

# ScRh<sub>3</sub>Si<sub>7</sub> Structure:

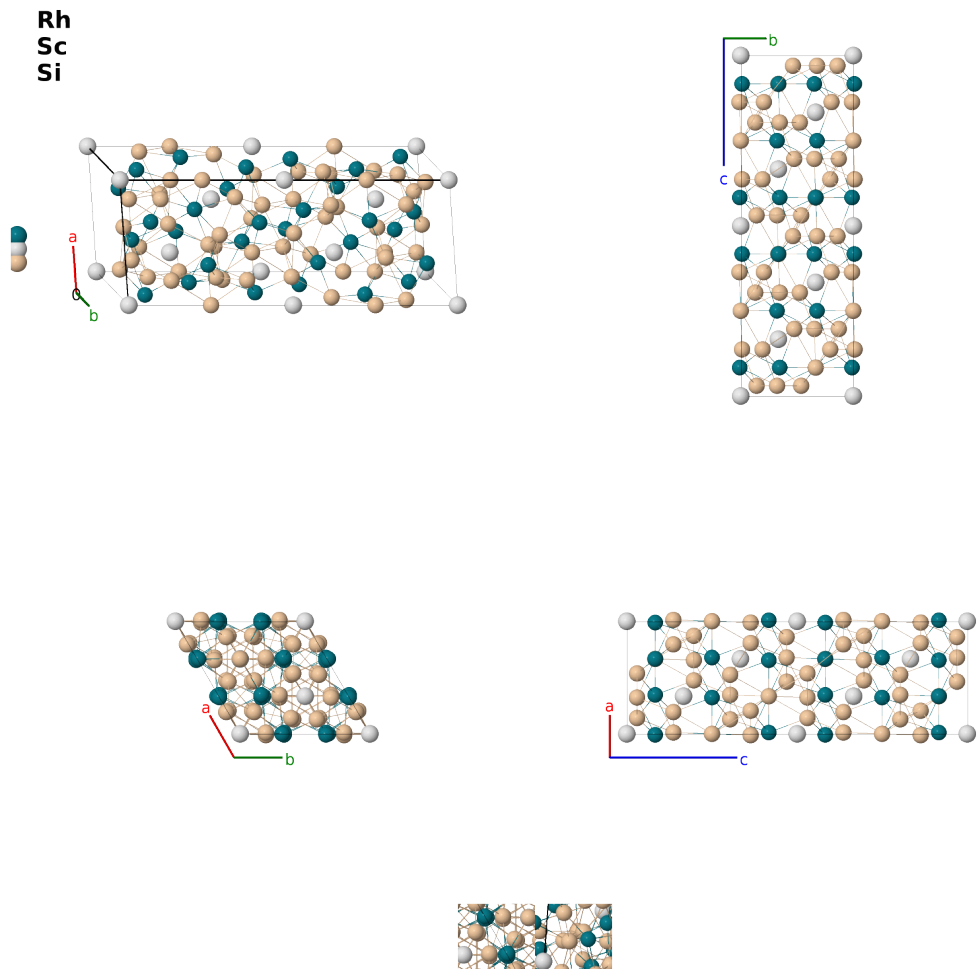
## A3BC7\_hR22\_167\_e\_b\_af-001

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- D. Hicks, M. J. Mehl, M. Esters, C. Osos, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/NS5K>

[https://aflow.org/prototype-encyclopedia/A3BC7\\_hR22\\_167\\_e\\_b\\_af-001](https://aflow.org/prototype-encyclopedia/A3BC7_hR22_167_e_b_af-001)



|                       |                                   |
|-----------------------|-----------------------------------|
| Prototype             | Rh <sub>3</sub> ScSi <sub>7</sub> |
| AFLOW prototype label | A3BC7_hR22_167_e_b_af-001         |
| ICSD                  | 15243                             |
| CCDC                  | 1596015                           |
| Pearson symbol        | hR22                              |
| Space group number    | 167                               |
| Space group symbol    | $R\bar{3}c$                       |

**AFLOW prototype command**    `aflow --proto=A3BC7_hR22_167_e_b_af-001`  
                                   `--params=a,c/a,x3,x4,y4,z4`

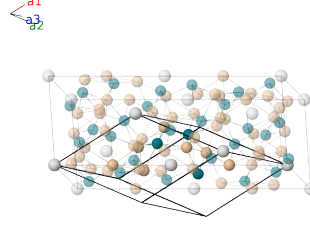
### Other compounds with this structure

CeAu<sub>3</sub>Al<sub>7</sub>, NdAu<sub>3</sub>Al<sub>7</sub>, PrAu<sub>3</sub>Al<sub>7</sub>, ScIr<sub>3</sub>Si<sub>7</sub>, SmAu<sub>3</sub>Al<sub>7</sub>, YbIr<sub>3</sub>Ge<sub>7</sub>, YbIr<sub>3</sub>Si<sub>7</sub>, YbRh<sub>3</sub>Si<sub>7</sub>

- Hexagonal settings of this structure can be obtained with the option `--hex`.

### Rhombohedral primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{\sqrt{3}}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= -\frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}}\end{aligned}$$



### Basis vectors

|                   | Lattice coordinates                                                                                         |     | Cartesian coordinates                                                                                                                                           | Wyckoff position | Atom type |
|-------------------|-------------------------------------------------------------------------------------------------------------|-----|-----------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------|-----------|
| $\mathbf{B}_1$    | $= \frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$                          | $=$ | $\frac{1}{4}c \hat{\mathbf{z}}$                                                                                                                                 | (2a)             | Si I      |
| $\mathbf{B}_2$    | $= \frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$                          | $=$ | $\frac{3}{4}c \hat{\mathbf{z}}$                                                                                                                                 | (2a)             | Si I      |
| $\mathbf{B}_3$    | $= 0$                                                                                                       | $=$ | $0$                                                                                                                                                             | (2b)             | Sc I      |
| $\mathbf{B}_4$    | $= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$                          | $=$ | $\frac{1}{2}c \hat{\mathbf{z}}$                                                                                                                                 | (2b)             | Sc I      |
| $\mathbf{B}_5$    | $= x_3 \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$                          | $=$ | $\frac{1}{8}a (4x_3 - 1) \hat{\mathbf{x}} - \frac{\sqrt{3}}{8}a (4x_3 - 1) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$                                    | (6e)             | Rh I      |
| $\mathbf{B}_6$    | $= \frac{1}{4} \mathbf{a}_1 + x_3 \mathbf{a}_2 - (x_3 - \frac{1}{2}) \mathbf{a}_3$                          | $=$ | $\frac{1}{8}a (4x_3 - 1) \hat{\mathbf{x}} + \frac{\sqrt{3}}{8}a (4x_3 - 1) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$                                    | (6e)             | Rh I      |
| $\mathbf{B}_7$    | $= -(x_3 - \frac{1}{2}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + x_3 \mathbf{a}_3$                         | $=$ | $-a (x_3 - \frac{1}{4}) \hat{\mathbf{x}} + \frac{1}{4}c \hat{\mathbf{z}}$                                                                                       | (6e)             | Rh I      |
| $\mathbf{B}_8$    | $= -x_3 \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$                         | $=$ | $-\frac{1}{8}a (4x_3 + 3) \hat{\mathbf{x}} + \frac{\sqrt{3}}{24}a (12x_3 + 1) \hat{\mathbf{y}} + \frac{5}{12}c \hat{\mathbf{z}}$                                | (6e)             | Rh I      |
| $\mathbf{B}_9$    | $= \frac{3}{4} \mathbf{a}_1 - x_3 \mathbf{a}_2 + (x_3 + \frac{1}{2}) \mathbf{a}_3$                          | $=$ | $-\frac{1}{8}a (4x_3 - 1) \hat{\mathbf{x}} - \frac{\sqrt{3}}{24}a (12x_3 + 5) \hat{\mathbf{y}} + \frac{5}{12}c \hat{\mathbf{z}}$                                | (6e)             | Rh I      |
| $\mathbf{B}_{10}$ | $= (x_3 + \frac{1}{2}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - x_3 \mathbf{a}_3$                          | $=$ | $a (x_3 + \frac{1}{4}) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + \frac{5}{12}c \hat{\mathbf{z}}$                                                | (6e)             | Rh I      |
| $\mathbf{B}_{11}$ | $= x_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$                                                  | $=$ | $\frac{1}{2}a (x_4 - z_4) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a (x_4 - 2y_4 + z_4) \hat{\mathbf{y}} + \frac{1}{3}c (x_4 + y_4 + z_4) \hat{\mathbf{z}}$         | (12f)            | Si II     |
| $\mathbf{B}_{12}$ | $= z_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + y_4 \mathbf{a}_3$                                                  | $=$ | $-\frac{1}{2}a (y_4 - z_4) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a (2x_4 - y_4 - z_4) \hat{\mathbf{y}} + \frac{1}{3}c (x_4 + y_4 + z_4) \hat{\mathbf{z}}$        | (12f)            | Si II     |
| $\mathbf{B}_{13}$ | $= y_4 \mathbf{a}_1 + z_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$                                                  | $=$ | $-\frac{1}{2}a (x_4 - y_4) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a (x_4 + y_4 - 2z_4) \hat{\mathbf{y}} + \frac{1}{3}c (x_4 + y_4 + z_4) \hat{\mathbf{z}}$        | (12f)            | Si II     |
| $\mathbf{B}_{14}$ | $= -(z_4 - \frac{1}{2}) \mathbf{a}_1 - (y_4 - \frac{1}{2}) \mathbf{a}_2 - (x_4 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $\frac{1}{2}a (x_4 - z_4) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a (x_4 - 2y_4 + z_4) \hat{\mathbf{y}} - \frac{1}{6}c (2x_4 + 2y_4 + 2z_4 - 3) \hat{\mathbf{z}}$  | (12f)            | Si II     |
| $\mathbf{B}_{15}$ | $= -(y_4 - \frac{1}{2}) \mathbf{a}_1 - (x_4 - \frac{1}{2}) \mathbf{a}_2 - (z_4 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $-\frac{1}{2}a (y_4 - z_4) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a (2x_4 - y_4 - z_4) \hat{\mathbf{y}} - \frac{1}{6}c (2x_4 + 2y_4 + 2z_4 - 3) \hat{\mathbf{z}}$ | (12f)            | Si II     |
| $\mathbf{B}_{16}$ | $= -(x_4 - \frac{1}{2}) \mathbf{a}_1 - (z_4 - \frac{1}{2}) \mathbf{a}_2 - (y_4 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $-\frac{1}{2}a (x_4 - y_4) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a (x_4 + y_4 - 2z_4) \hat{\mathbf{y}} - \frac{1}{6}c (2x_4 + 2y_4 + 2z_4 - 3) \hat{\mathbf{z}}$ | (12f)            | Si II     |

$$\begin{aligned}
\mathbf{B}_{17} &= -x_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 - z_4 \mathbf{a}_3 &= -\frac{1}{2}a(x_4 - z_4) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_4 - 2y_4 + z_4) \hat{\mathbf{y}} - \frac{1}{3}c(x_4 + y_4 + z_4) \hat{\mathbf{z}} &(12f) &\text{Si II} \\
\mathbf{B}_{18} &= -z_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - y_4 \mathbf{a}_3 &= \frac{1}{2}a(y_4 - z_4) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(2x_4 - y_4 - z_4) \hat{\mathbf{y}} - \frac{1}{3}c(x_4 + y_4 + z_4) \hat{\mathbf{z}} &(12f) &\text{Si II} \\
\mathbf{B}_{19} &= -y_4 \mathbf{a}_1 - z_4 \mathbf{a}_2 - x_4 \mathbf{a}_3 &= \frac{1}{2}a(x_4 - y_4) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_4 + y_4 - 2z_4) \hat{\mathbf{y}} - \frac{1}{3}c(x_4 + y_4 + z_4) \hat{\mathbf{z}} &(12f) &\text{Si II} \\
\mathbf{B}_{20} &= \left(z_4 + \frac{1}{2}\right) \mathbf{a}_1 + \left(y_4 + \frac{1}{2}\right) \mathbf{a}_2 + \left(x_4 + \frac{1}{2}\right) \mathbf{a}_3 &= -\frac{1}{2}a(x_4 - z_4) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_4 - 2y_4 + z_4) \hat{\mathbf{y}} + \frac{1}{6}c(2x_4 + 2y_4 + 2z_4 + 3) \hat{\mathbf{z}} &(12f) &\text{Si II} \\
\mathbf{B}_{21} &= \left(y_4 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_4 + \frac{1}{2}\right) \mathbf{a}_2 + \left(z_4 + \frac{1}{2}\right) \mathbf{a}_3 &= \frac{1}{2}a(y_4 - z_4) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(2x_4 - y_4 - z_4) \hat{\mathbf{y}} + \frac{1}{6}c(2x_4 + 2y_4 + 2z_4 + 3) \hat{\mathbf{z}} &(12f) &\text{Si II} \\
\mathbf{B}_{22} &= \left(x_4 + \frac{1}{2}\right) \mathbf{a}_1 + \left(z_4 + \frac{1}{2}\right) \mathbf{a}_2 + \left(y_4 + \frac{1}{2}\right) \mathbf{a}_3 &= \frac{1}{2}a(x_4 - y_4) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_4 + y_4 - 2z_4) \hat{\mathbf{y}} + \frac{1}{6}c(2x_4 + 2y_4 + 2z_4 + 3) \hat{\mathbf{z}} &(12f) &\text{Si II}
\end{aligned}$$

## References

- [1] B. Chabot, N. Engel, and E. Parthé, *Trirhodium scandium heptasilicide and triiridium scandium heptasilicide with a new rhombohedral structure type*, Acta Crystallogr. Sect. B **37**, 671–673 (1981), doi:10.1107/S0567740881003877.

## Found in

- [1] A. Jain, S. P. Ong, G. Hautier, W. Chen, W. D. Richards, S. Dacek, S. Cholia, D. Gunter, G. D. Ceder, and K. A. Persson, *Commentary: The Materials Project: A materials genome approach to accelerating materials innovation*, APL Materials **1**, 011002 (2013), doi:10.1063/1.4812323.

## First cited in

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