

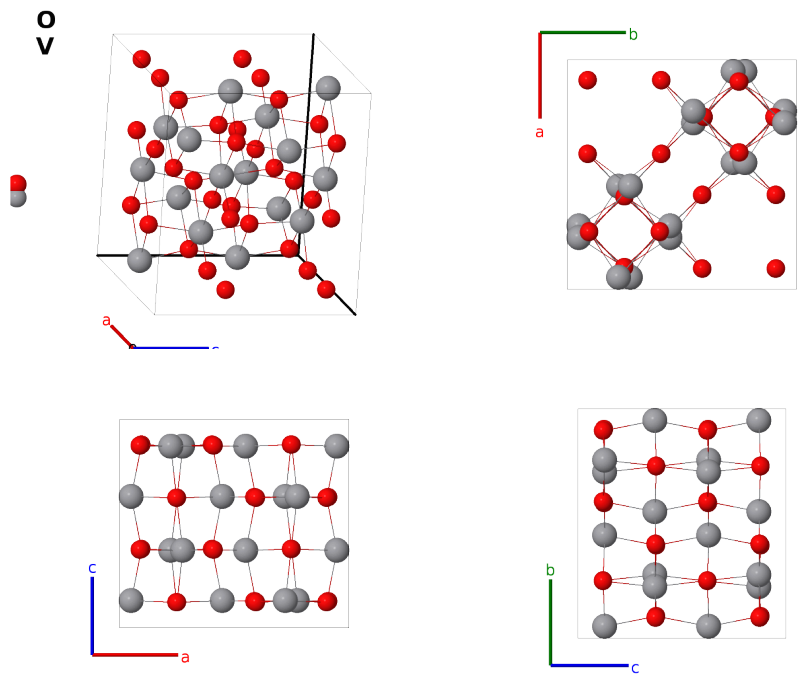
Room Temperature Metastable VO₂ Structure: A2B_tP48_130_2g_g-001

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- D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/P5YW>

https://aflow.org/prototype-encyclopedia/A2B_tP48_130_2g_g-001



Prototype	O ₂ V
AFLOW prototype label	A2B.tP48_130_2g_g-001
ICSD	51213
CCDC	1616106
Pearson symbol	tP48
Space group number	130
Space group symbol	<i>P4/ncc</i>
AFLOW prototype command	<code>aflow --proto=A2B_tP48_130_2g_g-001</code> <code>--params=a, c/a, x₁, y₁, z₁, x₂, y₂, z₂, x₃, y₃, z₃</code>

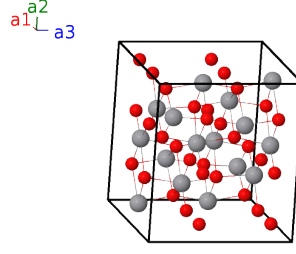
- While the ground state of VO₂ is similar to baddeleyite (*C43*) (Villars, 1918), there are several metastable states (Oka, 1998), including this structure, seen at 298K, and another tetragonal structure seen at 473K.
- It has also been seen in the arsenopyrite *E0₇* structure.

Simple Tetragonal primitive vectors

$$\mathbf{a}_1 = a \hat{\mathbf{x}}$$

$$\mathbf{a}_2 = a \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = c \hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= x_1 \mathbf{a}_1 + y_1 \mathbf{a}_2 + z_1 \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}} + ay_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_2$	$= -\left(x_1 - \frac{1}{2}\right) \mathbf{a}_1 - \left(y_1 - \frac{1}{2}\right) \mathbf{a}_2 + z_1 \mathbf{a}_3$	$=$	$-a\left(x_1 - \frac{1}{2}\right) \hat{\mathbf{x}} - a\left(y_1 - \frac{1}{2}\right) \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_3$	$= -\left(y_1 - \frac{1}{2}\right) \mathbf{a}_1 + x_1 \mathbf{a}_2 + z_1 \mathbf{a}_3$	$=$	$-a\left(y_1 - \frac{1}{2}\right) \hat{\mathbf{x}} + ax_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_4$	$= y_1 \mathbf{a}_1 - \left(x_1 - \frac{1}{2}\right) \mathbf{a}_2 + z_1 \mathbf{a}_3$	$=$	$ay_1 \hat{\mathbf{x}} - a\left(x_1 - \frac{1}{2}\right) \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_5$	$= -x_1 \mathbf{a}_1 + \left(y_1 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_1 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}} + a\left(y_1 + \frac{1}{2}\right) \hat{\mathbf{y}} - c\left(z_1 - \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_6$	$= \left(x_1 + \frac{1}{2}\right) \mathbf{a}_1 - y_1 \mathbf{a}_2 - \left(z_1 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$a\left(x_1 + \frac{1}{2}\right) \hat{\mathbf{x}} - ay_1 \hat{\mathbf{y}} - c\left(z_1 - \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_7$	$= \left(y_1 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_1 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_1 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$a\left(y_1 + \frac{1}{2}\right) \hat{\mathbf{x}} + a\left(x_1 + \frac{1}{2}\right) \hat{\mathbf{y}} - c\left(z_1 - \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_8$	$= -y_1 \mathbf{a}_1 - x_1 \mathbf{a}_2 - \left(z_1 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-ay_1 \hat{\mathbf{x}} - ax_1 \hat{\mathbf{y}} - c\left(z_1 - \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_9$	$= -x_1 \mathbf{a}_1 - y_1 \mathbf{a}_2 - z_1 \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}} - ay_1 \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_{10}$	$= \left(x_1 + \frac{1}{2}\right) \mathbf{a}_1 + \left(y_1 + \frac{1}{2}\right) \mathbf{a}_2 - z_1 \mathbf{a}_3$	$=$	$a\left(x_1 + \frac{1}{2}\right) \hat{\mathbf{x}} + a\left(y_1 + \frac{1}{2}\right) \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_{11}$	$= \left(y_1 + \frac{1}{2}\right) \mathbf{a}_1 - x_1 \mathbf{a}_2 - z_1 \mathbf{a}_3$	$=$	$a\left(y_1 + \frac{1}{2}\right) \hat{\mathbf{x}} - ax_1 \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_{12}$	$= -y_1 \mathbf{a}_1 + \left(x_1 + \frac{1}{2}\right) \mathbf{a}_2 - z_1 \mathbf{a}_3$	$=$	$-ay_1 \hat{\mathbf{x}} + a\left(x_1 + \frac{1}{2}\right) \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_{13}$	$= x_1 \mathbf{a}_1 - \left(y_1 - \frac{1}{2}\right) \mathbf{a}_2 + \left(z_1 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}} - a\left(y_1 - \frac{1}{2}\right) \hat{\mathbf{y}} + c\left(z_1 + \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_{14}$	$= -\left(x_1 - \frac{1}{2}\right) \mathbf{a}_1 + y_1 \mathbf{a}_2 + \left(z_1 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-a\left(x_1 - \frac{1}{2}\right) \hat{\mathbf{x}} + ay_1 \hat{\mathbf{y}} + c\left(z_1 + \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_{15}$	$= -\left(y_1 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_1 - \frac{1}{2}\right) \mathbf{a}_2 + \left(z_1 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-a\left(y_1 - \frac{1}{2}\right) \hat{\mathbf{x}} - a\left(x_1 - \frac{1}{2}\right) \hat{\mathbf{y}} + c\left(z_1 + \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_{16}$	$= y_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 + \left(z_1 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$ay_1 \hat{\mathbf{x}} + ax_1 \hat{\mathbf{y}} + c\left(z_1 + \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O I
$\mathbf{B}_{17}$	$= x_2 \mathbf{a}_1 + y_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + ay_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(16g)	O II
$\mathbf{B}_{18}$	$= -\left(x_2 - \frac{1}{2}\right) \mathbf{a}_1 - \left(y_2 - \frac{1}{2}\right) \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$-a\left(x_2 - \frac{1}{2}\right) \hat{\mathbf{x}} - a\left(y_2 - \frac{1}{2}\right) \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(16g)	O II
$\mathbf{B}_{19}$	$= -\left(y_2 - \frac{1}{2}\right) \mathbf{a}_1 + x_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$-a\left(y_2 - \frac{1}{2}\right) \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(16g)	O II
$\mathbf{B}_{20}$	$= y_2 \mathbf{a}_1 - \left(x_2 - \frac{1}{2}\right) \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$ay_2 \hat{\mathbf{x}} - a\left(x_2 - \frac{1}{2}\right) \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(16g)	O II
$\mathbf{B}_{21}$	$= -x_2 \mathbf{a}_1 + \left(y_2 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_2 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + a\left(y_2 + \frac{1}{2}\right) \hat{\mathbf{y}} - c\left(z_2 - \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O II
$\mathbf{B}_{22}$	$= \left(x_2 + \frac{1}{2}\right) \mathbf{a}_1 - y_2 \mathbf{a}_2 - \left(z_2 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$a\left(x_2 + \frac{1}{2}\right) \hat{\mathbf{x}} - ay_2 \hat{\mathbf{y}} - c\left(z_2 - \frac{1}{2}\right) \hat{\mathbf{z}}$	(16g)	O II

$$\begin{aligned}
\mathbf{B}_{23} &= \begin{pmatrix} y_2 + \frac{1}{2} \\ z_2 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_2 + \frac{1}{2} \\ z_2 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - \mathbf{a}_3 &= a \begin{pmatrix} y_2 + \frac{1}{2} \\ z_2 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + a \begin{pmatrix} x_2 + \frac{1}{2} \\ z_2 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - c \begin{pmatrix} y_2 + \frac{1}{2} \\ z_2 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{24} &= -y_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - \begin{pmatrix} z_2 - \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= -ay_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - c \begin{pmatrix} z_2 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{25} &= -x_2 \mathbf{a}_1 - y_2 \mathbf{a}_2 - z_2 \mathbf{a}_3 &= -ax_2 \hat{\mathbf{x}} - ay_2 \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{26} &= \begin{pmatrix} x_2 + \frac{1}{2} \\ y_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} y_2 + \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - z_2 \mathbf{a}_3 &= a \begin{pmatrix} x_2 + \frac{1}{2} \\ y_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + a \begin{pmatrix} y_2 + \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{27} &= \begin{pmatrix} y_2 + \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - x_2 \mathbf{a}_2 - z_2 \mathbf{a}_3 &= a \begin{pmatrix} y_2 + \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{28} &= -y_2 \mathbf{a}_1 + \begin{pmatrix} x_2 + \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - z_2 \mathbf{a}_3 &= -ay_2 \hat{\mathbf{x}} + a \begin{pmatrix} x_2 + \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{29} &= x_2 \mathbf{a}_1 - \begin{pmatrix} y_2 - \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \begin{pmatrix} z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= ax_2 \hat{\mathbf{x}} - a \begin{pmatrix} y_2 - \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + c \begin{pmatrix} z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{30} &= -\begin{pmatrix} x_2 - \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + y_2 \mathbf{a}_2 + \begin{pmatrix} z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= -a \begin{pmatrix} x_2 - \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + ay_2 \hat{\mathbf{y}} + c \begin{pmatrix} z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{31} &= -\begin{pmatrix} y_2 - \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_2 - \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \begin{pmatrix} z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= -a \begin{pmatrix} y_2 - \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - a \begin{pmatrix} x_2 - \frac{1}{2} \\ z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + c \begin{pmatrix} z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{32} &= y_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + \begin{pmatrix} z_2 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= ay_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + c \begin{pmatrix} z_2 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{O II} \\
\mathbf{B}_{33} &= x_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 + z_3 \mathbf{a}_3 &= ax_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{34} &= -\begin{pmatrix} x_3 - \frac{1}{2} \\ z_3 \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} y_3 - \frac{1}{2} \\ z_3 \end{pmatrix} \mathbf{a}_2 + z_3 \mathbf{a}_3 &= -a \begin{pmatrix} x_3 - \frac{1}{2} \\ z_3 \end{pmatrix} \hat{\mathbf{x}} - a \begin{pmatrix} y_3 - \frac{1}{2} \\ z_3 \end{pmatrix} \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{35} &= -\begin{pmatrix} y_3 - \frac{1}{2} \\ z_3 \end{pmatrix} \mathbf{a}_1 + x_3 \mathbf{a}_2 + z_3 \mathbf{a}_3 &= -a \begin{pmatrix} y_3 - \frac{1}{2} \\ z_3 \end{pmatrix} \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{36} &= y_3 \mathbf{a}_1 - \begin{pmatrix} x_3 - \frac{1}{2} \\ z_3 \end{pmatrix} \mathbf{a}_2 + z_3 \mathbf{a}_3 &= ay_3 \hat{\mathbf{x}} - a \begin{pmatrix} x_3 - \frac{1}{2} \\ z_3 \end{pmatrix} \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{37} &= -x_3 \mathbf{a}_1 + \begin{pmatrix} y_3 + \frac{1}{2} \\ z_3 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - \begin{pmatrix} z_3 - \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= -ax_3 \hat{\mathbf{x}} + a \begin{pmatrix} y_3 + \frac{1}{2} \\ z_3 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - c \begin{pmatrix} z_3 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{38} &= \begin{pmatrix} x_3 + \frac{1}{2} \\ y_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - y_3 \mathbf{a}_2 - \begin{pmatrix} z_3 - \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= a \begin{pmatrix} x_3 + \frac{1}{2} \\ y_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} - c \begin{pmatrix} z_3 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{39} &= \begin{pmatrix} y_3 + \frac{1}{2} \\ z_3 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_3 + \frac{1}{2} \\ z_3 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - \begin{pmatrix} z_3 - \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= a \begin{pmatrix} y_3 + \frac{1}{2} \\ z_3 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + a \begin{pmatrix} x_3 + \frac{1}{2} \\ z_3 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - c \begin{pmatrix} z_3 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{40} &= -y_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - \begin{pmatrix} z_3 - \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= -ay_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - c \begin{pmatrix} z_3 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{41} &= -x_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 - z_3 \mathbf{a}_3 &= -ax_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{42} &= \begin{pmatrix} x_3 + \frac{1}{2} \\ y_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} y_3 + \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - z_3 \mathbf{a}_3 &= a \begin{pmatrix} x_3 + \frac{1}{2} \\ y_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + a \begin{pmatrix} y_3 + \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{43} &= \begin{pmatrix} y_3 + \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - x_3 \mathbf{a}_2 - z_3 \mathbf{a}_3 &= a \begin{pmatrix} y_3 + \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{44} &= -y_3 \mathbf{a}_1 + \begin{pmatrix} x_3 + \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - z_3 \mathbf{a}_3 &= -ay_3 \hat{\mathbf{x}} + a \begin{pmatrix} x_3 + \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{45} &= x_3 \mathbf{a}_1 - \begin{pmatrix} y_3 - \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \begin{pmatrix} z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= ax_3 \hat{\mathbf{x}} - a \begin{pmatrix} y_3 - \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + c \begin{pmatrix} z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{46} &= -\begin{pmatrix} x_3 - \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + y_3 \mathbf{a}_2 + \begin{pmatrix} z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= -a \begin{pmatrix} x_3 - \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} + c \begin{pmatrix} z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{47} &= -\begin{pmatrix} y_3 - \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_3 - \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \begin{pmatrix} z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= -a \begin{pmatrix} y_3 - \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - a \begin{pmatrix} x_3 - \frac{1}{2} \\ z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + c \begin{pmatrix} z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{V I} \\
\mathbf{B}_{48} &= y_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + \begin{pmatrix} z_3 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= ay_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + c \begin{pmatrix} z_3 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(16g) & \text{V I}
\end{aligned}$$

References

- [1] Y. Oka, S. Sato, T. Yao, and N. Yamamoto, *Crystal Structures and Transition Mechanism of VO₂ (A)*, J. Solid State Chem. **141**, 594–598 (1998), doi:10.1006/jssc.1998.8025.
- [2] P. Villars, H. Okamoto, and K. Cenzual, eds., *ASM Alloy Phase Diagram Database* (ASM International, 2018), chap. Oxygen-Vanadium Binary Phase Diagram (1990 Wriedt H.A.). Copyright ©2006-2018 ASM International.

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