ -ReO<sub>3</sub> (*D*<sub>0</sub><sub>9</sub>) phase. Based on (Woodward, 1997 and Vogt, 1999), the known stable phases and their approximate temperature ranges are:

- $\alpha$ -WO<sub>3</sub> (1010-1170 K) (Vogt, 1999) (this structure)
- $\beta$ -WO<sub>3</sub> (600-1170 K) (Vogt, 1999)
- $\gamma$ -WO<sub>3</sub> (290-600 K) (Vogt, 1999)
- $\delta$ -WO<sub>3</sub> (230-290 K) (Diehl, 1978)
- $\epsilon$ -WO<sub>3</sub> (below 23 K) (Woodward, 1997)
- Woodward notes that “The transition temperatures display large hysteresis effects and universal agreement is not found in the literature.”
- In addition, several other structures have been proposed and/or found:
  - The original  $D0_{10}$  structure (Bräkken, 1931; Hermann, 1937), superseded by  $\delta$ -WO<sub>3</sub>
  - The original  $\beta$ -WO<sub>3</sub> (Salje, 1977),
  - Hexagonal WO<sub>3</sub>, presumably metastable, found by (Gerand, 1979) while dehydrating WO<sub>3</sub>·H<sub>2</sub>O.
- We use the  $\alpha$ -WO<sub>3</sub> data taken by (Vogt, 1999) at 800°C (1073K).
- (Kehl, 1952) originally put this structure in space group  $P4/nmm$  #129, with a  $c$ -lattice constant set to half of the current value. This structure was corrected by (Vogh, 1999).

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### Simple Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$




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### Basis vectors

|                   | Lattice coordinates                                                                                  |     | Cartesian coordinates                                                                                            | Wyckoff position | Atom type |
|-------------------|------------------------------------------------------------------------------------------------------|-----|------------------------------------------------------------------------------------------------------------------|------------------|-----------|
| $\mathbf{B}_1$    | $= \frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_1 \mathbf{a}_3$                           | $=$ | $\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$                          | (4c)             | O I       |
| $\mathbf{B}_2$    | $= \frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - (z_1 - \frac{1}{2}) \mathbf{a}_3$           | $=$ | $\frac{3}{4}a \hat{\mathbf{x}} + \frac{3}{4}a \hat{\mathbf{y}} - c(z_1 - \frac{1}{2}) \hat{\mathbf{z}}$          | (4c)             | O I       |
| $\mathbf{B}_3$    | $= \frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_1 \mathbf{a}_3$                           | $=$ | $\frac{3}{4}a \hat{\mathbf{x}} + \frac{3}{4}a \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$                          | (4c)             | O I       |
| $\mathbf{B}_4$    | $= \frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + (z_1 + \frac{1}{2}) \mathbf{a}_3$           | $=$ | $\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + c(z_1 + \frac{1}{2}) \hat{\mathbf{z}}$          | (4c)             | O I       |
| $\mathbf{B}_5$    | $= \frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_2 \mathbf{a}_3$                           | $=$ | $\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$                          | (4c)             | W I       |
| $\mathbf{B}_6$    | $= \frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - (z_2 - \frac{1}{2}) \mathbf{a}_3$           | $=$ | $\frac{3}{4}a \hat{\mathbf{x}} + \frac{3}{4}a \hat{\mathbf{y}} - c(z_2 - \frac{1}{2}) \hat{\mathbf{z}}$          | (4c)             | W I       |
| $\mathbf{B}_7$    | $= \frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_2 \mathbf{a}_3$                           | $=$ | $\frac{3}{4}a \hat{\mathbf{x}} + \frac{3}{4}a \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}}$                          | (4c)             | W I       |
| $\mathbf{B}_8$    | $= \frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$           | $=$ | $\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + c(z_2 + \frac{1}{2}) \hat{\mathbf{z}}$          | (4c)             | W I       |
| $\mathbf{B}_9$    | $= x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$                                   | $=$ | $ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$                                  | (8f)             | O II      |
| $\mathbf{B}_{10}$ | $= - (x_3 - \frac{1}{2}) \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$ | $=$ | $-a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$ | (8f)             | O II      |
| $\mathbf{B}_{11}$ | $= (x_3 + \frac{1}{2}) \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$                   | $=$ | $a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$                  | (8f)             | O II      |
| $\mathbf{B}_{12}$ | $= -x_3 \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$                  | $=$ | $-ax_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$                 | (8f)             | O II      |
| $\mathbf{B}_{13}$ | $= -x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$                                  | $=$ | $-ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + \frac{3}{4}c \hat{\mathbf{z}}$                                 | (8f)             | O II      |

$$\begin{aligned}
\mathbf{B}_{14} &= \left(x_3 + \frac{1}{2}\right) \mathbf{a}_1 - \left(x_3 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 = a \left(x_3 + \frac{1}{2}\right) \hat{\mathbf{x}} - a \left(x_3 - \frac{1}{2}\right) \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}} & (8f) & \quad \text{O II} \\
\mathbf{B}_{15} &= -\left(x_3 - \frac{1}{2}\right) \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 = -a \left(x_3 - \frac{1}{2}\right) \hat{\mathbf{x}} - a x_3 \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}} & (8f) & \quad \text{O II} \\
\mathbf{B}_{16} &= x_3 \mathbf{a}_1 + \left(x_3 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 = a x_3 \hat{\mathbf{x}} + a \left(x_3 + \frac{1}{2}\right) \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}} & (8f) & \quad \text{O II}
\end{aligned}$$

## References

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