

Ca₃Al₂O₆ (*E*9₁) Structure: A2B3C6_cP33_221_cd_ag_fh-001

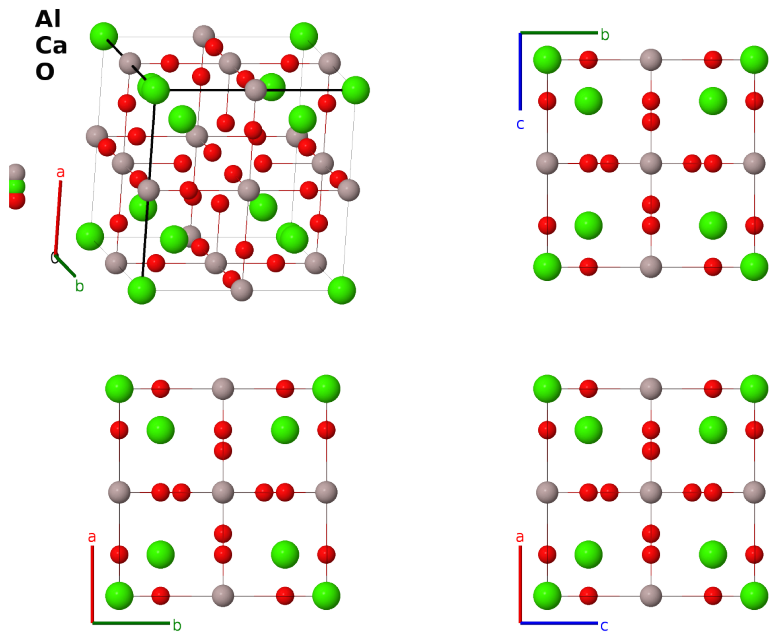
This structure previously used the label(s) **A2B3C6_cP33_221_cd_ag_fh**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/TZEN>

https://aflow.org/prototype-encyclopedia/A2B3C6_cP33_221_cd_ag_fh-001



Prototype	Al ₂ Ca ₃ O ₆
AFLOW prototype label	A2B3C6_cP33_221_cd_ag_fh-001
<i>Strukturbericht</i> designation	<i>E</i> 9 ₁
ICSD	151369
CCDC	1668204
Pearson symbol	cP33
Space group number	221
Space group symbol	<i>Pm</i> $\bar{3}$ <i>m</i>
AFLOW prototype command	<code>aflow --proto=A2B3C6_cP33_221_cd_ag_fh-001</code> <code>--params=<i>a</i>, <i>x</i>₄, <i>x</i>₅, <i>x</i>₆</code>

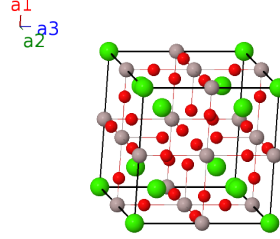
- (Steele, 1929) do not use the standard Wyckoff position notation to describe the atomic positions, so we use the parameters found in (Herman, 1937). An alternative description of the structure places the O-I atoms on the (6e) $(\pm x, 0, 0) \dots$ site rather than the (6f) site.
- (Mondal, 1975) reanalyzed this structure and concluded that the true structure was one where the lattice constant was doubled and contained 264 atoms. See the Ca3Al2O6 (A2B3C6.cP264.205.2d.ab2c2d.6d) structure page.

Simple Cubic primitive vectors

$$\mathbf{a}_1 = a \hat{\mathbf{x}}$$

$$\mathbf{a}_2 = a \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = a \hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1 =$	0	=	0	(1a)	Ca I
$\mathbf{B}_2 =$	$\frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(3c)	Al I
$\mathbf{B}_3 =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$	(3c)	Al I
$\mathbf{B}_4 =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	=	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(3c)	Al I
$\mathbf{B}_5 =$	$\frac{1}{2} \mathbf{a}_1$	=	$\frac{1}{2} a \hat{\mathbf{x}}$	(3d)	Al II
$\mathbf{B}_6 =$	$\frac{1}{2} \mathbf{a}_2$	=	$\frac{1}{2} a \hat{\mathbf{y}}$	(3d)	Al II
$\mathbf{B}_7 =$	$\frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{z}}$	(3d)	Al II
$\mathbf{B}_8 =$	$x_4 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$ax_4 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f)	O I
$\mathbf{B}_9 =$	$-x_4 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-ax_4 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f)	O I
$\mathbf{B}_{10} =$	$\frac{1}{2} \mathbf{a}_1 + x_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f)	O I
$\mathbf{B}_{11} =$	$\frac{1}{2} \mathbf{a}_1 - x_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f)	O I
$\mathbf{B}_{12} =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + x_4 \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(6f)	O I
$\mathbf{B}_{13} =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - x_4 \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(6f)	O I
$\mathbf{B}_{14} =$	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(8g)	Ca II
$\mathbf{B}_{15} =$	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(8g)	Ca II
$\mathbf{B}_{16} =$	$-x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(8g)	Ca II
$\mathbf{B}_{17} =$	$x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(8g)	Ca II
$\mathbf{B}_{18} =$	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(8g)	Ca II
$\mathbf{B}_{19} =$	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(8g)	Ca II
$\mathbf{B}_{20} =$	$x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(8g)	Ca II
$\mathbf{B}_{21} =$	$-x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(8g)	Ca II
$\mathbf{B}_{22} =$	$x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	=	$ax_6 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(12h)	O II
$\mathbf{B}_{23} =$	$-x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	=	$-ax_6 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(12h)	O II
$\mathbf{B}_{24} =$	$x_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$ax_6 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(12h)	O II

$$\begin{array}{llllll}
\mathbf{B}_{25} & = & -x_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3 & = & -ax_6 \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}} & (12h) \quad \text{O II} \\
\mathbf{B}_{26} & = & \frac{1}{2} \mathbf{a}_1 + x_6 \mathbf{a}_3 & = & \frac{1}{2}a \hat{\mathbf{x}} + ax_6 \hat{\mathbf{z}} & (12h) \quad \text{O II} \\
\mathbf{B}_{27} & = & \frac{1}{2} \mathbf{a}_1 - x_6 \mathbf{a}_3 & = & \frac{1}{2}a \hat{\mathbf{x}} - ax_6 \hat{\mathbf{z}} & (12h) \quad \text{O II} \\
\mathbf{B}_{28} & = & \frac{1}{2} \mathbf{a}_1 + x_6 \mathbf{a}_2 & = & \frac{1}{2}a \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} & (12h) \quad \text{O II} \\
\mathbf{B}_{29} & = & \frac{1}{2} \mathbf{a}_1 - x_6 \mathbf{a}_2 & = & \frac{1}{2}a \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} & (12h) \quad \text{O II} \\
\mathbf{B}_{30} & = & x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3 & = & ax_6 \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{z}} & (12h) \quad \text{O II} \\
\mathbf{B}_{31} & = & -x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3 & = & -ax_6 \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{z}} & (12h) \quad \text{O II} \\
\mathbf{B}_{32} & = & \frac{1}{2} \mathbf{a}_2 - x_6 \mathbf{a}_3 & = & \frac{1}{2}a \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}} & (12h) \quad \text{O II} \\
\mathbf{B}_{33} & = & \frac{1}{2} \mathbf{a}_2 + x_6 \mathbf{a}_3 & = & \frac{1}{2}a \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}} & (12h) \quad \text{O II}
\end{array}$$

References

- [1] F. A. Steele and W. P. Davey, *The Crystal Structure of Tricalcium Aluminate*, J. Am. Chem. Soc. **51**, 689–697 (1929), doi:10.1021/ja01383a001.
- [2] C. Hermann, O. Lohrmann, and H. Philipp, eds., *Strukturebericht Band II, 1928-1932* (Akademische Verlagsgesellschaft M. B. H, Leipzig, 1937).

Found in

- [1] P. Mondal and J. W. Jeffery, *The crystal structure of tricalcium aluminate, $\text{Ca}_3\text{Al}_2\text{O}_6$* , Acta Crystallogr. Sect. B **31**, 689–697 (1975), doi:10.1107/S0567740875003639.

First cited in

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