

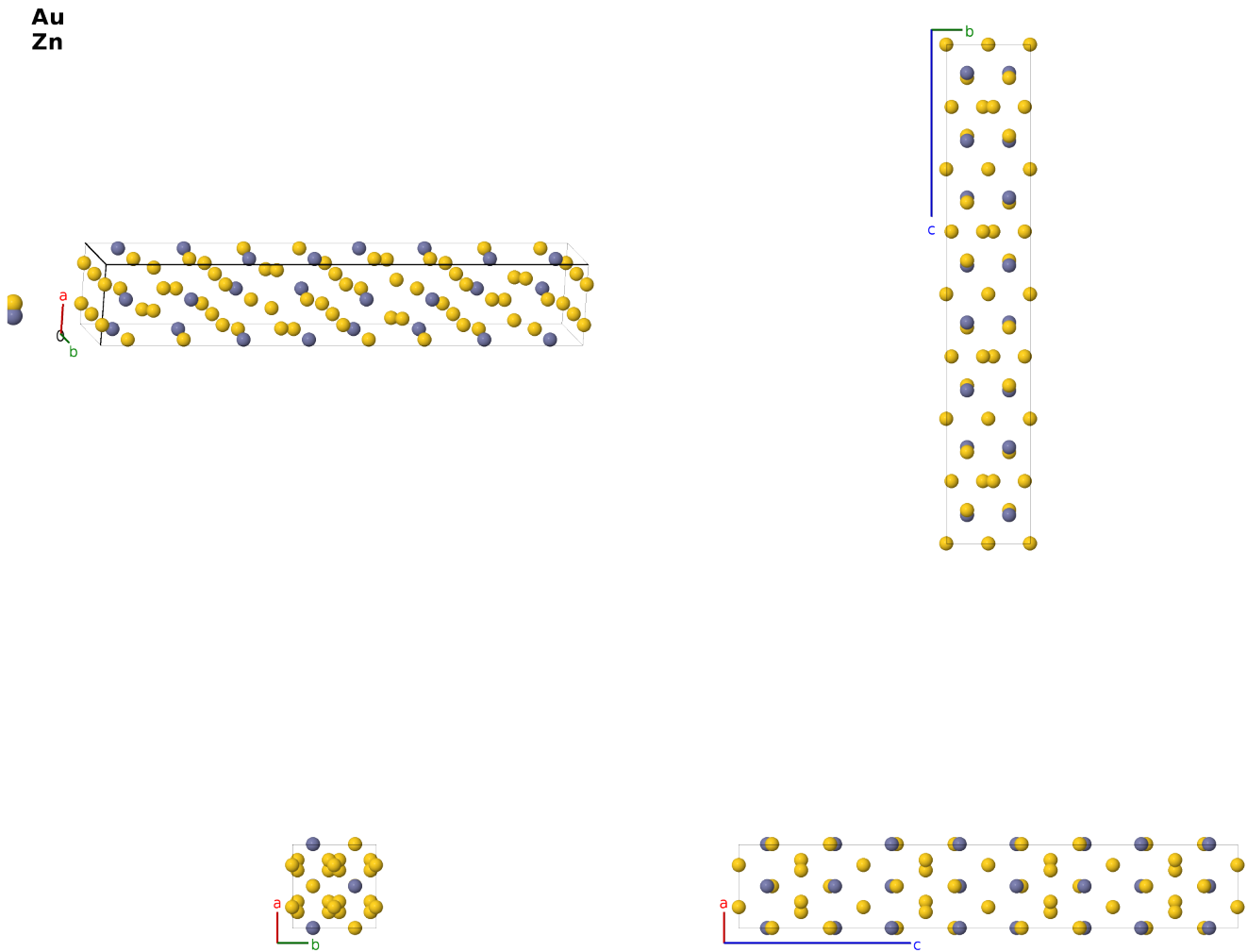
R₁ Au₃Zn Structure: A3B_tI64_142_def_d-001

Cite this page as:

- H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettel, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.
- D. Hicks, M. J. Mehl, M. Esters, C. Osos, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/Q6FW>

https://aflow.org/prototype-encyclopedia/A3B_tI64_142_def_d-001



Prototype

Au₃Zn

AFLOW prototype label

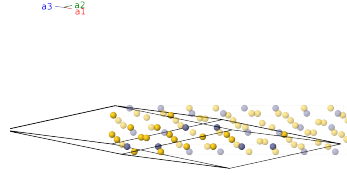
A3B_tI64_142_def_d-001

ICSD	58628
CCDC	1622634
Pearson symbol	tI64
Space group number	142
Space group symbol	$I4_1/acd$
AFLOW prototype command	<code>aflow --proto=A3B_tI64_142_def_d-001</code> <code>--params=a, c/a, z₁, z₂, x₃, x₄</code>

- Au_3Zn is known to exist in three forms, depending upon the exact composition and temperature (Hisatsune, 1998):
 - The tetragonal R_1 phase (this structure) is stable below $\approx 475\text{K}$ with a composition very nearly stoichiometric.
 - The orthorhombic R_2 phase is stable below $\approx 550\text{K}$ with a composition range somewhat wider than the R_1 phase.
 - The tetragonal H phase has the $D0_{23}$ structure and is stable at temperatures up to $\approx 700\text{K}$ over a considerably wider range of stoichiometries than either the R_1 or R_2 phases.
- (Iwaskai, 1962) gave structure of the R_1 phase in setting 1 of space group $I4_1/acd$ #142. We used FINDSYM to transform this to the standard setting 2.
- (Iwaskai, 1962) gave the lattice constants in kX units. We used the conversion factor $1 \text{ kX} = 1.00202\text{\AA}$. (Wood, 1947)

Body-centered Tetragonal primitive vectors

$$\begin{aligned}
 \mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\
 \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\
 \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}
 \end{aligned}$$



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= (z_1 + \frac{1}{4}) \mathbf{a}_1 + z_1 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$= \frac{1}{4}a \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_2$	$= z_1 \mathbf{a}_1 + (z_1 + \frac{1}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + c(z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_3$	$= -(z_1 - \frac{1}{4}) \mathbf{a}_1 - (z_1 - \frac{1}{2}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_4$	$= -(z_1 - \frac{1}{2}) \mathbf{a}_1 - (z_1 - \frac{1}{4}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$= \frac{1}{4}a \hat{\mathbf{y}} - c(z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_5$	$= -(z_1 - \frac{3}{4}) \mathbf{a}_1 - z_1 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$= \frac{3}{4}a \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_6$	$= -z_1 \mathbf{a}_1 - (z_1 - \frac{3}{4}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{4}a \hat{\mathbf{y}} - c(z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_7$	$= (z_1 + \frac{3}{4}) \mathbf{a}_1 + (z_1 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$= \frac{1}{4}a \hat{\mathbf{y}} + c(z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_8$	$= (z_1 + \frac{1}{2}) \mathbf{a}_1 + (z_1 + \frac{3}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + c(z_1 + \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_9$	$= (z_2 + \frac{1}{4}) \mathbf{a}_1 + z_2 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$= \frac{1}{4}a \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(16d)	Zn I

$$\begin{aligned}
\mathbf{B}_{10} &= z_2 \mathbf{a}_1 + \left(z_2 + \frac{1}{4}\right) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 = \frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} + c \left(z_2 - \frac{1}{4}\right) \hat{\mathbf{z}} & (16d) & \text{Zn I} \\
\mathbf{B}_{11} &= -\left(z_2 - \frac{1}{4}\right) \mathbf{a}_1 - \left(z_2 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 = \frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} - c z_2 \hat{\mathbf{z}} & (16d) & \text{Zn I} \\
\mathbf{B}_{12} &= -\left(z_2 - \frac{1}{2}\right) \mathbf{a}_1 - \left(z_2 - \frac{1}{4}\right) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3 = \frac{1}{4} a \hat{\mathbf{y}} - c \left(z_2 - \frac{1}{4}\right) \hat{\mathbf{z}} & (16d) & \text{Zn I} \\
\mathbf{B}_{13} &= -\left(z_2 - \frac{3}{4}\right) \mathbf{a}_1 - z_2 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 = \frac{3}{4} a \hat{\mathbf{y}} - c z_2 \hat{\mathbf{z}} & (16d) & \text{Zn I} \\
\mathbf{B}_{14} &= -z_2 \mathbf{a}_1 - \left(z_2 - \frac{3}{4}\right) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3 = \frac{1}{2} a \hat{\mathbf{x}} - \frac{1}{4} a \hat{\mathbf{y}} - c \left(z_2 - \frac{1}{4}\right) \hat{\mathbf{z}} & (16d) & \text{Zn I} \\
\mathbf{B}_{15} &= \left(z_2 + \frac{3}{4}\right) \mathbf{a}_1 + \left(z_2 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3 = \frac{1}{4} a \hat{\mathbf{y}} + c \left(z_2 + \frac{1}{2}\right) \hat{\mathbf{z}} & (16d) & \text{Zn I} \\
\mathbf{B}_{16} &= \left(z_2 + \frac{1}{2}\right) \mathbf{a}_1 + \left(z_2 + \frac{3}{4}\right) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 = \frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} + c \left(z_2 + \frac{1}{4}\right) \hat{\mathbf{z}} & (16d) & \text{Zn I} \\
\mathbf{B}_{17} &= \frac{1}{4} \mathbf{a}_1 + \left(x_3 + \frac{1}{4}\right) \mathbf{a}_2 + x_3 \mathbf{a}_3 = a x_3 \hat{\mathbf{x}} + \frac{1}{4} c \hat{\mathbf{z}} & (16e) & \text{Au II} \\
\mathbf{B}_{18} &= \frac{3}{4} \mathbf{a}_1 - \left(x_3 - \frac{1}{4}\right) \mathbf{a}_2 - \left(x_3 - \frac{1}{2}\right) \mathbf{a}_3 = -a x_3 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}} & (16e) & \text{Au II} \\
\mathbf{B}_{19} &= \left(x_3 + \frac{1}{4}\right) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + x_3 \mathbf{a}_3 = \frac{1}{4} a \hat{\mathbf{x}} + a \left(x_3 - \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}} & (16e) & \text{Au II} \\
\mathbf{B}_{20} &= -\left(x_3 - \frac{1}{4}\right) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - \left(x_3 - \frac{1}{2}\right) \mathbf{a}_3 = \frac{1}{4} a \hat{\mathbf{x}} - a \left(x_3 - \frac{1}{4}\right) \hat{\mathbf{y}} & (16e) & \text{Au II} \\
\mathbf{B}_{21} &= \frac{3}{4} \mathbf{a}_1 - \left(x_3 - \frac{3}{4}\right) \mathbf{a}_2 - x_3 \mathbf{a}_3 = -a x_3 \hat{\mathbf{x}} + \frac{3}{4} c \hat{\mathbf{z}} & (16e) & \text{Au II} \\
\mathbf{B}_{22} &= \frac{1}{4} \mathbf{a}_1 + \left(x_3 + \frac{3}{4}\right) \mathbf{a}_2 + \left(x_3 + \frac{1}{2}\right) \mathbf{a}_3 = a \left(x_3 + \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{4} c \hat{\mathbf{z}} & (16e) & \text{Au II} \\
\mathbf{B}_{23} &= -\left(x_3 - \frac{3}{4}\right) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - x_3 \mathbf{a}_3 = -\frac{1}{4} a \hat{\mathbf{x}} - a \left(x_3 - \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}} & (16e) & \text{Au II} \\
\mathbf{B}_{24} &= \left(x_3 + \frac{3}{4}\right) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + \left(x_3 + \frac{1}{2}\right) \mathbf{a}_3 = \frac{1}{4} a \hat{\mathbf{x}} + a \left(x_3 + \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}} & (16e) & \text{Au II} \\
\mathbf{B}_{25} &= \left(x_4 + \frac{3}{8}\right) \mathbf{a}_1 + \left(x_4 + \frac{1}{8}\right) \mathbf{a}_2 + \left(2x_4 + \frac{1}{4}\right) \mathbf{a}_3 = a x_4 \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{1}{8} c \hat{\mathbf{z}} & (16f) & \text{Au III} \\
\mathbf{B}_{26} &= -\left(x_4 - \frac{3}{8}\right) \mathbf{a}_1 - \left(x_4 - \frac{1}{8}\right) \mathbf{a}_2 - \left(2x_4 - \frac{1}{4}\right) \mathbf{a}_3 = -a x_4 \hat{\mathbf{x}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{1}{8} c \hat{\mathbf{z}} & (16f) & \text{Au III} \\
\mathbf{B}_{27} &= \left(x_4 + \frac{1}{8}\right) \mathbf{a}_1 - \left(x_4 - \frac{3}{8}\right) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 = -a \left(x_4 - \frac{1}{2}\right) \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{y}} - \frac{1}{8} c \hat{\mathbf{z}} & (16f) & \text{Au III} \\
\mathbf{B}_{28} &= -\left(x_4 - \frac{1}{8}\right) \mathbf{a}_1 + \left(x_4 + \frac{3}{8}\right) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 = a \left(x_4 + \frac{1}{2}\right) \hat{\mathbf{x}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{y}} - \frac{1}{8} c \hat{\mathbf{z}} & (16f) & \text{Au III} \\
\mathbf{B}_{29} &= -\left(x_4 - \frac{5}{8}\right) \mathbf{a}_1 - \left(x_4 - \frac{7}{8}\right) \mathbf{a}_2 - \left(2x_4 - \frac{3}{4}\right) \mathbf{a}_3 = -a \left(x_4 - \frac{1}{2}\right) \hat{\mathbf{x}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{3}{8} c \hat{\mathbf{z}} & (16f) & \text{Au III} \\
\mathbf{B}_{30} &= \left(x_4 + \frac{5}{8}\right) \mathbf{a}_1 + \left(x_4 + \frac{7}{8}\right) \mathbf{a}_2 + \left(2x_4 + \frac{3}{4}\right) \mathbf{a}_3 = a \left(x_4 + \frac{1}{2}\right) \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{3}{8} c \hat{\mathbf{z}} & (16f) & \text{Au III} \\
\mathbf{B}_{31} &= -\left(x_4 - \frac{7}{8}\right) \mathbf{a}_1 + \left(x_4 + \frac{5}{8}\right) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3 = a x_4 \hat{\mathbf{x}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{5}{8} c \hat{\mathbf{z}} & (16f) & \text{Au III} \\
\mathbf{B}_{32} &= \left(x_4 + \frac{7}{8}\right) \mathbf{a}_1 - \left(x_4 - \frac{5}{8}\right) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3 = -a x_4 \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{5}{8} c \hat{\mathbf{z}} & (16f) & \text{Au III}
\end{aligned}$$

References

- [1] H. Iwaskai, *Study on the Ordered Phases with Long Period in the Gold-Zinc Alloy System II. Structure Analysis of $\text{Au}_3\text{Zn}[R_1]$, $\text{Au}_3\text{Zn}[R_2]$ and Au_3+Zn* , J. Phys. Soc. Jpn. **17**, 1620–1633 (1962), doi:10.1143/JPSJ.17.1620.
- [2] E. A. Wood, *The Conversion Factor for kX Units to Angström Units*, J. Appl. Phys. **18**, 929–930 (1947), doi:10.1063/1.1697570.

Found in

- [1] K. Hisatsune, Y. Takuma, Y. Tanaka, K. Udoh, T. Morimura, and M. Hasaka, *Martensite transformation in Au_3Zn alloy*, Solid State Commun. **106**, 509–512 (1998), doi:10.1016/S0038-1098(98)00077-5.

First cited in

H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettel, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.