

Sc₂S₃ Structure:

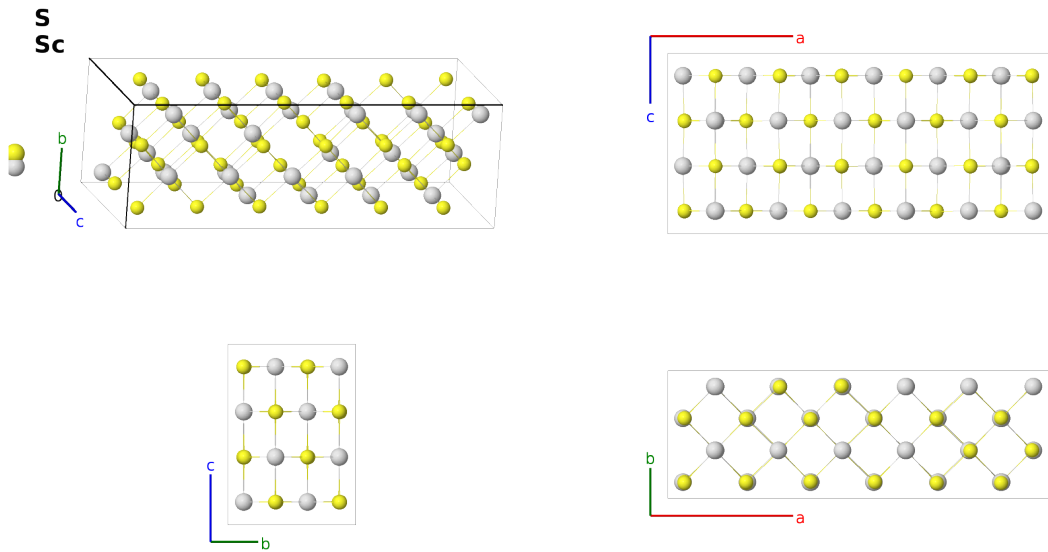
A3B2_oF80_70_fh_2e-001

Cite this page as:

- H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettl, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.
- D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/HQ18>

https://aflow.org/prototype-encyclopedia/A3B2_oF80_70_fh_2e-001



Prototype	S ₃ Sc ₂
AFLOW prototype label	A3B2_oF80_70_fh_2e-001
ICSD	22236
CCDC	1599011
Pearson symbol	oF80
Space group number	70
Space group symbol	<i>Fddd</i>
AFLOW prototype command	<code>aflow --proto=A3B2_oF80_70_fh_2e-001</code> <code>--params=a, b/a, c/a, x₁, x₂, y₃, x₄, y₄, z₄</code>

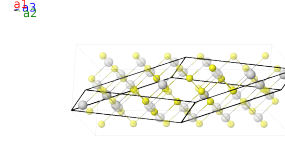
Other compounds with this structure

Dy₂Se₃, Dy₂Te₃, Eu₂Se₃, Eu₂Te₃, Lu₂Se₃, Sc₂Se₃, Y₂Se₃, Y₂Te₃, Yb₂Se₃

- This structure has been rotated from the orientation given by (Dismukes, 1964).

Face-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= -\left(x_1 - \frac{1}{4}\right) \mathbf{a}_1 + x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Sc I
$\mathbf{B}_2$	$= x_1 \mathbf{a}_1 - \left(x_1 - \frac{1}{4}\right) \mathbf{a}_2 - \left(x_1 - \frac{1}{4}\right) \mathbf{a}_3$	$=$	$-a\left(x_1 - \frac{1}{4}\right) \hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Sc I
$\mathbf{B}_3$	$= \left(x_1 + \frac{3}{4}\right) \mathbf{a}_1 - x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Sc I
$\mathbf{B}_4$	$= -x_1 \mathbf{a}_1 + \left(x_1 + \frac{3}{4}\right) \mathbf{a}_2 +$ $\left(x_1 + \frac{3}{4}\right) \mathbf{a}_3$	$=$	$a\left(x_1 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Sc I
$\mathbf{B}_5$	$= -\left(x_2 - \frac{1}{4}\right) \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Sc II
$\mathbf{B}_6$	$= x_2 \mathbf{a}_1 - \left(x_2 - \frac{1}{4}\right) \mathbf{a}_2 - \left(x_2 - \frac{1}{4}\right) \mathbf{a}_3$	$=$	$-a\left(x_2 - \frac{1}{4}\right) \hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Sc II
$\mathbf{B}_7$	$= \left(x_2 + \frac{3}{4}\right) \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Sc II
$\mathbf{B}_8$	$= -x_2 \mathbf{a}_1 + \left(x_2 + \frac{3}{4}\right) \mathbf{a}_2 +$ $\left(x_2 + \frac{3}{4}\right) \mathbf{a}_3$	$=$	$a\left(x_2 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Sc II
$\mathbf{B}_9$	$= y_3 \mathbf{a}_1 - \left(y_3 - \frac{1}{4}\right) \mathbf{a}_2 + y_3 \mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16f)	S I
$\mathbf{B}_{10}$	$= -\left(y_3 - \frac{1}{4}\right) \mathbf{a}_1 + y_3 \mathbf{a}_2 -$ $\left(y_3 - \frac{1}{4}\right) \mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} - b\left(y_3 - \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16f)	S I
$\mathbf{B}_{11}$	$= -y_3 \mathbf{a}_1 + \left(y_3 + \frac{3}{4}\right) \mathbf{a}_2 - y_3 \mathbf{a}_3$	$=$	$\frac{3}{8}a\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16f)	S I
$\mathbf{B}_{12}$	$= \left(y_3 + \frac{3}{4}\right) \mathbf{a}_1 - y_3 \mathbf{a}_2 + \left(y_3 + \frac{3}{4}\right) \mathbf{a}_3$	$=$	$\frac{3}{8}a\hat{\mathbf{x}} + b\left(y_3 + \frac{3}{4}\right) \hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16f)	S I
$\mathbf{B}_{13}$	$= \left(-x_4 + y_4 + z_4\right) \mathbf{a}_1 +$ $\left(x_4 - y_4 + z_4\right) \mathbf{a}_2 +$ $\left(x_4 + y_4 - z_4\right) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(32h)	S II
$\mathbf{B}_{14}$	$= \left(x_4 - y_4 + z_4\right) \mathbf{a}_1 +$ $\left(-x_4 + y_4 + z_4\right) \mathbf{a}_2 -$ $\left(x_4 + y_4 + z_4 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-a\left(x_4 - \frac{1}{4}\right) \hat{\mathbf{x}} - b\left(y_4 - \frac{1}{4}\right) \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(32h)	S II
$\mathbf{B}_{15}$	$= \left(x_4 + y_4 - z_4\right) \mathbf{a}_1 -$ $\left(x_4 + y_4 + z_4 - \frac{1}{2}\right) \mathbf{a}_2 +$ $\left(-x_4 + y_4 + z_4\right) \mathbf{a}_3$	$=$	$-a\left(x_4 - \frac{1}{4}\right) \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} - c\left(z_4 - \frac{1}{4}\right) \hat{\mathbf{z}}$	(32h)	S II
$\mathbf{B}_{16}$	$= -\left(x_4 + y_4 + z_4 - \frac{1}{2}\right) \mathbf{a}_1 +$ $\left(x_4 + y_4 - z_4\right) \mathbf{a}_2 +$ $\left(x_4 - y_4 + z_4\right) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - b\left(y_4 - \frac{1}{4}\right) \hat{\mathbf{y}} - c\left(z_4 - \frac{1}{4}\right) \hat{\mathbf{z}}$	(32h)	S II
$\mathbf{B}_{17}$	$= \left(x_4 - y_4 - z_4\right) \mathbf{a}_1 -$ $\left(x_4 - y_4 + z_4\right) \mathbf{a}_2 -$ $\left(x_4 + y_4 - z_4\right) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(32h)	S II
$\mathbf{B}_{18}$	$= -\left(x_4 - y_4 + z_4\right) \mathbf{a}_1 +$ $\left(x_4 - y_4 - z_4\right) \mathbf{a}_2 +$ $\left(x_4 + y_4 + z_4 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$a\left(x_4 + \frac{1}{4}\right) \hat{\mathbf{x}} + b\left(y_4 + \frac{1}{4}\right) \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(32h)	S II

$$\begin{aligned} \mathbf{B}_{19} &= \begin{aligned} &-(x_4 + y_4 - z_4) \mathbf{a}_1 + \\ &(x_4 + y_4 + z_4 + \tfrac{1}{2}) \mathbf{a}_2 + \\ &(x_4 - y_4 - z_4) \mathbf{a}_3 \end{aligned} &= a \left(x_4 + \tfrac{1}{4}\right) \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + c \left(z_4 + \tfrac{1}{4}\right) \hat{\mathbf{z}} \end{aligned} \quad (32h) \quad \text{S II}$$

$$\begin{aligned} \mathbf{B}_{20} &= \begin{aligned} &(x_4 + y_4 + z_4 + \tfrac{1}{2}) \mathbf{a}_1 - \\ &(x_4 + y_4 - z_4) \mathbf{a}_2 - \\ &(x_4 - y_4 + z_4) \mathbf{a}_3 \end{aligned} &= -ax_4 \hat{\mathbf{x}} + b \left(y_4 + \tfrac{1}{4}\right) \hat{\mathbf{y}} + c \left(z_4 + \tfrac{1}{4}\right) \hat{\mathbf{z}} \end{aligned} \quad (32h) \quad \text{S II}$$

References

- [1] J. P. Dismukes and J. G. White, *The Preparation, Properties, and Crystal Structures of Some Scandium Sulfides in the Range Sc_2S_3 - ScS* , Inorg. Chem. **3**, 1220–1228 (1964), doi:10.1021/ic50019a004.

First cited in

H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettel, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.