

Sb₂Tl₇ (*L2*₂) Structure: A2B7_cI54_229_e_afh-001

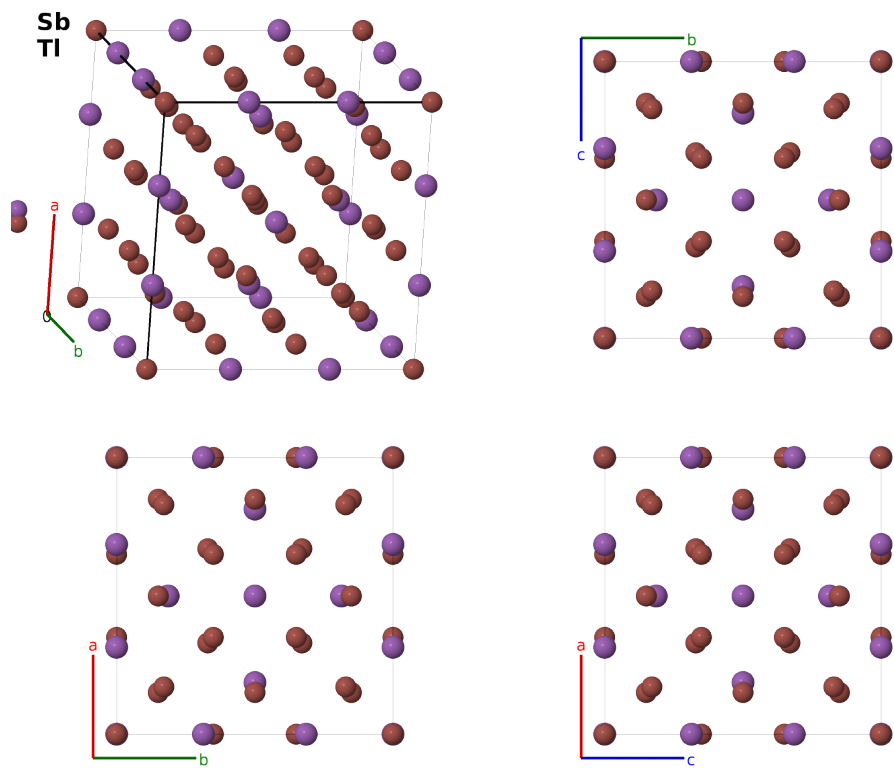
This structure previously used the label(s) **A2B7_cI54_229_e_afh**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/KM4R>

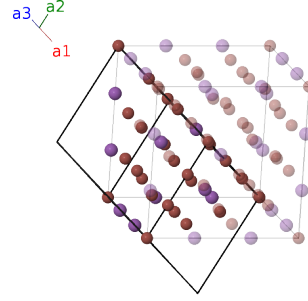
https://aflow.org/prototype-encyclopedia/A2B7_cI54_229_e_afh-001



Prototype	Sb ₂ Tl ₇
AFLOW prototype label	A2B7_cI54_229_e_afh-001
<i>Strukturbericht</i> designation	<i>L2</i> ₂
ICSD	41816
CCDC	1611567
Pearson symbol	cI54
Space group number	229
Space group symbol	<i>Im</i> $\bar{3}m$
AFLOW prototype command	<code>aflow --proto=A2B7_cI54_229_e_afh-001 --params=<i>a</i>, <i>x</i>₂, <i>x</i>₃, <i>y</i>₄</code>

Body-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} - \frac{1}{2}a\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	0	$=$	0	Tl I
$\mathbf{B}_2$	$=$	$x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}}$	(12e) Sb I
$\mathbf{B}_3$	$=$	$-x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}}$	(12e) Sb I
$\mathbf{B}_4$	$=$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{y}}$	(12e) Sb I
$\mathbf{B}_5$	$=$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{y}}$	(12e) Sb I
$\mathbf{B}_6$	$=$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2$	$=$	$ax_2 \hat{\mathbf{z}}$	(12e) Sb I
$\mathbf{B}_7$	$=$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2$	$=$	$-ax_2 \hat{\mathbf{z}}$	(12e) Sb I
$\mathbf{B}_8$	$=$	$2x_3 \mathbf{a}_1 + 2x_3 \mathbf{a}_2 + 2x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(16f) Tl II
$\mathbf{B}_9$	$=$	$-2x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(16f) Tl II
$\mathbf{B}_{10}$	$=$	$-2x_3 \mathbf{a}_2$	$=$	$-ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16f) Tl II
$\mathbf{B}_{11}$	$=$	$-2x_3 \mathbf{a}_1$	$=$	$ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16f) Tl II
$\mathbf{B}_{12}$	$=$	$2x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16f) Tl II
$\mathbf{B}_{13}$	$=$	$-2x_3 \mathbf{a}_1 - 2x_3 \mathbf{a}_2 - 2x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16f) Tl II
$\mathbf{B}_{14}$	$=$	$2x_3 \mathbf{a}_2$	$=$	$ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(16f) Tl II
$\mathbf{B}_{15}$	$=$	$2x_3 \mathbf{a}_1$	$=$	$-ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(16f) Tl II
$\mathbf{B}_{16}$	$=$	$2y_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + y_4 \mathbf{a}_3$	$=$	$ay_4 \hat{\mathbf{y}} + ay_4 \hat{\mathbf{z}}$	(24h) Tl III
$\mathbf{B}_{17}$	$=$	$y_4 \mathbf{a}_2 - y_4 \mathbf{a}_3$	$=$	$-ay_4 \hat{\mathbf{y}} + ay_4 \hat{\mathbf{z}}$	(24h) Tl III
$\mathbf{B}_{18}$	$=$	$-y_4 \mathbf{a}_2 + y_4 \mathbf{a}_3$	$=$	$ay_4 \hat{\mathbf{y}} - ay_4 \hat{\mathbf{z}}$	(24h) Tl III
$\mathbf{B}_{19}$	$=$	$-2y_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 - y_4 \mathbf{a}_3$	$=$	$-ay_4 \hat{\mathbf{y}} - ay_4 \hat{\mathbf{z}}$	(24h) Tl III
$\mathbf{B}_{20}$	$=$	$y_4 \mathbf{a}_1 + 2y_4 \mathbf{a}_2 + y_4 \mathbf{a}_3$	$=$	$ay_4 \hat{\mathbf{x}} + ay_4 \hat{\mathbf{z}}$	(24h) Tl III
$\mathbf{B}_{21}$	$=$	$-y_4 \mathbf{a}_1 + y_4 \mathbf{a}_3$	$=$	$ay_4 \hat{\mathbf{x}} - ay_4 \hat{\mathbf{z}}$	(24h) Tl III
$\mathbf{B}_{22}$	$=$	$y_4 \mathbf{a}_1 - y_4 \mathbf{a}_3$	$=$	$-ay_4 \hat{\mathbf{x}} + ay_4 \hat{\mathbf{z}}$	(24h) Tl III
$\mathbf{B}_{23}$	$=$	$-y_4 \mathbf{a}_1 - 2y_4 \mathbf{a}_2 - y_4 \mathbf{a}_3$	$=$	$-ay_4 \hat{\mathbf{x}} - ay_4 \hat{\mathbf{z}}$	(24h) Tl III
$\mathbf{B}_{24}$	$=$	$y_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + 2y_4 \mathbf{a}_3$	$=$	$ay_4 \hat{\mathbf{x}} + ay_4 \hat{\mathbf{y}}$	(24h) Tl III
$\mathbf{B}_{25}$	$=$	$y_4 \mathbf{a}_1 - y_4 \mathbf{a}_2$	$=$	$-ay_4 \hat{\mathbf{x}} + ay_4 \hat{\mathbf{y}}$	(24h) Tl III
$\mathbf{B}_{26}$	$=$	$-y_4 \mathbf{a}_1 + y_4 \mathbf{a}_2$	$=$	$ay_4 \hat{\mathbf{x}} - ay_4 \hat{\mathbf{y}}$	(24h) Tl III
$\mathbf{B}_{27}$	$=$	$-y_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 - 2y_4 \mathbf{a}_3$	$=$	$-ay_4 \hat{\mathbf{x}} - ay_4 \hat{\mathbf{y}}$	(24h) Tl III

References

- [1] R. Stokhuyzen, C. Chieh, and W. B. Pearson, *Crystal Structure of Sb_2Te_7* , Can. J. Chem. **55**, 1120–1122 (1977), doi:10.1139/v77-157.

Found in

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