

Thenardite [Na₂SO₄ (V), *H1*₇] Structure: A2B4C_oF56_70_e_h_a-001

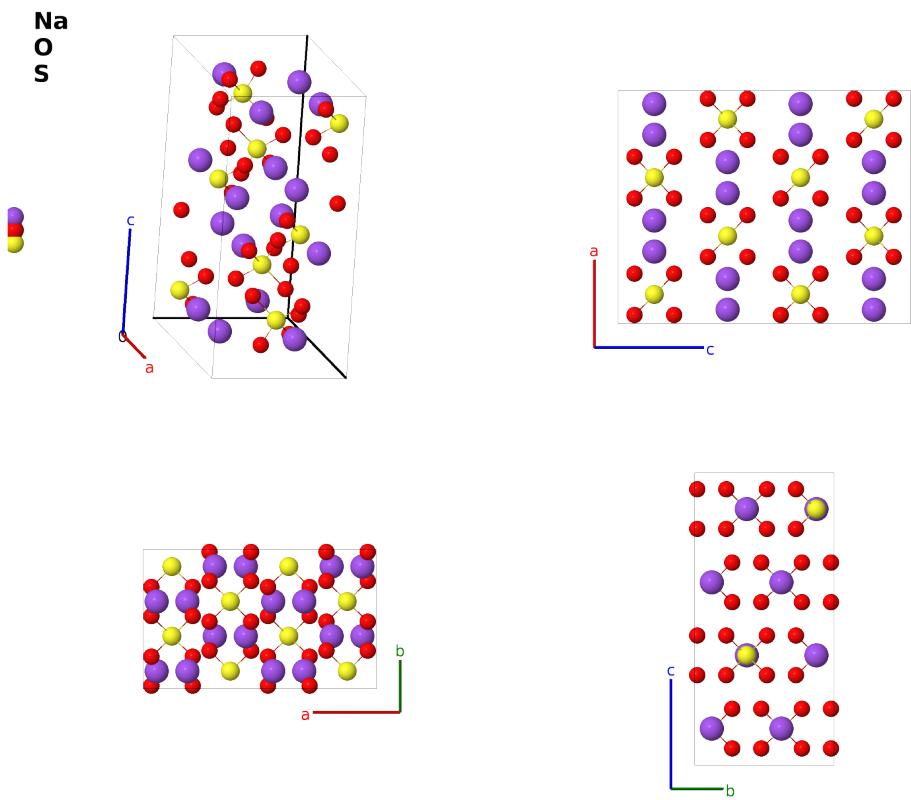
This structure previously used the label(s) **A2B4C_oF56_70_g_h_a**. Calls to these addresses will be redirected here.

Cite this page as:

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- D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/8CBQ>

https://aflow.org/prototype-encyclopedia/A2B4C_oF56_70_e_h_a-001



Prototype	Na ₂ O ₄ S
AFLOW prototype label	A2B4C_oF56_70_e_h_a-001
<i>Strukturbericht</i> designation	<i>H1</i> ₇
Mineral name	thenardite
ICSD	2895
CCDC	1592687
Pearson symbol	oF56
Space group number	70

Space group symbol $Fddd$

AFLOW prototype command `aflow --proto=A2B4C_oF56_70_e_h_a-001`
`--params=a, b/a, c/a, x2, x3, y3, z3`

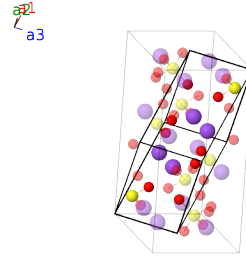
Other compounds with this structure

Ag₂SO₄, Ag₂SeO₄, Cd₂SiO₄, Cr₂SO₄, Cr₂SiO₄, Hg₂GeO₄, Na₂MoO₄, Na₂SeO₄

- Na₂SO₄ has eight known anhydrous phases. For now we have
 - Na₂SO₄ III and
 - Thenardite (Na₂SO₄ V, $H1_7$) (this structure).
- The thenardite phase is “reported to be stable between 32°C and about 180°C” (Nord, 1973), however the data reported here was taken on synthetic thenardite at 25°C.
- The AFLOW label protocol moves the sodium atoms from the reported (16g) site to the (16e) site. This involves shifting the axes so that $\hat{z} \rightarrow \hat{x} \rightarrow \hat{y} \rightarrow \hat{z}$.

Face-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{1}{8}\mathbf{a}_1 + \frac{1}{8}\mathbf{a}_2 + \frac{1}{8}\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(8a)	S I
$\mathbf{B}_2$	$= \frac{7}{8}\mathbf{a}_1 + \frac{7}{8}\mathbf{a}_2 + \frac{7}{8}\mathbf{a}_3$	$=$	$\frac{7}{8}a\hat{\mathbf{x}} + \frac{7}{8}b\hat{\mathbf{y}} + \frac{7}{8}c\hat{\mathbf{z}}$	(8a)	S I
$\mathbf{B}_3$	$= -(x_2 - \frac{1}{4})\mathbf{a}_1 + x_2\mathbf{a}_2 + x_2\mathbf{a}_3$	$=$	$ax_2\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_4$	$= x_2\mathbf{a}_1 - (x_2 - \frac{1}{4})\mathbf{a}_2 - (x_2 - \frac{1}{4})\mathbf{a}_3$	$=$	$-a(x_2 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_5$	$= (x_2 + \frac{3}{4})\mathbf{a}_1 - x_2\mathbf{a}_2 - x_2\mathbf{a}_3$	$=$	$-ax_2\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_6$	$= -x_2\mathbf{a}_1 + (x_2 + \frac{3}{4})\mathbf{a}_2 + (x_2 + \frac{3}{4})\mathbf{a}_3$	$=$	$a(x_2 + \frac{3}{4})\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_7$	$= (-x_3 + y_3 + z_3)\mathbf{a}_1 + (x_3 - y_3 + z_3)\mathbf{a}_2 + (x_3 + y_3 - z_3)\mathbf{a}_3$	$=$	$ax_3\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(32h)	O I
$\mathbf{B}_8$	$= (x_3 - y_3 + z_3)\mathbf{a}_1 + (-x_3 + y_3 + z_3)\mathbf{a}_2 - (x_3 + y_3 + z_3 - \frac{1}{2})\mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{4})\hat{\mathbf{x}} - b(y_3 - \frac{1}{4})\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(32h)	O I
$\mathbf{B}_9$	$= (x_3 + y_3 - z_3)\mathbf{a}_1 - (x_3 + y_3 + z_3 - \frac{1}{2})\mathbf{a}_2 + (-x_3 + y_3 + z_3)\mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{4})\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} - c(z_3 - \frac{1}{4})\hat{\mathbf{z}}$	(32h)	O I

$$\begin{aligned} \mathbf{B}_{10} = & -\left(x_3 + y_3 + z_3 - \frac{1}{2}\right) \mathbf{a}_1 + & = & ax_3 \hat{\mathbf{x}} - b\left(y_3 - \frac{1}{4}\right) \hat{\mathbf{y}} - c\left(z_3 - \frac{1}{4}\right) \hat{\mathbf{z}} & (32h) & \text{O I} \\ & \left(x_3 + y_3 - z_3\right) \mathbf{a}_2 + \\ & \left(x_3 - y_3 + z_3\right) \mathbf{a}_3 \end{aligned}$$

$$\begin{aligned} \mathbf{B}_{11} = & \left(x_3 - y_3 - z_3\right) \mathbf{a}_1 - & = & -ax_3 \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}} & (32h) & \text{O I} \\ & \left(x_3 - y_3 + z_3\right) \mathbf{a}_2 - \\ & \left(x_3 + y_3 - z_3\right) \mathbf{a}_3 \end{aligned}$$

$$\begin{aligned} \mathbf{B}_{12} = & -\left(x_3 - y_3 + z_3\right) \mathbf{a}_1 + & = & a\left(x_3 + \frac{1}{4}\right) \hat{\mathbf{x}} + b\left(y_3 + \frac{1}{4}\right) \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}} & (32h) & \text{O I} \\ & \left(x_3 - y_3 - z_3\right) \mathbf{a}_2 + \\ & \left(x_3 + y_3 + z_3 + \frac{1}{2}\right) \mathbf{a}_3 \end{aligned}$$

$$\begin{aligned} \mathbf{B}_{13} = & -\left(x_3 + y_3 - z_3\right) \mathbf{a}_1 + & = & a\left(x_3 + \frac{1}{4}\right) \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + c\left(z_3 + \frac{1}{4}\right) \hat{\mathbf{z}} & (32h) & \text{O I} \\ & \left(x_3 + y_3 + z_3 + \frac{1}{2}\right) \mathbf{a}_2 + \\ & \left(x_3 - y_3 - z_3\right) \mathbf{a}_3 \end{aligned}$$

$$\begin{aligned} \mathbf{B}_{14} = & \left(x_3 + y_3 + z_3 + \frac{1}{2}\right) \mathbf{a}_1 - & = & -ax_3 \hat{\mathbf{x}} + b\left(y_3 + \frac{1}{4}\right) \hat{\mathbf{y}} + c\left(z_3 + \frac{1}{4}\right) \hat{\mathbf{z}} & (32h) & \text{O I} \\ & \left(x_3 + y_3 - z_3\right) \mathbf{a}_2 - \\ & \left(x_3 - y_3 + z_3\right) \mathbf{a}_3 \end{aligned}$$

References

- [1] A. C. Nord, *Refinement of the Crystal Structure of Thenardite Na_2SO_4 (V)*, Acta Chem. Scand. **27**, 814–822 (1973).

First cited in

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