

$D6_2$ (Sb_2O_4 , *Obsolete*) Structure: A2B_cF96_227_abf_cd-001

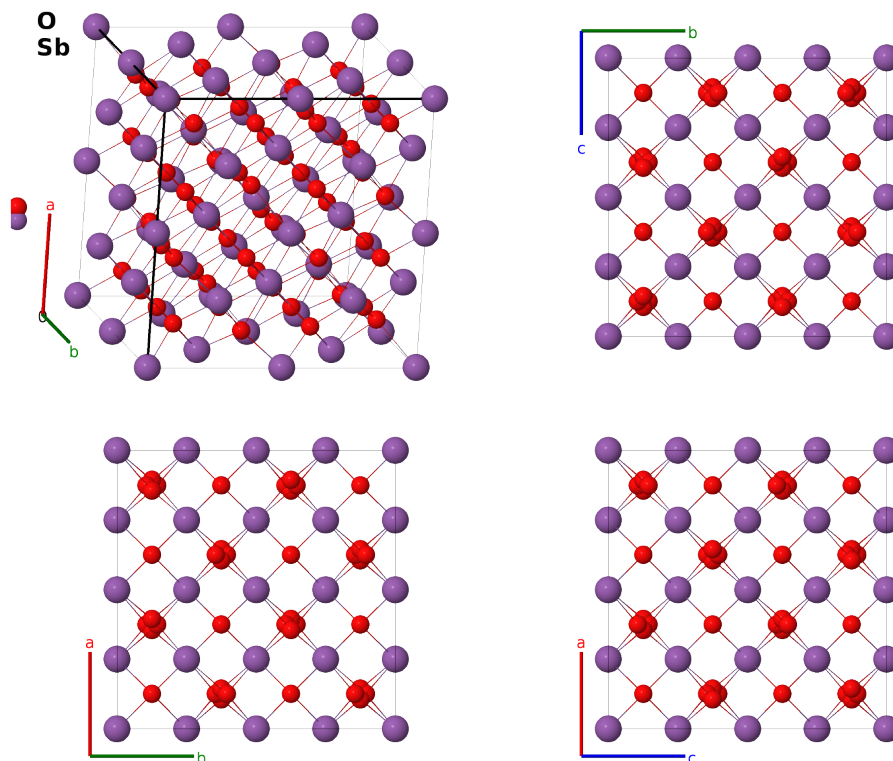
This structure previously used the label(s) **A2B_cF96_227_abf_cd**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/UGWY>

https://aflow.org/prototype-encyclopedia/A2B_cF96_227_abf_cd-001

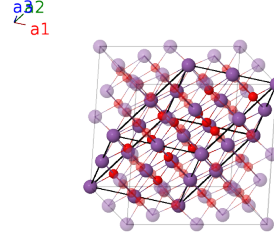


Prototype	O_2Sb
AFLOW prototype label	A2B_cF96_227_abf_cd-001
<i>Strukturbericht</i> designation	$D6_2$
ICSD	24244
CCDC	1600290
Pearson symbol	cF96
Space group number	227
Space group symbol	$Fd\bar{3}m$
AFLOW prototype command	<code>aflow --proto=A2B_cF96_227_abf_cd-001</code> <code>--params=a, x_5</code>

- Shortly after (Gottfried, 1937) gave this compound the *Strukturbericht* designation $D6_2$, (Dihiström, 1937) showed that they were actually determining the structure of $\text{Sb}_3\text{O}_6\text{OH}$, making this structure obsolete. Indeed, (Herrman, 1943) formally withdraws this from the *Strukturbericht* list, saying “The type and description [in (Gottfried, 1937)] should be deleted, as the radiographs were not based on the supposed substance.” We present it for its historical interest.
- Modern experiments have determined that SbO_2 appears as cervantite ($\alpha\text{-Sb}_2\text{O}_4$) or clinocervantite ($\beta\text{-Sb}_2\text{O}_4$).

Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{1}{8}\mathbf{a}_1 + \frac{1}{8}\mathbf{a}_2 + \frac{1}{8}\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(8a)	O I
$\mathbf{B}_2$	$= \frac{7}{8}\mathbf{a}_1 + \frac{7}{8}\mathbf{a}_2 + \frac{7}{8}\mathbf{a}_3$	$=$	$\frac{7}{8}a\hat{\mathbf{x}} + \frac{7}{8}a\hat{\mathbf{y}} + \frac{7}{8}a\hat{\mathbf{z}}$	(8a)	O I
$\mathbf{B}_3$	$= \frac{3}{8}\mathbf{a}_1 + \frac{3}{8}\mathbf{a}_2 + \frac{3}{8}\mathbf{a}_3$	$=$	$\frac{3}{8}a\hat{\mathbf{x}} + \frac{3}{8}a\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}}$	(8b)	O II
$\mathbf{B}_4$	$= \frac{5}{8}\mathbf{a}_1 + \frac{5}{8}\mathbf{a}_2 + \frac{5}{8}\mathbf{a}_3$	$=$	$\frac{5}{8}a\hat{\mathbf{x}} + \frac{5}{8}a\hat{\mathbf{y}} + \frac{5}{8}a\hat{\mathbf{z}}$	(8b)	O II
$\mathbf{B}_5$	$= 0$	$=$	0	(16c)	Sb I
$\mathbf{B}_6$	$= \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}}$	(16c)	Sb I
$\mathbf{B}_7$	$= \frac{1}{2}\mathbf{a}_2$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16c)	Sb I
$\mathbf{B}_8$	$= \frac{1}{2}\mathbf{a}_1$	$=$	$\frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16c)	Sb I
$\mathbf{B}_9$	$= \frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}}$	(16d)	Sb II
$\mathbf{B}_{10}$	$= \frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}}$	(16d)	Sb II
$\mathbf{B}_{11}$	$= \frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16d)	Sb II
$\mathbf{B}_{12}$	$= \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16d)	Sb II
$\mathbf{B}_{13}$	$= -\left(x_5 - \frac{1}{4}\right)\mathbf{a}_1 + x_5\mathbf{a}_2 + x_5\mathbf{a}_3$	$=$	$ax_5\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	O III
$\mathbf{B}_{14}$	$= x_5\mathbf{a}_1 - \left(x_5 - \frac{1}{4}\right)\mathbf{a}_2 - \left(x_5 - \frac{1}{4}\right)\mathbf{a}_3$	$=$	$-a\left(x_5 - \frac{1}{4}\right)\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	O III
$\mathbf{B}_{15}$	$= x_5\mathbf{a}_1 - \left(x_5 - \frac{1}{4}\right)\mathbf{a}_2 + x_5\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	O III
$\mathbf{B}_{16}$	$= -\left(x_5 - \frac{1}{4}\right)\mathbf{a}_1 + x_5\mathbf{a}_2 - \left(x_5 - \frac{1}{4}\right)\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} - a\left(x_5 - \frac{1}{4}\right)\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	O III
$\mathbf{B}_{17}$	$= x_5\mathbf{a}_1 + x_5\mathbf{a}_2 - \left(x_5 - \frac{1}{4}\right)\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + ax_5\hat{\mathbf{z}}$	(48f)	O III
$\mathbf{B}_{18}$	$= -\left(x_5 - \frac{1}{4}\right)\mathbf{a}_1 - \left(x_5 - \frac{1}{4}\right)\mathbf{a}_2 + x_5\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} - a\left(x_5 - \frac{1}{4}\right)\hat{\mathbf{z}}$	(48f)	O III
$\mathbf{B}_{19}$	$= \left(x_5 + \frac{3}{4}\right)\mathbf{a}_1 - x_5\mathbf{a}_2 + \left(x_5 + \frac{3}{4}\right)\mathbf{a}_3$	$=$	$\frac{3}{8}a\hat{\mathbf{x}} + a\left(x_5 + \frac{3}{4}\right)\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}}$	(48f)	O III
$\mathbf{B}_{20}$	$= -x_5\mathbf{a}_1 + \left(x_5 + \frac{3}{4}\right)\mathbf{a}_2 - x_5\mathbf{a}_3$	$=$	$\frac{3}{8}a\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}}$	(48f)	O III

$$\begin{aligned}
\mathbf{B}_{21} &= -x_5 \mathbf{a}_1 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_2 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_3 = a \left(x_5 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{O III} \\
\mathbf{B}_{22} &= \left(x_5 + \frac{3}{4}\right) \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3 = -ax_5 \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{O III} \\
\mathbf{B}_{23} &= -x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_3 = \frac{3}{8}a \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} & (48f) & \text{O III} \\
\mathbf{B}_{24} &= \left(x_5 + \frac{3}{4}\right) \mathbf{a}_1 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_2 - x_5 \mathbf{a}_3 = \frac{3}{8}a \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} + a \left(x_5 + \frac{3}{4}\right) \hat{\mathbf{z}} & (48f) & \text{O III}
\end{aligned}$$

References

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D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.