

Monoclinic Nb₁₂O₂₉ Structure:

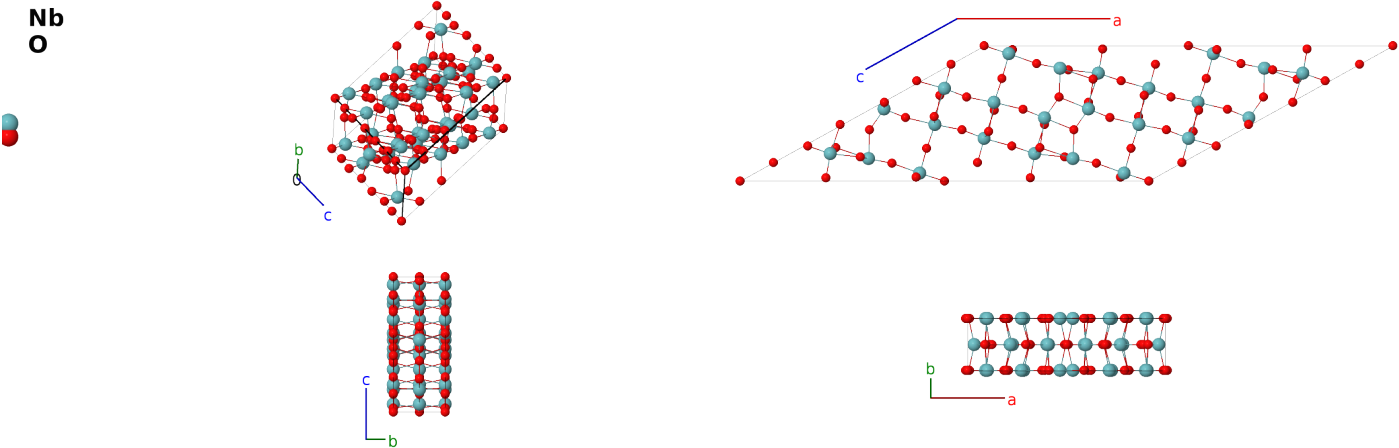
A12B29_mC82_12_6i_a14i-001

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<https://aflow.org/prototype-encyclopedia/BPW1>

https://aflow.org/prototype-encyclopedia/A12B29_mC82_12_6i_a14i-001



Prototype	Nb ₁₂ O ₂₉
AFLOW prototype label	A12B29_mC82_12_6i_a14i-001
ICSD	24111
CCDC	1600160
Pearson symbol	mC82
Space group number	12
Space group symbol	<i>C</i> 2/ <i>m</i>
AFLOW prototype command	<code>aflow --proto=A12B29_mC82_12_6i_a14i-001</code> <code>--params=a,b/a,c/a,β,x₂,z₂,x₃,z₃,x₄,z₄,x₅,z₅,x₆,z₆,x₇,z₇,x₈,z₈,x₉,z₉,x₁₀,z₁₀,x₁₁,z₁₁,x₁₂,z₁₂,x₁₃,z₁₃,x₁₄,z₁₄,x₁₅,z₁₅,x₁₆,z₁₆,x₁₇,z₁₇,x₁₈,z₁₈,x₁₉,z₁₉,x₂₀,z₂₀,x₂₁,z₂₁</code>

Other compounds with this structure

Ti₂Nb₁₀O₂₉

- Nb₁₂O₂₉ is known to exist in a least two phases (Norin, 1963; Norin, 1966):
 - a monoclinic phase (this structure) and
 - an orthorhombic phase.
- (Wadsley, 1961) earlier found that both known phases of Ti₂Nb₁₂O₂₉ are isostructural with the corresponding Nb₁₂O₂₉ phase, but as the titanium and niobium atoms are alloyed on the same site we use the binary Nb₁₂O₂₉ as the prototype.

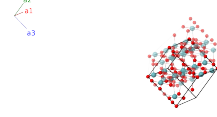
- (Norin, 1966) gives the structure of orthorhombic Nb₁₂O₂₉ in the *A2/a* setting of space group #15, with the origin at -1 on the *a*-glide plane. We when we checked this with FINDSYM we found that the structure could be placed in space group *C2/m* #12 with a unit cell half that found by (Norin, 1966), and close to the dimensions of the cell found in (Wadsley, 1961) and (Norin, 1963).

Base-centered Monoclinic primitive vectors

$$\mathbf{a}_1 = \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}}$$

$$\mathbf{a}_2 = \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = c \cos \beta \hat{\mathbf{x}} + c \sin \beta \hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	0	$=$	0	(2a) O I
$\mathbf{B}_2$	$=$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$(ax_2 + cz_2 \cos \beta) \hat{\mathbf{x}} + cz_2 \sin \beta \hat{\mathbf{z}}$	(4i) Nb I
$\mathbf{B}_3$	$=$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - z_2 \mathbf{a}_3$	$=$	$-(ax_2 + cz_2 \cos \beta) \hat{\mathbf{x}} - cz_2 \sin \beta \hat{\mathbf{z}}$	(4i) Nb I
$\mathbf{B}_4$	$=$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$(ax_3 + cz_3 \cos \beta) \hat{\mathbf{x}} + cz_3 \sin \beta \hat{\mathbf{z}}$	(4i) Nb II
$\mathbf{B}_5$	$=$	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$-(ax_3 + cz_3 \cos \beta) \hat{\mathbf{x}} - cz_3 \sin \beta \hat{\mathbf{z}}$	(4i) Nb II
$\mathbf{B}_6$	$=$	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$(ax_4 + cz_4 \cos \beta) \hat{\mathbf{x}} + cz_4 \sin \beta \hat{\mathbf{z}}$	(4i) Nb III
$\mathbf{B}_7$	$=$	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - z_4 \mathbf{a}_3$	$=$	$-(ax_4 + cz_4 \cos \beta) \hat{\mathbf{x}} - cz_4 \sin \beta \hat{\mathbf{z}}$	(4i) Nb III
$\mathbf{B}_8$	$=$	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} + cz_5 \sin \beta \hat{\mathbf{z}}$	(4i) Nb IV
$\mathbf{B}_9$	$=$	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$-(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} - cz_5 \sin \beta \hat{\mathbf{z}}$	(4i) Nb IV
$\mathbf{B}_{10}$	$=$	$x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$(ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} + cz_6 \sin \beta \hat{\mathbf{z}}$	(4i) Nb V
$\mathbf{B}_{11}$	$=$	$-x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$-(ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} - cz_6 \sin \beta \hat{\mathbf{z}}$	(4i) Nb V
$\mathbf{B}_{12}$	$=$	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} + cz_7 \sin \beta \hat{\mathbf{z}}$	(4i) Nb VI
$\mathbf{B}_{13}$	$=$	$-x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$-(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} - cz_7 \sin \beta \hat{\mathbf{z}}$	(4i) Nb VI
$\mathbf{B}_{14}$	$=$	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + cz_8 \sin \beta \hat{\mathbf{z}}$	(4i) O II
$\mathbf{B}_{15}$	$=$	$-x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$-(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} - cz_8 \sin \beta \hat{\mathbf{z}}$	(4i) O II
$\mathbf{B}_{16}$	$=$	$x_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} + cz_9 \sin \beta \hat{\mathbf{z}}$	(4i) O III
$\mathbf{B}_{17}$	$=$	$-x_9 \mathbf{a}_1 - x_9 \mathbf{a}_2 - z_9 \mathbf{a}_3$	$=$	$-(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} - cz_9 \sin \beta \hat{\mathbf{z}}$	(4i) O III
$\mathbf{B}_{18}$	$=$	$x_{10} \mathbf{a}_1 + x_{10} \mathbf{a}_2 + z_{10} \mathbf{a}_3$	$=$	$(ax_{10} + cz_{10} \cos \beta) \hat{\mathbf{x}} + cz_{10} \sin \beta \hat{\mathbf{z}}$	(4i) O IV
$\mathbf{B}_{19}$	$=$	$-x_{10} \mathbf{a}_1 - x_{10} \mathbf{a}_2 - z_{10} \mathbf{a}_3$	$=$	$-(ax_{10} + cz_{10} \cos \beta) \hat{\mathbf{x}} - cz_{10} \sin \beta \hat{\mathbf{z}}$	(4i) O IV
$\mathbf{B}_{20}$	$=$	$x_{11} \mathbf{a}_1 + x_{11} \mathbf{a}_2 + z_{11} \mathbf{a}_3$	$=$	$(ax_{11} + cz_{11} \cos \beta) \hat{\mathbf{x}} + cz_{11} \sin \beta \hat{\mathbf{z}}$	(4i) O V
$\mathbf{B}_{21}$	$=$	$-x_{11} \mathbf{a}_1 - x_{11} \mathbf{a}_2 - z_{11} \mathbf{a}_3$	$=$	$-(ax_{11} + cz_{11} \cos \beta) \hat{\mathbf{x}} - cz_{11} \sin \beta \hat{\mathbf{z}}$	(4i) O V
$\mathbf{B}_{22}$	$=$	$x_{12} \mathbf{a}_1 + x_{12} \mathbf{a}_2 + z_{12} \mathbf{a}_3$	$=$	$(ax_{12} + cz_{12} \cos \beta) \hat{\mathbf{x}} + cz_{12} \sin \beta \hat{\mathbf{z}}$	(4i) O VI
$\mathbf{B}_{23}$	$=$	$-x_{12} \mathbf{a}_1 - x_{12} \mathbf{a}_2 - z_{12} \mathbf{a}_3$	$=$	$-(ax_{12} + cz_{12} \cos \beta) \hat{\mathbf{x}} - cz_{12} \sin \beta \hat{\mathbf{z}}$	(4i) O VI
$\mathbf{B}_{24}$	$=$	$x_{13} \mathbf{a}_1 + x_{13} \mathbf{a}_2 + z_{13} \mathbf{a}_3$	$=$	$(ax_{13} + cz_{13} \cos \beta) \hat{\mathbf{x}} + cz_{13} \sin \beta \hat{\mathbf{z}}$	(4i) O VII
$\mathbf{B}_{25}$	$=$	$-x_{13} \mathbf{a}_1 - x_{13} \mathbf{a}_2 - z_{13} \mathbf{a}_3$	$=$	$-(ax_{13} + cz_{13} \cos \beta) \hat{\mathbf{x}} - cz_{13} \sin \beta \hat{\mathbf{z}}$	(4i) O VII
$\mathbf{B}_{26}$	$=$	$x_{14} \mathbf{a}_1 + x_{14} \mathbf{a}_2 + z_{14} \mathbf{a}_3$	$=$	$(ax_{14} + cz_{14} \cos \beta) \hat{\mathbf{x}} + cz_{14} \sin \beta \hat{\mathbf{z}}$	(4i) O VIII
$\mathbf{B}_{27}$	$=$	$-x_{14} \mathbf{a}_1 - x_{14} \mathbf{a}_2 - z_{14} \mathbf{a}_3$	$=$	$-(ax_{14} + cz_{14} \cos \beta) \hat{\mathbf{x}} - cz_{14} \sin \beta \hat{\mathbf{z}}$	(4i) O VIII
$\mathbf{B}_{28}$	$=$	$x_{15} \mathbf{a}_1 + x_{15} \mathbf{a}_2 + z_{15} \mathbf{a}_3$	$=$	$(ax_{15} + cz_{15} \cos \beta) \hat{\mathbf{x}} + cz_{15} \sin \beta \hat{\mathbf{z}}$	(4i) O IX
$\mathbf{B}_{29}$	$=$	$-x_{15} \mathbf{a}_1 - x_{15} \mathbf{a}_2 - z_{15} \mathbf{a}_3$	$=$	$-(ax_{15} + cz_{15} \cos \beta) \hat{\mathbf{x}} - cz_{15} \sin \beta \hat{\mathbf{z}}$	(4i) O IX
$\mathbf{B}_{30}$	$=$	$x_{16} \mathbf{a}_1 + x_{16} \mathbf{a}_2 + z_{16} \mathbf{a}_3$	$=$	$(ax_{16} + cz_{16} \cos \beta) \hat{\mathbf{x}} + cz_{16} \sin \beta \hat{\mathbf{z}}$	(4i) O X

$\mathbf{B}_{31}$	$=$	$-x_{16} \mathbf{a}_1 - x_{16} \mathbf{a}_2 - z_{16} \mathbf{a}_3$	$=$	$-(ax_{16} + cz_{16} \cos \beta) \hat{\mathbf{x}} - cz_{16} \sin \beta \hat{\mathbf{z}}$	(4i)	O X
$\mathbf{B}_{32}$	$=$	$x_{17} \mathbf{a}_1 + x_{17} \mathbf{a}_2 + z_{17} \mathbf{a}_3$	$=$	$(ax_{17} + cz_{17} \cos \beta) \hat{\mathbf{x}} + cz_{17} \sin \beta \hat{\mathbf{z}}$	(4i)	O XI
$\mathbf{B}_{33}$	$=$	$-x_{17} \mathbf{a}_1 - x_{17} \mathbf{a}_2 - z_{17} \mathbf{a}_3$	$=$	$-(ax_{17} + cz_{17} \cos \beta) \hat{\mathbf{x}} - cz_{17} \sin \beta \hat{\mathbf{z}}$	(4i)	O XI
$\mathbf{B}_{34}$	$=$	$x_{18} \mathbf{a}_1 + x_{18} \mathbf{a}_2 + z_{18} \mathbf{a}_3$	$=$	$(ax_{18} + cz_{18} \cos \beta) \hat{\mathbf{x}} + cz_{18} \sin \beta \hat{\mathbf{z}}$	(4i)	O XII
$\mathbf{B}_{35}$	$=$	$-x_{18} \mathbf{a}_1 - x_{18} \mathbf{a}_2 - z_{18} \mathbf{a}_3$	$=$	$-(ax_{18} + cz_{18} \cos \beta) \hat{\mathbf{x}} - cz_{18} \sin \beta \hat{\mathbf{z}}$	(4i)	O XII
$\mathbf{B}_{36}$	$=$	$x_{19} \mathbf{a}_1 + x_{19} \mathbf{a}_2 + z_{19} \mathbf{a}_3$	$=$	$(ax_{19} + cz_{19} \cos \beta) \hat{\mathbf{x}} + cz_{19} \sin \beta \hat{\mathbf{z}}$	(4i)	O XIII
$\mathbf{B}_{37}$	$=$	$-x_{19} \mathbf{a}_1 - x_{19} \mathbf{a}_2 - z_{19} \mathbf{a}_3$	$=$	$-(ax_{19} + cz_{19} \cos \beta) \hat{\mathbf{x}} - cz_{19} \sin \beta \hat{\mathbf{z}}$	(4i)	O XIII
$\mathbf{B}_{38}$	$=$	$x_{20} \mathbf{a}_1 + x_{20} \mathbf{a}_2 + z_{20} \mathbf{a}_3$	$=$	$(ax_{20} + cz_{20} \cos \beta) \hat{\mathbf{x}} + cz_{20} \sin \beta \hat{\mathbf{z}}$	(4i)	O XIV
$\mathbf{B}_{39}$	$=$	$-x_{20} \mathbf{a}_1 - x_{20} \mathbf{a}_2 - z_{20} \mathbf{a}_3$	$=$	$-(ax_{20} + cz_{20} \cos \beta) \hat{\mathbf{x}} - cz_{20} \sin \beta \hat{\mathbf{z}}$	(4i)	O XIV
$\mathbf{B}_{40}$	$=$	$x_{21} \mathbf{a}_1 + x_{21} \mathbf{a}_2 + z_{21} \mathbf{a}_3$	$=$	$(ax_{21} + cz_{21} \cos \beta) \hat{\mathbf{x}} + cz_{21} \sin \beta \hat{\mathbf{z}}$	(4i)	O XV
$\mathbf{B}_{41}$	$=$	$-x_{21} \mathbf{a}_1 - x_{21} \mathbf{a}_2 - z_{21} \mathbf{a}_3$	$=$	$-(ax_{21} + cz_{21} \cos \beta) \hat{\mathbf{x}} - cz_{21} \sin \beta \hat{\mathbf{z}}$	(4i)	O XV

References

- [1] R. Norin, *The Crystal Structure of $\text{Nb}_{12}\text{O}_{29}$ (*o-rh*)*, Acta Chem. Scand. **17**, 1391–1404 (1963), doi:10.3891/acta.chem.scand.17-1391.
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- [3] A. D. Wadsley, *Mixed oxides of titanium and niobium. II. The crystal structures of the dimorphic forms $\text{Ti}_2\text{Nb}_{10}\text{O}_{29}$* , Acta Cryst. **14**, 664–670 (1961), doi:10.1107/S0365110X6100200X.

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