

Phase III Cd₂Re₂O₇ Structure: A2B7C2_tI44_98_f_acde_f-001

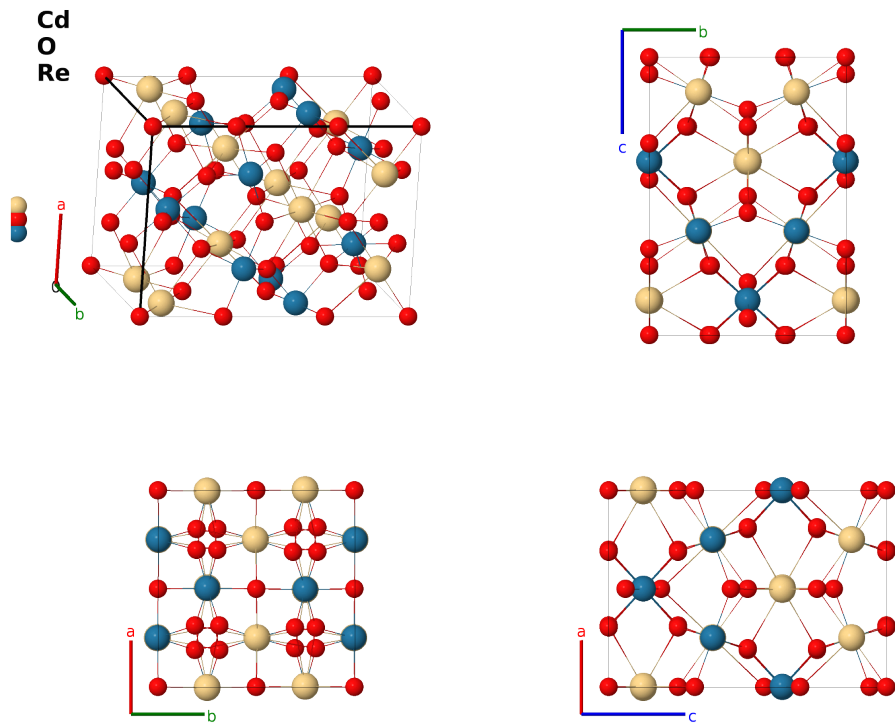
This structure previously used the label(s) **A2B7C2_tI44_98_f_bcde_f**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/XLYF>

https://aflow.org/prototype-encyclopedia/A2B7C2_tI44_98_f_acde_f-001



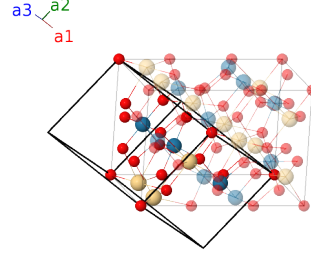
Prototype	Cd ₂ O ₇ Re ₂
AFLOW prototype label	A2B7C2_tI44_98_f_acde_f-001
Pearson symbol	tI44
Space group number	98
Space group symbol	I4 ₁ 22
AFLOW prototype command	<code>aflow --proto=A2B7C2_tI44_98_f_acde_f-001</code> <code>--params=a, c/a, z₂, x₃, x₄, x₅, x₆</code>

- Cd₂Re₂O₇ exhibits a number of phases. We will use the notation of (Kapcia, 2020) to describe them:

- Phase I: Above 200K the system takes on the cubic pyrochlore ($E8_1$) structure.
- Phase II: in the range 120-200K the system is in the tetragonal $I\bar{4}m2$ #119 structure.
- Phase III: in the range 80-120K the system is in the tetragonal $I4_122$ #98 structure (this structure).
- Phase IV: (Kapcia, 2020) did a first-principles study of this system and found that below 80K Phase III develops a soft phonon mode which transforms the system into an orthorhombic $F222$ #22 structure.
- There are many issues with all of these structures (Norman, 2020):
 - Phases II, III, and IV are all close to phase I. If we loosen the tolerance using AFLOW-SYM or FINDSYM the structures are seen to be equivalent to cubic pyrochlore.
 - Using the default tolerance, Phase II and Phase IV are equivalent.

Body-centered Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= 0$	$=$	0	(4a)	O I
$\mathbf{B}_2$	$= \frac{3}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(4a)	O I
$\mathbf{B}_3$	$= z_2 \mathbf{a}_1 + z_2 \mathbf{a}_2$	$=$	$cz_2 \hat{\mathbf{z}}$	(8c)	O II
$\mathbf{B}_4$	$= (z_2 + \frac{3}{4}) \mathbf{a}_1 + (z_2 + \frac{1}{4}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{y}} + c(z_2 + \frac{1}{4}) \hat{\mathbf{z}}$	(8c)	O II
$\mathbf{B}_5$	$= -(z_2 - \frac{3}{4}) \mathbf{a}_1 - (z_2 - \frac{1}{4}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{y}} - c(z_2 - \frac{1}{4}) \hat{\mathbf{z}}$	(8c)	O II
$\mathbf{B}_6$	$= -z_2 \mathbf{a}_1 - z_2 \mathbf{a}_2$	$=$	$-cz_2 \hat{\mathbf{z}}$	(8c)	O II
$\mathbf{B}_7$	$= x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + 2x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}}$	(8d)	O III
$\mathbf{B}_8$	$= -x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - 2x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}}$	(8d)	O III
$\mathbf{B}_9$	$= (x_3 + \frac{3}{4}) \mathbf{a}_1 - (x_3 - \frac{1}{4}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + a(x_3 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8d)	O III
$\mathbf{B}_{10}$	$= -(x_3 - \frac{3}{4}) \mathbf{a}_1 + (x_3 + \frac{1}{4}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8d)	O III
$\mathbf{B}_{11}$	$= x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2$	$=$	$-ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}}$	(8e)	O IV
$\mathbf{B}_{12}$	$= -x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2$	$=$	$ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}}$	(8e)	O IV
$\mathbf{B}_{13}$	$= -(x_4 - \frac{3}{4}) \mathbf{a}_1 - (x_4 - \frac{1}{4}) \mathbf{a}_2 - (2x_4 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - a(x_4 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8e)	O IV
$\mathbf{B}_{14}$	$= (x_4 + \frac{3}{4}) \mathbf{a}_1 + (x_4 + \frac{1}{4}) \mathbf{a}_2 + (2x_4 + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + a(x_4 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8e)	O IV
$\mathbf{B}_{15}$	$= \frac{3}{8} \mathbf{a}_1 + (x_5 + \frac{1}{8}) \mathbf{a}_2 + (x_5 + \frac{1}{4}) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(8f)	Cd I
$\mathbf{B}_{16}$	$= \frac{7}{8} \mathbf{a}_1 - (x_5 - \frac{1}{8}) \mathbf{a}_2 - (x_5 - \frac{3}{4}) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + \frac{3}{4}a \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(8f)	Cd I

$$\begin{aligned}
\mathbf{B}_{17} &= \left(x_5 + \frac{7}{8}\right) \mathbf{a}_1 + \frac{1}{8} \mathbf{a}_2 + \left(x_5 + \frac{1}{4}\right) \mathbf{a}_3 = -\frac{1}{4}a \hat{\mathbf{x}} + a \left(x_5 + \frac{1}{2}\right) \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}} & (8f) & \text{Cd I} \\
\mathbf{B}_{18} &= -\left(x_5 - \frac{7}{8}\right) \mathbf{a}_1 + \frac{5}{8} \mathbf{a}_2 - \left(x_5 - \frac{3}{4}\right) \mathbf{a}_3 = \frac{1}{4}a \hat{\mathbf{x}} - a \left(x_5 - \frac{1}{2}\right) \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}} & (8f) & \text{Cd I} \\
\mathbf{B}_{19} &= \frac{3}{8} \mathbf{a}_1 + \left(x_6 + \frac{1}{8}\right) \mathbf{a}_2 + \left(x_6 + \frac{1}{4}\right) \mathbf{a}_3 = ax_6 \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}} & (8f) & \text{Re I} \\
\mathbf{B}_{20} &= \frac{7}{8} \mathbf{a}_1 - \left(x_6 - \frac{1}{8}\right) \mathbf{a}_2 - \left(x_6 - \frac{3}{4}\right) \mathbf{a}_3 = -ax_6 \hat{\mathbf{x}} + \frac{3}{4}a \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}} & (8f) & \text{Re I} \\
\mathbf{B}_{21} &= \left(x_6 + \frac{7}{8}\right) \mathbf{a}_1 + \frac{1}{8} \mathbf{a}_2 + \left(x_6 + \frac{1}{4}\right) \mathbf{a}_3 = -\frac{1}{4}a \hat{\mathbf{x}} + a \left(x_6 + \frac{1}{2}\right) \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}} & (8f) & \text{Re I} \\
\mathbf{B}_{22} &= -\left(x_6 - \frac{7}{8}\right) \mathbf{a}_1 + \frac{5}{8} \mathbf{a}_2 - \left(x_6 - \frac{3}{4}\right) \mathbf{a}_3 = \frac{1}{4}a \hat{\mathbf{x}} - a \left(x_6 - \frac{1}{2}\right) \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}} & (8f) & \text{Re I}
\end{aligned}$$

References

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Found in

- [1] M. R. Norman, *Crystal structure of the inversion-breaking metal $\text{Cd}_2\text{Re}_2\text{O}_7$* , Phys. Rev. B **101**, 045117 (2020), doi:10.1103/PhysRevB.101.045117.

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