

Mn_{1.4}PtSn Structure:

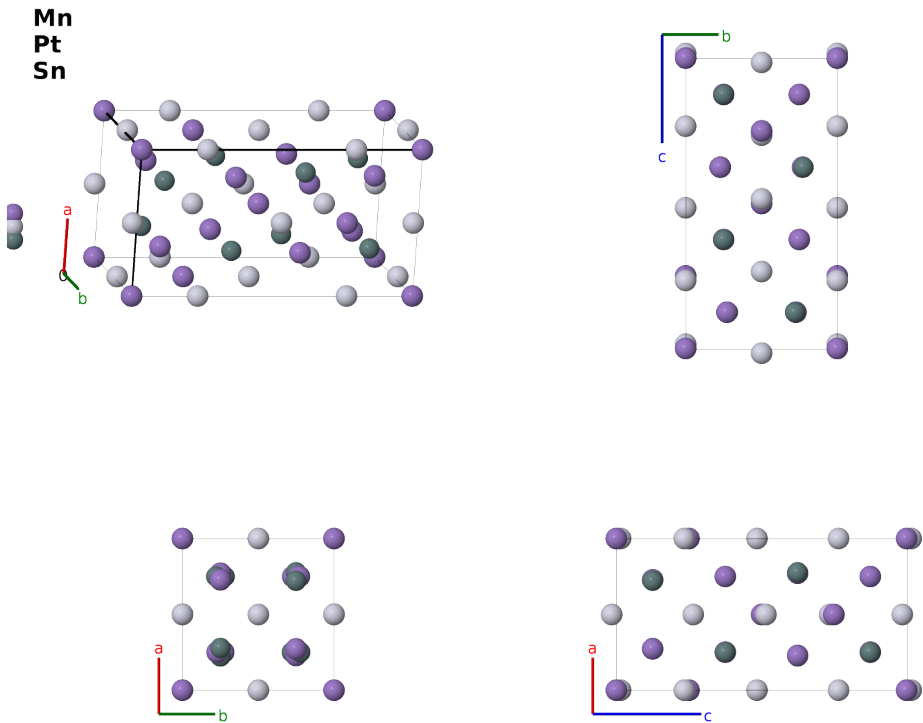
A3B2C2_tI28_122_ad_c_d-001

Cite this page as:

- H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettl, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.
- D. Hicks, M. J. Mehl, M. Esters, C. Osas, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/1YSS>

https://aflow.org/prototype-encyclopedia/A3B2C2_tI28_122_ad_c_d-001

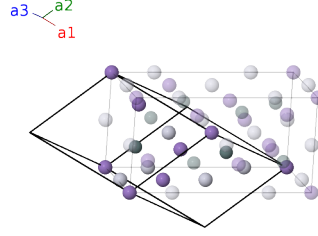


Prototype	Mn _{1.4} PtSn
AFLOW prototype label	A3B2C2_tI28_122_ad_c_d-001
ICSD	11061
CCDC	2134250
Pearson symbol	tI28
Space group number	122
Space group symbol	$I\bar{4}2d$
AFLOW prototype command	<code>aflow --proto=A3B2C2_tI28_122_ad_c_d-001</code> <code>--params=a, c/a, z₂, x₃, x₄</code>

- (Vir, 2019) found that the Mn (4a) site (in the layer with the platinum (8c) atoms) has 20% vacancies, giving the noted departure from the nominal $\text{Mn}_3\text{Pt}_2\text{Sn}_2$ stoichiometry.

Body-centered Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= 0$	$=$	0	(4a)	Mn I
$\mathbf{B}_2$	$= \frac{3}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(4a)	Mn I
$\mathbf{B}_3$	$= z_2\mathbf{a}_1 + z_2\mathbf{a}_2$	$=$	$cz_2\hat{\mathbf{z}}$	(8c)	Pt I
$\mathbf{B}_4$	$= -z_2\mathbf{a}_1 - z_2\mathbf{a}_2$	$=$	$-cz_2\hat{\mathbf{z}}$	(8c)	Pt I
$\mathbf{B}_5$	$= -\left(z_2 - \frac{3}{4}\right)\mathbf{a}_1 - \left(z_2 - \frac{1}{4}\right)\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{y}} - c\left(z_2 - \frac{1}{4}\right)\hat{\mathbf{z}}$	(8c)	Pt I
$\mathbf{B}_6$	$= \left(z_2 + \frac{3}{4}\right)\mathbf{a}_1 + \left(z_2 + \frac{1}{4}\right)\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{y}} + c\left(z_2 + \frac{1}{4}\right)\hat{\mathbf{z}}$	(8c)	Pt I
$\mathbf{B}_7$	$= \frac{3}{8}\mathbf{a}_1 + \left(x_3 + \frac{1}{8}\right)\mathbf{a}_2 + \left(x_3 + \frac{1}{4}\right)\mathbf{a}_3$	$=$	$ax_3\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(8d)	Mn II
$\mathbf{B}_8$	$= \frac{7}{8}\mathbf{a}_1 - \left(x_3 - \frac{1}{8}\right)\mathbf{a}_2 - \left(x_3 - \frac{3}{4}\right)\mathbf{a}_3$	$=$	$-ax_3\hat{\mathbf{x}} + \frac{3}{4}a\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(8d)	Mn II
$\mathbf{B}_9$	$= -\left(x_3 - \frac{7}{8}\right)\mathbf{a}_1 + \frac{1}{8}\mathbf{a}_2 - \left(x_3 - \frac{1}{4}\right)\mathbf{a}_3$	$=$	$-\frac{1}{4}a\hat{\mathbf{x}} - a\left(x_3 - \frac{1}{2}\right)\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(8d)	Mn II
$\mathbf{B}_{10}$	$= \left(x_3 + \frac{7}{8}\right)\mathbf{a}_1 + \frac{5}{8}\mathbf{a}_2 + \left(x_3 + \frac{3}{4}\right)\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + a\left(x_3 + \frac{1}{2}\right)\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(8d)	Mn II
$\mathbf{B}_{11}$	$= \frac{3}{8}\mathbf{a}_1 + \left(x_4 + \frac{1}{8}\right)\mathbf{a}_2 + \left(x_4 + \frac{1}{4}\right)\mathbf{a}_3$	$=$	$ax_4\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(8d)	Sn I
$\mathbf{B}_{12}$	$= \frac{7}{8}\mathbf{a}_1 - \left(x_4 - \frac{1}{8}\right)\mathbf{a}_2 - \left(x_4 - \frac{3}{4}\right)\mathbf{a}_3$	$=$	$-ax_4\hat{\mathbf{x}} + \frac{3}{4}a\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(8d)	Sn I
$\mathbf{B}_{13}$	$= -\left(x_4 - \frac{7}{8}\right)\mathbf{a}_1 + \frac{1}{8}\mathbf{a}_2 - \left(x_4 - \frac{1}{4}\right)\mathbf{a}_3$	$=$	$-\frac{1}{4}a\hat{\mathbf{x}} - a\left(x_4 - \frac{1}{2}\right)\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(8d)	Sn I
$\mathbf{B}_{14}$	$= \left(x_4 + \frac{7}{8}\right)\mathbf{a}_1 + \frac{5}{8}\mathbf{a}_2 + \left(x_4 + \frac{3}{4}\right)\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + a\left(x_4 + \frac{1}{2}\right)\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(8d)	Sn I

References

- [1] P. Vir, N. Kumar, H. Borrmann, B. Jamijansuren, G. Kreiner, C. Shekhar, and C. Felser, *Tetragonal Superstructure of the Antiskyrmion Hosting Heusler Compound $\text{Mn}_{1.4}\text{PtSn}$* , Chem. Mater. **31**, 5876–5880 (2019), doi:10.1021/acs.chemmater.9b02013.

First cited in

H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettel, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.