

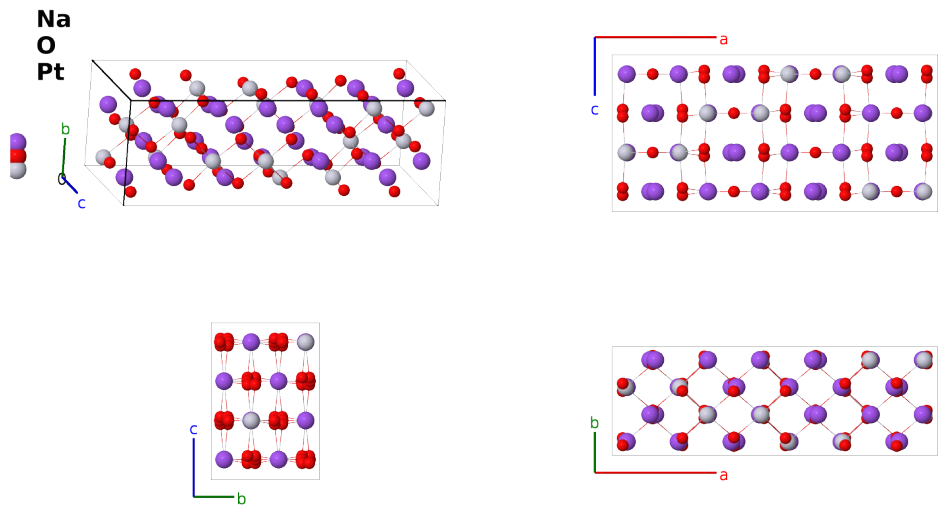
β -Na₂PtO₃ Structure: A2B3C_oF96_70_2e_fh_e-001

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<https://aflow.org/prototype-encyclopedia/7WUP>

https://aflow.org/prototype-encyclopedia/A2B3C_oF96_70_2e_fh_e-001



Prototype	Na ₂ O ₃ Pt
AFLOW prototype label	A2B3C_oF96_70_2e_fh_e-001
ICSD	25020
CCDC	1601011
Pearson symbol	oF96
Space group number	70
Space group symbol	<i>Fddd</i>
AFLOW prototype command	<code>aflow --proto=A2B3C_oF96_70_2e_fh_e-001</code> <code>--params=a, b/a, c/a, x₁, x₂, x₃, y₄, x₅, y₅, z₅</code>

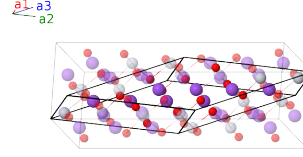
Other compounds with this structure

β -Li₂IrO₃, β -Na₂PrO₃

- Na₂PtO₃ can also be found in the α -Na₂PtO₃ phase, which has the Na₂PrO₃ structure.

Face-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= -(x_1 - \frac{1}{4})\mathbf{a}_1 + x_1\mathbf{a}_2 + x_1\mathbf{a}_3 =$	$ax_1\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_2$	$= x_1\mathbf{a}_1 - (x_1 - \frac{1}{4})\mathbf{a}_2 - (x_1 - \frac{1}{4})\mathbf{a}_3 =$	$-a(x_1 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_3$	$= (x_1 + \frac{3}{4})\mathbf{a}_1 - x_1\mathbf{a}_2 - x_1\mathbf{a}_3 =$	$-ax_1\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_4$	$= -x_1\mathbf{a}_1 + (x_1 + \frac{3}{4})\mathbf{a}_2 + (x_1 + \frac{3}{4})\mathbf{a}_3 =$	$a(x_1 + \frac{3}{4})\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_5$	$= -(x_2 - \frac{1}{4})\mathbf{a}_1 + x_2\mathbf{a}_2 + x_2\mathbf{a}_3 =$	$ax_2\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Na II
$\mathbf{B}_6$	$= x_2\mathbf{a}_1 - (x_2 - \frac{1}{4})\mathbf{a}_2 - (x_2 - \frac{1}{4})\mathbf{a}_3 =$	$-a(x_2 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Na II
$\mathbf{B}_7$	$= (x_2 + \frac{3}{4})\mathbf{a}_1 - x_2\mathbf{a}_2 - x_2\mathbf{a}_3 =$	$-ax_2\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Na II
$\mathbf{B}_8$	$= -x_2\mathbf{a}_1 + (x_2 + \frac{3}{4})\mathbf{a}_2 + (x_2 + \frac{3}{4})\mathbf{a}_3 =$	$a(x_2 + \frac{3}{4})\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Na II
$\mathbf{B}_9$	$= -(x_3 - \frac{1}{4})\mathbf{a}_1 + x_3\mathbf{a}_2 + x_3\mathbf{a}_3 =$	$ax_3\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Pt I
$\mathbf{B}_{10}$	$= x_3\mathbf{a}_1 - (x_3 - \frac{1}{4})\mathbf{a}_2 - (x_3 - \frac{1}{4})\mathbf{a}_3 =$	$-a(x_3 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Pt I
$\mathbf{B}_{11}$	$= (x_3 + \frac{3}{4})\mathbf{a}_1 - x_3\mathbf{a}_2 - x_3\mathbf{a}_3 =$	$-ax_3\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Pt I
$\mathbf{B}_{12}$	$= -x_3\mathbf{a}_1 + (x_3 + \frac{3}{4})\mathbf{a}_2 + (x_3 + \frac{3}{4})\mathbf{a}_3 =$	$a(x_3 + \frac{3}{4})\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Pt I
$\mathbf{B}_{13}$	$= y_4\mathbf{a}_1 - (y_4 - \frac{1}{4})\mathbf{a}_2 + y_4\mathbf{a}_3 =$	$\frac{1}{8}a\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16f)	O I
$\mathbf{B}_{14}$	$= -(y_4 - \frac{1}{4})\mathbf{a}_1 + y_4\mathbf{a}_2 - (y_4 - \frac{1}{4})\mathbf{a}_3 =$	$\frac{1}{8}a\hat{\mathbf{x}} - b(y_4 - \frac{1}{4})\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16f)	O I
$\mathbf{B}_{15}$	$= -y_4\mathbf{a}_1 + (y_4 + \frac{3}{4})\mathbf{a}_2 - y_4\mathbf{a}_3 =$	$\frac{3}{8}a\hat{\mathbf{x}} - by_4\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16f)	O I
$\mathbf{B}_{16}$	$= (y_4 + \frac{3}{4})\mathbf{a}_1 - y_4\mathbf{a}_2 + (y_4 + \frac{3}{4})\mathbf{a}_3 =$	$\frac{3}{8}a\hat{\mathbf{x}} + b(y_4 + \frac{3}{4})\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16f)	O I
$\mathbf{B}_{17}$	$= (-x_5 + y_5 + z_5)\mathbf{a}_1 + (x_5 - y_5 + z_5)\mathbf{a}_2 + (x_5 + y_5 - z_5)\mathbf{a}_3 =$	$ax_5\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(32h)	O II
$\mathbf{B}_{18}$	$= (x_5 - y_5 + z_5)\mathbf{a}_1 + (-x_5 + y_5 + z_5)\mathbf{a}_2 - (x_5 + y_5 + z_5 - \frac{1}{2})\mathbf{a}_3 =$	$-a(x_5 - \frac{1}{4})\hat{\mathbf{x}} - b(y_5 - \frac{1}{4})\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(32h)	O II
$\mathbf{B}_{19}$	$= (x_5 + y_5 - z_5)\mathbf{a}_1 - (x_5 + y_5 + z_5 - \frac{1}{2})\mathbf{a}_2 + (-x_5 + y_5 + z_5)\mathbf{a}_3 =$	$-a(x_5 - \frac{1}{4})\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} - c(z_5 - \frac{1}{4})\hat{\mathbf{z}}$	(32h)	O II
$\mathbf{B}_{20}$	$= -(x_5 + y_5 + z_5 - \frac{1}{2})\mathbf{a}_1 + (x_5 + y_5 - z_5)\mathbf{a}_2 + (x_5 - y_5 + z_5)\mathbf{a}_3 =$	$ax_5\hat{\mathbf{x}} - b(y_5 - \frac{1}{4})\hat{\mathbf{y}} - c(z_5 - \frac{1}{4})\hat{\mathbf{z}}$	(32h)	O II

$$\begin{aligned}
\mathbf{B}_{21} &= \begin{pmatrix} (x_5 - y_5 - z_5) \mathbf{a}_1 - \\ (x_5 - y_5 + z_5) \mathbf{a}_2 - \\ (x_5 + y_5 - z_5) \mathbf{a}_3 \end{pmatrix} = -ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (32h) & \text{O II} \\
\mathbf{B}_{22} &= \begin{pmatrix} -(x_5 - y_5 + z_5) \mathbf{a}_1 + \\ (x_5 - y_5 - z_5) \mathbf{a}_2 + \\ (x_5 + y_5 + z_5 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a \left(x_5 + \frac{1}{4}\right) \hat{\mathbf{x}} + b \left(y_5 + \frac{1}{4}\right) \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (32h) & \text{O II} \\
\mathbf{B}_{23} &= \begin{pmatrix} -(x_5 + y_5 - z_5) \mathbf{a}_1 + \\ (x_5 + y_5 + z_5 + \frac{1}{2}) \mathbf{a}_2 + \\ (x_5 - y_5 - z_5) \mathbf{a}_3 \end{pmatrix} = a \left(x_5 + \frac{1}{4}\right) \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + c \left(z_5 + \frac{1}{4}\right) \hat{\mathbf{z}} & (32h) & \text{O II} \\
\mathbf{B}_{24} &= \begin{pmatrix} (x_5 + y_5 + z_5 + \frac{1}{2}) \mathbf{a}_1 - \\ (x_5 + y_5 - z_5) \mathbf{a}_2 - \\ (x_5 - y_5 + z_5) \mathbf{a}_3 \end{pmatrix} = -ax_5 \hat{\mathbf{x}} + b \left(y_5 + \frac{1}{4}\right) \hat{\mathbf{y}} + c \left(z_5 + \frac{1}{4}\right) \hat{\mathbf{z}} & (32h) & \text{O II}
\end{aligned}$$

References

- [1] W. Urland and R. Hoppe, *Zur Kenntnis der Oxoplatinate Na_2PtO_2 , Na_2PtO_3 , " K_2PtO_3 " und " Rb_2PtO_3 "*, Z. Anorganische und Allgemeine Chemie **392**, 23–36 (1972), doi:10.1002/zaac.19723920104.

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