

Predicted Phase IV $\text{Cd}_2\text{Re}_2\text{O}_7$ Structure: A2B7C2_oF88_22_k_acefghij_k-001

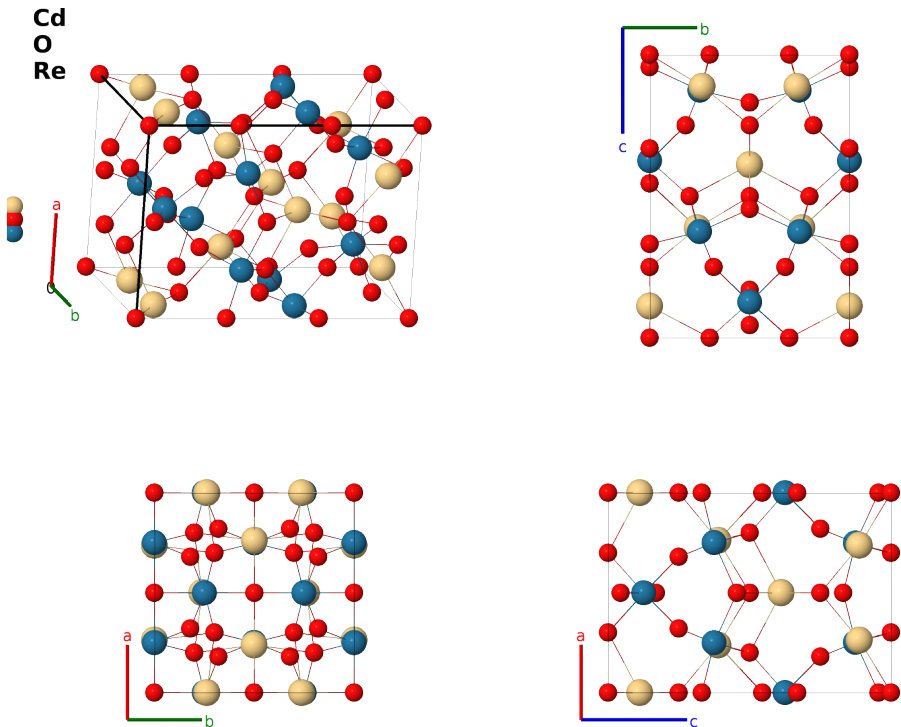
This structure previously used the label(s) A2B7C2_oF88_22_k.bdefghij_k. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/71CA>

https://aflow.org/prototype-encyclopedia/A2B7C2_oF88_22_k_acefghij_k-001



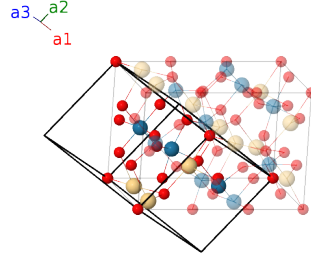
Prototype	$\text{Cd}_2\text{O}_7\text{Re}_2$
AFLOW prototype label	A2B7C2_oF88_22_k_acefghij_k-001
Pearson symbol	tI44
Space group number	82
Space group symbol	$I\bar{4}$
AFLOW prototype command	<pre>aflow --proto=A2B7C2_oF88_22_k_acefghij_k-001 --params=a, c/a, z3, z4, x5, y5, z5, x6, y6, z6, x7, y7, z7, x8, y8, z8</pre>

- $\text{Cd}_2\text{Re}_2\text{O}_7$ exhibits a number of phases. We will use the notation of (Kapcia, 2020) to describe them:

- Phase I: Above 200K the system takes on the cubic pyrochlore ($E8_1$) structure.
- Phase II: in the range 120-200K the system is in the tetragonal $I\bar{4}m2$ #119 structure.
- Phase III: in the range 80-120K the system is in the tetragonal $I4_122$ #98 structure.
- Phase IV: (Kapcia, 2020) did a first-principles study of this system and found that below 80K Phase III develops a soft phonon mode which transforms the system into an orthorhombic $F222$ #22 structure. (This structure)
- There are many issues with all of these structures (Norman, 2020):
 - Phases II, III, and IV are all close to phase I. If we loosen the tolerance using AFLOW-SYM or FINDSYM the structures are seen to be equivalent to cubic pyrochlore.
 - Using the default tolerance, Phase II and Phase IV are equivalent.
- Although the default AFLOW tolerance makes this structure equivalent to Phase II, the published structure can be recovered using the command:
- `afLOW--proto=A2B7C2_oF88_22_k_acefghij_k:Cd:O:Re --params=a,c/a,z3,z4,x5,x6,x7,z7,x8,z8 --tolerance=0.001.`

Body-centered Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	0	$=$	0	(2a)	O I
$\mathbf{B}_2$	$\frac{3}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(2c)	O II
$\mathbf{B}_3$	$z_3\mathbf{a}_1 + z_3\mathbf{a}_2$	$=$	$cz_3\hat{\mathbf{z}}$	(4e)	O III
$\mathbf{B}_4$	$-z_3\mathbf{a}_1 - z_3\mathbf{a}_2$	$=$	$-cz_3\hat{\mathbf{z}}$	(4e)	O III
$\mathbf{B}_5$	$(z_4 + \frac{1}{2})\mathbf{a}_1 + z_4\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(4f)	O IV
$\mathbf{B}_6$	$-z_4\mathbf{a}_1 - (z_4 - \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} - cz_4\hat{\mathbf{z}}$	(4f)	O IV
$\mathbf{B}_7$	$(y_5 + z_5)\mathbf{a}_1 + (x_5 + z_5)\mathbf{a}_2 + (x_5 + y_5)\mathbf{a}_3$	$=$	$ax_5\hat{\mathbf{x}} + ay_5\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8g)	Cd I
$\mathbf{B}_8$	$-(y_5 - z_5)\mathbf{a}_1 - (x_5 - z_5)\mathbf{a}_2 - (x_5 + y_5)\mathbf{a}_3$	$=$	$-ax_5\hat{\mathbf{x}} - ay_5\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8g)	Cd I
$\mathbf{B}_9$	$-(x_5 + z_5)\mathbf{a}_1 + (y_5 - z_5)\mathbf{a}_2 - (x_5 - y_5)\mathbf{a}_3$	$=$	$ay_5\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}} - cz_5\hat{\mathbf{z}}$	(8g)	Cd I
$\mathbf{B}_{10}$	$(x_5 - z_5)\mathbf{a}_1 - (y_5 + z_5)\mathbf{a}_2 + (x_5 - y_5)\mathbf{a}_3$	$=$	$-ay_5\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}} - cz_5\hat{\mathbf{z}}$	(8g)	Cd I
$\mathbf{B}_{11}$	$(y_6 + z_6)\mathbf{a}_1 + (x_6 + z_6)\mathbf{a}_2 + (x_6 + y_6)\mathbf{a}_3$	$=$	$ax_6\hat{\mathbf{x}} + ay_6\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8g)	O V
$\mathbf{B}_{12}$	$-(y_6 - z_6)\mathbf{a}_1 - (x_6 - z_6)\mathbf{a}_2 - (x_6 + y_6)\mathbf{a}_3$	$=$	$-ax_6\hat{\mathbf{x}} - ay_6\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8g)	O V

$$\begin{aligned}
\mathbf{B}_{13} &= \begin{matrix} -(x_6 + z_6) \mathbf{a}_1 + (y_6 - z_6) \mathbf{a}_2 - \\ (x_6 - y_6) \mathbf{a}_3 \end{matrix} = ay_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (8g) & \text{O V} \\
\mathbf{B}_{14} &= \begin{matrix} (x_6 - z_6) \mathbf{a}_1 - (y_6 + z_6) \mathbf{a}_2 + \\ (x_6 - y_6) \mathbf{a}_3 \end{matrix} = -ay_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (8g) & \text{O V} \\
\mathbf{B}_{15} &= \begin{matrix} (y_7 + z_7) \mathbf{a}_1 + (x_7 + z_7) \mathbf{a}_2 + \\ (x_7 + y_7) \mathbf{a}_3 \end{matrix} = ax_7 \hat{\mathbf{x}} + ay_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (8g) & \text{O VI} \\
\mathbf{B}_{16} &= \begin{matrix} -(y_7 - z_7) \mathbf{a}_1 - (x_7 - z_7) \mathbf{a}_2 - \\ (x_7 + y_7) \mathbf{a}_3 \end{matrix} = -ax_7 \hat{\mathbf{x}} - ay_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (8g) & \text{O VI} \\
\mathbf{B}_{17} &= \begin{matrix} -(x_7 + z_7) \mathbf{a}_1 + (y_7 - z_7) \mathbf{a}_2 - \\ (x_7 - y_7) \mathbf{a}_3 \end{matrix} = ay_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (8g) & \text{O VI} \\
\mathbf{B}_{18} &= \begin{matrix} (x_7 - z_7) \mathbf{a}_1 - (y_7 + z_7) \mathbf{a}_2 + \\ (x_7 - y_7) \mathbf{a}_3 \end{matrix} = -ay_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (8g) & \text{O VI} \\
\mathbf{B}_{19} &= \begin{matrix} (y_8 + z_8) \mathbf{a}_1 + (x_8 + z_8) \mathbf{a}_2 + \\ (x_8 + y_8) \mathbf{a}_3 \end{matrix} = ax_8 \hat{\mathbf{x}} + ay_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (8g) & \text{Re I} \\
\mathbf{B}_{20} &= \begin{matrix} -(y_8 - z_8) \mathbf{a}_1 - (x_8 - z_8) \mathbf{a}_2 - \\ (x_8 + y_8) \mathbf{a}_3 \end{matrix} = -ax_8 \hat{\mathbf{x}} - ay_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (8g) & \text{Re I} \\
\mathbf{B}_{21} &= \begin{matrix} -(x_8 + z_8) \mathbf{a}_1 + (y_8 - z_8) \mathbf{a}_2 - \\ (x_8 - y_8) \mathbf{a}_3 \end{matrix} = ay_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (8g) & \text{Re I} \\
\mathbf{B}_{22} &= \begin{matrix} (x_8 - z_8) \mathbf{a}_1 - (y_8 + z_8) \mathbf{a}_2 + \\ (x_8 - y_8) \mathbf{a}_3 \end{matrix} = -ay_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (8g) & \text{Re I}
\end{aligned}$$

References

- [1] K. J. Kapcia, M. Reedyk, M. Hajialamdari, A. Ptok, P. Piekarczyk, A. Schulz, F. S. Razavi, R. K. Kremer, and A. M. Oleś, *Discovery of a low-temperature orthorhombic phase of the $\text{Cd}_2\text{Re}_2\text{O}_7$ superconductor*, Phys. Rev. Res. **2**, 033108 (2020), doi:10.1103/PhysRevResearch.2.033108.

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