

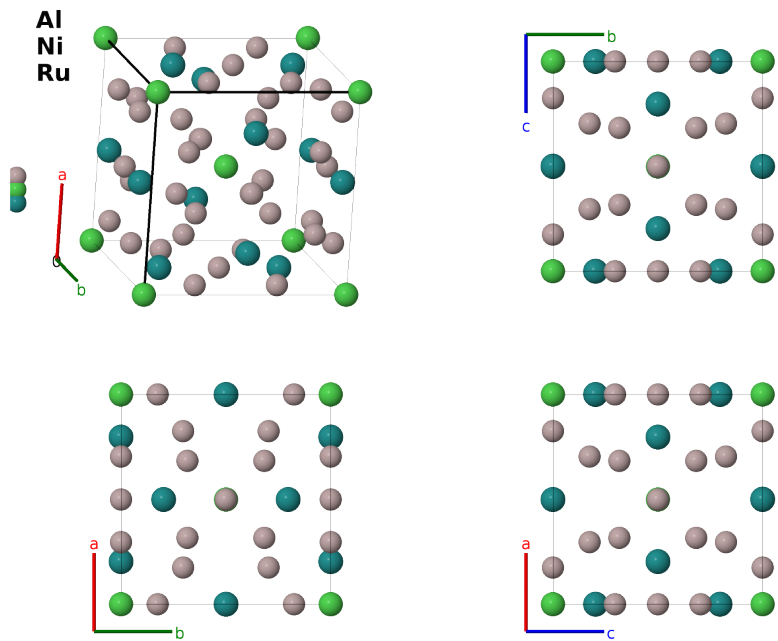
# C-AlRuNi (Al<sub>20</sub>Ni<sub>3</sub>Ru<sub>5</sub>) Structure: A23B2C6\_cP31\_200\_cij\_ab\_f-001

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- D. Hicks, M. J. Mehl, M. Esters, C. Osos, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/L1EN>

[https://aflow.org/prototype-encyclopedia/A23B2C6\\_cP31\\_200\\_cij\\_ab\\_f-001](https://aflow.org/prototype-encyclopedia/A23B2C6_cP31_200_cij_ab_f-001)



|                         |                                                                                                                                                 |
|-------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------|
| Prototype               | Al <sub>20</sub> Ni <sub>3</sub> Ru <sub>5</sub>                                                                                                |
| AFLOW prototype label   | A23B2C6_cP31_200_cij_ab_f-001                                                                                                                   |
| ICSD                    | 230569                                                                                                                                          |
| CCDC                    | 2037181                                                                                                                                         |
| Pearson symbol          | cP31                                                                                                                                            |
| Space group number      | 200                                                                                                                                             |
| Space group symbol      | $Pm\bar{3}$                                                                                                                                     |
| AFLOW prototype command | <code>aflow --proto=A23B2C6_cP31_200_cij_ab_f-001</code><br><code>--params=a, x<sub>4</sub>, x<sub>5</sub>, y<sub>6</sub>, z<sub>6</sub></code> |

- Most of these sites are partially or contained a mixture of species. We label them by the majority species:
  - Ni-I (1a) is 79% nickel and 21% ruthenium,
  - Ni-II (1b) is 100% nickel,

- Al-I (3c) is 77% aluminum and 23% vacancies,
- Ru-I (6g) is 81.4% ruthenium and 18.6% nickel,
- Al-II (8i) is 74% aluminum and 26% vacancies, and
- Al-III (12k) is 100% aluminum.

- This gives an actual composition of  $\text{Al}_{20.23}\text{Ni}_{2.906}\text{Ru}_{5.094}$ , which we simplify to  $\text{Al}_{20}\text{Ni}_3\text{Ru}_5$ .

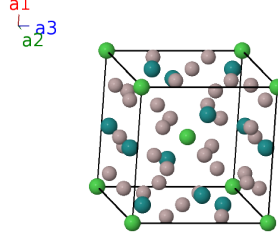
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### Simple Cubic primitive vectors

$$\mathbf{a}_1 = a \hat{\mathbf{x}}$$

$$\mathbf{a}_2 = a \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = a \hat{\mathbf{z}}$$




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### Basis vectors

|                   | Lattice<br>coordinates |                                                                                  | Cartesian<br>coordinates | Wyckoff<br>position                                                                                | Atom<br>type |
|-------------------|------------------------|----------------------------------------------------------------------------------|--------------------------|----------------------------------------------------------------------------------------------------|--------------|
| $\mathbf{B}_1$    | $=$                    | $0$                                                                              | $=$                      | $0$                                                                                                | (1a) Ni I    |
| $\mathbf{B}_2$    | $=$                    | $\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$ | $=$                      | $\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$ | (1b) Ni II   |
| $\mathbf{B}_3$    | $=$                    | $\frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$                            | $=$                      | $\frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$                                  | (3c) Al I    |
| $\mathbf{B}_4$    | $=$                    | $\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$                            | $=$                      | $\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$                                  | (3c) Al I    |
| $\mathbf{B}_5$    | $=$                    | $\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$                            | $=$                      | $\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$                                  | (3c) Al I    |
| $\mathbf{B}_6$    | $=$                    | $x_4 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$                                    | $=$                      | $ax_4 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$                                           | (6f) Ru I    |
| $\mathbf{B}_7$    | $=$                    | $-x_4 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$                                   | $=$                      | $-ax_4 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$                                          | (6f) Ru I    |
| $\mathbf{B}_8$    | $=$                    | $\frac{1}{2} \mathbf{a}_1 + x_4 \mathbf{a}_2$                                    | $=$                      | $\frac{1}{2} a \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}}$                                           | (6f) Ru I    |
| $\mathbf{B}_9$    | $=$                    | $\frac{1}{2} \mathbf{a}_1 - x_4 \mathbf{a}_2$                                    | $=$                      | $\frac{1}{2} a \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}}$                                           | (6f) Ru I    |
| $\mathbf{B}_{10}$ | $=$                    | $\frac{1}{2} \mathbf{a}_2 + x_4 \mathbf{a}_3$                                    | $=$                      | $\frac{1}{2} a \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$                                           | (6f) Ru I    |
| $\mathbf{B}_{11}$ | $=$                    | $\frac{1}{2} \mathbf{a}_2 - x_4 \mathbf{a}_3$                                    | $=$                      | $\frac{1}{2} a \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$                                           | (6f) Ru I    |
| $\mathbf{B}_{12}$ | $=$                    | $x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$                         | $=$                      | $ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$                            | (8i) Al II   |
| $\mathbf{B}_{13}$ | $=$                    | $-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$                        | $=$                      | $-ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$                           | (8i) Al II   |
| $\mathbf{B}_{14}$ | $=$                    | $-x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$                        | $=$                      | $-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$                           | (8i) Al II   |
| $\mathbf{B}_{15}$ | $=$                    | $x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$                         | $=$                      | $ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$                            | (8i) Al II   |
| $\mathbf{B}_{16}$ | $=$                    | $-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$                        | $=$                      | $-ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$                           | (8i) Al II   |
| $\mathbf{B}_{17}$ | $=$                    | $x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$                         | $=$                      | $ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$                            | (8i) Al II   |
| $\mathbf{B}_{18}$ | $=$                    | $x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$                         | $=$                      | $ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$                            | (8i) Al II   |
| $\mathbf{B}_{19}$ | $=$                    | $-x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$                        | $=$                      | $-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$                           | (8i) Al II   |
| $\mathbf{B}_{20}$ | $=$                    | $y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$                                            | $=$                      | $ay_6 \hat{\mathbf{y}} + az_6 \hat{\mathbf{z}}$                                                    | (12j) Al III |
| $\mathbf{B}_{21}$ | $=$                    | $-y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$                                           | $=$                      | $-ay_6 \hat{\mathbf{y}} + az_6 \hat{\mathbf{z}}$                                                   | (12j) Al III |
| $\mathbf{B}_{22}$ | $=$                    | $y_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$                                            | $=$                      | $ay_6 \hat{\mathbf{y}} - az_6 \hat{\mathbf{z}}$                                                    | (12j) Al III |
| $\mathbf{B}_{23}$ | $=$                    | $-y_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$                                           | $=$                      | $-ay_6 \hat{\mathbf{y}} - az_6 \hat{\mathbf{z}}$                                                   | (12j) Al III |

|                   |     |                                        |     |                                                  |         |        |
|-------------------|-----|----------------------------------------|-----|--------------------------------------------------|---------|--------|
| $\mathbf{B}_{24}$ | $=$ | $z_6 \mathbf{a}_1 + y_6 \mathbf{a}_3$  | $=$ | $az_6 \hat{\mathbf{x}} + ay_6 \hat{\mathbf{z}}$  | $(12j)$ | Al III |
| $\mathbf{B}_{25}$ | $=$ | $z_6 \mathbf{a}_1 - y_6 \mathbf{a}_3$  | $=$ | $az_6 \hat{\mathbf{x}} - ay_6 \hat{\mathbf{z}}$  | $(12j)$ | Al III |
| $\mathbf{B}_{26}$ | $=$ | $-z_6 \mathbf{a}_1 + y_6 \mathbf{a}_3$ | $=$ | $-az_6 \hat{\mathbf{x}} + ay_6 \hat{\mathbf{z}}$ | $(12j)$ | Al III |
| $\mathbf{B}_{27}$ | $=$ | $-z_6 \mathbf{a}_1 - y_6 \mathbf{a}_3$ | $=$ | $-az_6 \hat{\mathbf{x}} - ay_6 \hat{\mathbf{z}}$ | $(12j)$ | Al III |
| $\mathbf{B}_{28}$ | $=$ | $y_6 \mathbf{a}_1 + z_6 \mathbf{a}_2$  | $=$ | $ay_6 \hat{\mathbf{x}} + az_6 \hat{\mathbf{y}}$  | $(12j)$ | Al III |
| $\mathbf{B}_{29}$ | $=$ | $-y_6 \mathbf{a}_1 + z_6 \mathbf{a}_2$ | $=$ | $-ay_6 \hat{\mathbf{x}} + az_6 \hat{\mathbf{y}}$ | $(12j)$ | Al III |
| $\mathbf{B}_{30}$ | $=$ | $y_6 \mathbf{a}_1 - z_6 \mathbf{a}_2$  | $=$ | $ay_6 \hat{\mathbf{x}} - az_6 \hat{\mathbf{y}}$  | $(12j)$ | Al III |
| $\mathbf{B}_{31}$ | $=$ | $-y_6 \mathbf{a}_1 - z_6 \mathbf{a}_2$ | $=$ | $-ay_6 \hat{\mathbf{x}} - az_6 \hat{\mathbf{y}}$ | $(12j)$ | Al III |

## References

- [1] R. Simura, K. Sugiyama, S. Suzuki, and T. Kawamata, *Crystal Structure of the C-AlRuNi Phase*, Mater. Trans. **58**, 1101–1105 (2017), doi:10.2320/matertrans.M2017106.

## First cited in

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