

Cr₅B₃ (*D*8_{*l*}) Structure: A3B5_tI32_140_ah_cl-001

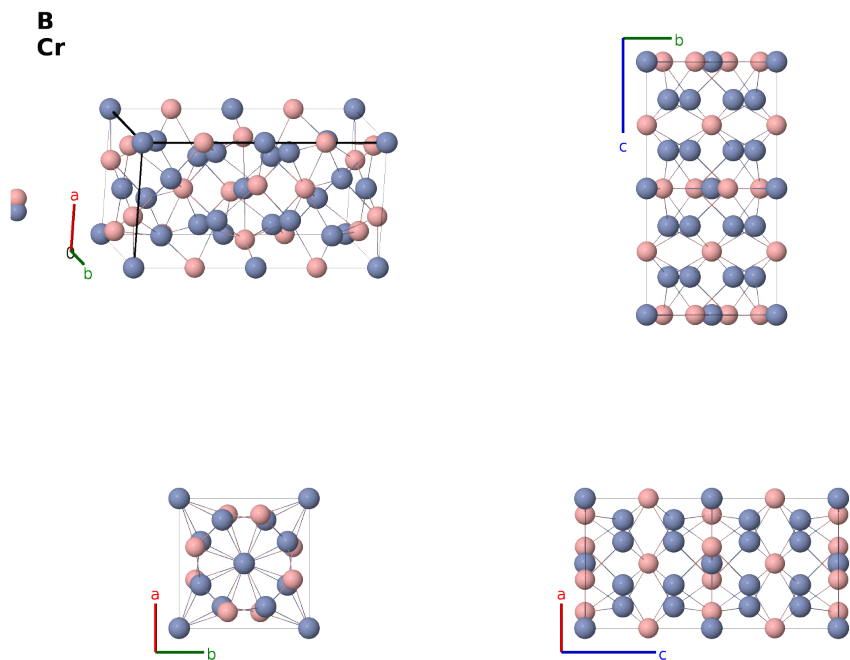
This structure previously used the label(s) **A3B5_tI32_140_ah.cl**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/AK18>

https://aflow.org/prototype-encyclopedia/A3B5_tI32_140_ah_cl-001



Prototype	B ₃ Cr ₅
AFLOW prototype label	A3B5_tI32_140_ah_cl-001
<i>Strukturbericht</i> designation	<i>D</i> 8 _{<i>l</i>}
ICSD	27124
CCDC	1602452
Pearson symbol	tI32
Space group number	140
Space group symbol	<i>I</i> 4/ <i>mcm</i>
AFLOW prototype command	<code>aflow --proto=A3B5_tI32_140_ah_cl-001</code> <code>--params=<i>a</i>, <i>c/a</i>, <i>x</i>₃, <i>x</i>₄, <i>z</i>₄</code>

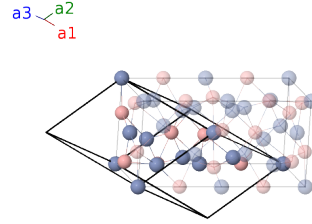
Other compounds with this structure

Ca₅Si₃, Eu₅Ge₃, EuIrGe₂, Fe₅PB₂, Fe₅SiB₂, Fe₄CoPB₂, Fe₄CoSiB₂, Fe₄MnPB₂, Fe₄MnSiB₂, Gd₅CoSi₂, Mo₅SiB₂, Nb₅Si₃, Pr₅Si₃, Sr₅In₃, Sr₅Si₃, Sr₅Sn₃, Ta₅Ge₃, Ta₅Si₃

- We have been unable to obtain a copy of (Bertaut, 1953), so we use the data found online from (Downs, 2003). Although Cr₅B₃ is universally regarded as the prototype for $D8_l$, it appears that no other determination of the internal parameters has ever been made. The values found in (Downs, 2003) seem to be reasonable choices, and agree with the ICSD entry.
- We originally transposed the decimal part of the value for c, using c = 10.46 rather than c = 10.64. This has now been corrected.

Body-centered Tetragonal primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2$	$=$	$\frac{1}{4}c \hat{\mathbf{z}}$	(4a)	B I
$\mathbf{B}_2$	$= \frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2$	$=$	$\frac{3}{4}c \hat{\mathbf{z}}$	(4a)	B I
$\mathbf{B}_3$	$= 0$	$=$	0	(4c)	Cr I
$\mathbf{B}_4$	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2}c \hat{\mathbf{z}}$	(4c)	Cr I
$\mathbf{B}_5$	$= \left(x_3 + \frac{1}{2}\right) \mathbf{a}_1 + x_3 \mathbf{a}_2 + \left(2x_3 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + a \left(x_3 + \frac{1}{2}\right) \hat{\mathbf{y}}$	(8h)	B II
$\mathbf{B}_6$	$= -\left(x_3 - \frac{1}{2}\right) \mathbf{a}_1 - x_3 \mathbf{a}_2 - \left(2x_3 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - a \left(x_3 - \frac{1}{2}\right) \hat{\mathbf{y}}$	(8h)	B II
$\mathbf{B}_7$	$= x_3 \mathbf{a}_1 - \left(x_3 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a \left(x_3 - \frac{1}{2}\right) \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}}$	(8h)	B II
$\mathbf{B}_8$	$= -x_3 \mathbf{a}_1 + \left(x_3 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a \left(x_3 + \frac{1}{2}\right) \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}}$	(8h)	B II
$\mathbf{B}_9$	$= \left(x_4 + z_4 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_4 + z_4\right) \mathbf{a}_2 + \left(2x_4 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{2}\right) \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(16l)	Cr II
$\mathbf{B}_{10}$	$= \left(-x_4 + z_4 + \frac{1}{2}\right) \mathbf{a}_1 - \left(x_4 - z_4\right) \mathbf{a}_2 - \left(2x_4 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - a \left(x_4 - \frac{1}{2}\right) \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(16l)	Cr II
$\mathbf{B}_{11}$	$= \left(x_4 + z_4\right) \mathbf{a}_1 + \left(-x_4 + z_4 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a \left(x_4 - \frac{1}{2}\right) \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(16l)	Cr II
$\mathbf{B}_{12}$	$= -\left(x_4 - z_4\right) \mathbf{a}_1 + \left(x_4 + z_4 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a \left(x_4 + \frac{1}{2}\right) \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(16l)	Cr II
$\mathbf{B}_{13}$	$= \left(x_4 - z_4\right) \mathbf{a}_1 - \left(x_4 + z_4 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a \left(x_4 - \frac{1}{2}\right) \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(16l)	Cr II
$\mathbf{B}_{14}$	$= -\left(x_4 + z_4\right) \mathbf{a}_1 + \left(x_4 - z_4 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a \left(x_4 + \frac{1}{2}\right) \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(16l)	Cr II

$$\mathbf{B}_{15} = \begin{pmatrix} (x_4 - z_4 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_4 - z_4) \mathbf{a}_2 + (2x_4 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = ax_4 \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{2}\right) \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}} \quad (16l) \quad \text{Cr II}$$

$$\mathbf{B}_{16} = \begin{pmatrix} -(x_4 + z_4 - \frac{1}{2}) \mathbf{a}_1 - \\ (x_4 + z_4) \mathbf{a}_2 - (2x_4 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -ax_4 \hat{\mathbf{x}} - a \left(x_4 - \frac{1}{2}\right) \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}} \quad (16l) \quad \text{Cr II}$$

References

- [1] F. Bertaut and P. Blum, *C. R. Acad. Sci.*, Comptes Rendus Hebdomadaires des Seances de l'Academie des Sciences **236**, 1055–1056 (1953).

Found in

- [1] R. T. Downs and M. Hall-Wallace, *The American Mineralogist Crystal Structure Database*, Am. Mineral. **88**, 247–250 (2003).

First cited in

D. Hicks, M. J. Mehl, E. Gossett, C. Toher, O. Levy, R. M. Hanson, G. Hart, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 2*, Comput. Mater. Sci. **161**, S1 (2019). doi: 10.1016/j.commatsci.2018.10.043