

γ -Ga₂O₃ Structure: A11B4_cF120_227_acdf_e-001

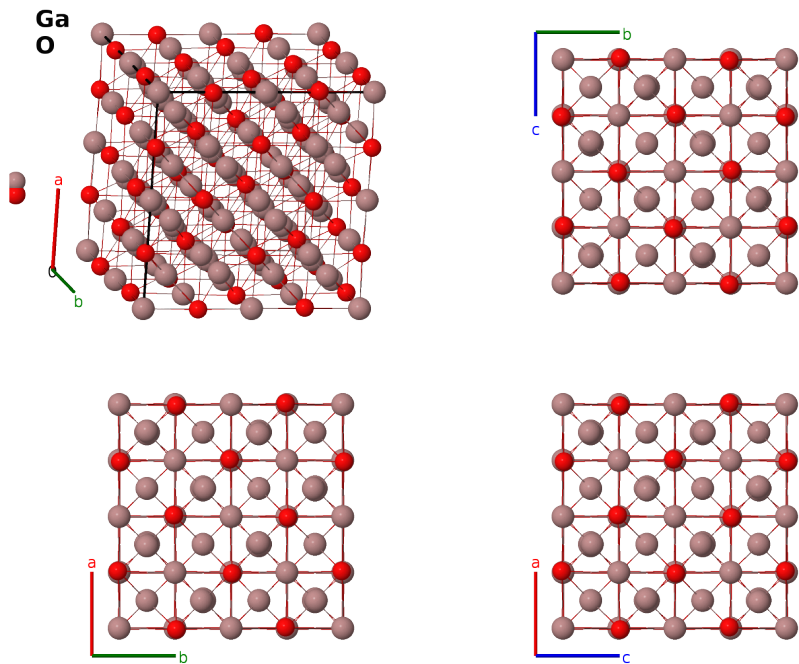
This structure previously used the label(s) **A11B4_cF120_227_acdf_e**. Calls to these addresses will be redirected here.

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<https://aflow.org/prototype-encyclopedia/VTDR>

https://aflow.org/prototype-encyclopedia/A11B4_cF120_227_acdf_e-001



Prototype	Ga ₂ O ₃
AFLOW prototype label	A11B4_cF120_227_acdf_e-001
ICSD	236276
CCDC	1707890
Pearson symbol	cF120
Space group number	227
Space group symbol	$Fd\bar{3}m$
AFLOW prototype command	<code>aflow --proto=A11B4_cF120_227_acdf_e-001</code> <code>--params=a, x_4, x_5</code>

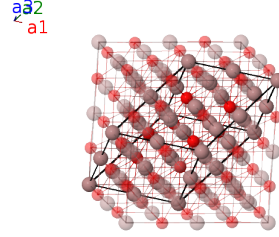
- Ga₂O₃ exhibits a variety of structures:

- $\alpha\text{Ga}_2\text{O}_3$, which has the corundum ($D5_1$) structure ,
- $\beta\text{Ga}_2\text{O}_3$,
- $\gamma\text{Ga}_2\text{O}_3$, this structure, and
- $\epsilon\text{Ga}_2\text{O}_3$, a structure with many vacancies which can be approximated by the κ alumina structure.

- In $\gamma\text{Ga}_2\text{O}_3$ none of the gallium sites have full occupancy. Ga-I and Ga-II are 74.1% occupied, Ga-III is 6.6% occupied, and Ga-IV is only 2.4% occupied.

Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{1}{8}\mathbf{a}_1 + \frac{1}{8}\mathbf{a}_2 + \frac{1}{8}\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(8a)	Ga I
$\mathbf{B}_2$	$= \frac{7}{8}\mathbf{a}_1 + \frac{7}{8}\mathbf{a}_2 + \frac{7}{8}\mathbf{a}_3$	$=$	$\frac{7}{8}a\hat{\mathbf{x}} + \frac{7}{8}a\hat{\mathbf{y}} + \frac{7}{8}a\hat{\mathbf{z}}$	(8a)	Ga I
$\mathbf{B}_3$	$= 0$	$=$	0	(16c)	Ga II
$\mathbf{B}_4$	$= \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}}$	(16c)	Ga II
$\mathbf{B}_5$	$= \frac{1}{2}\mathbf{a}_2$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16c)	Ga II
$\mathbf{B}_6$	$= \frac{1}{2}\mathbf{a}_1$	$=$	$\frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16c)	Ga II
$\mathbf{B}_7$	$= \frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}}$	(16d)	Ga III
$\mathbf{B}_8$	$= \frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}}$	(16d)	Ga III
$\mathbf{B}_9$	$= \frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16d)	Ga III
$\mathbf{B}_{10}$	$= \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16d)	Ga III
$\mathbf{B}_{11}$	$= x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	$=$	$ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{12}$	$= x_4\mathbf{a}_1 + x_4\mathbf{a}_2 - (3x_4 - \frac{1}{2})\mathbf{a}_3$	$=$	$-a(x_4 - \frac{1}{4})\hat{\mathbf{x}} - a(x_4 - \frac{1}{4})\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{13}$	$= x_4\mathbf{a}_1 - (3x_4 - \frac{1}{2})\mathbf{a}_2 + x_4\mathbf{a}_3$	$=$	$-a(x_4 - \frac{1}{4})\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - a(x_4 - \frac{1}{4})\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{14}$	$= -(3x_4 - \frac{1}{2})\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	$=$	$ax_4\hat{\mathbf{x}} - a(x_4 - \frac{1}{4})\hat{\mathbf{y}} - a(x_4 - \frac{1}{4})\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{15}$	$= -x_4\mathbf{a}_1 - x_4\mathbf{a}_2 + (3x_4 + \frac{1}{2})\mathbf{a}_3$	$=$	$a(x_4 + \frac{1}{4})\hat{\mathbf{x}} + a(x_4 + \frac{1}{4})\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{16}$	$= -x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$	$=$	$-ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{17}$	$= -x_4\mathbf{a}_1 + (3x_4 + \frac{1}{2})\mathbf{a}_2 - x_4\mathbf{a}_3$	$=$	$a(x_4 + \frac{1}{4})\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} + a(x_4 + \frac{1}{4})\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{18}$	$= (3x_4 + \frac{1}{2})\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$	$=$	$-ax_4\hat{\mathbf{x}} + a(x_4 + \frac{1}{4})\hat{\mathbf{y}} + a(x_4 + \frac{1}{4})\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{19}$	$= -(x_5 - \frac{1}{4})\mathbf{a}_1 + x_5\mathbf{a}_2 + x_5\mathbf{a}_3$	$=$	$ax_5\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	Ga IV
$\mathbf{B}_{20}$	$= x_5\mathbf{a}_1 - (x_5 - \frac{1}{4})\mathbf{a}_2 - (x_5 - \frac{1}{4})\mathbf{a}_3$	$=$	$-a(x_5 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	Ga IV
$\mathbf{B}_{21}$	$= x_5\mathbf{a}_1 - (x_5 - \frac{1}{4})\mathbf{a}_2 + x_5\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	Ga IV

$$\begin{aligned}
\mathbf{B}_{22} &= -\left(x_5 - \frac{1}{4}\right) \mathbf{a}_1 + x_5 \mathbf{a}_2 - \left(x_5 - \frac{1}{4}\right) \mathbf{a}_3 = \frac{1}{8}a \hat{\mathbf{x}} - a \left(x_5 - \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{1}{8}a \hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{23} &= x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - \left(x_5 - \frac{1}{4}\right) \mathbf{a}_3 = \frac{1}{8}a \hat{\mathbf{x}} + \frac{1}{8}a \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{24} &= -\left(x_5 - \frac{1}{4}\right) \mathbf{a}_1 - \left(x_5 - \frac{1}{4}\right) \mathbf{a}_2 + x_5 \mathbf{a}_3 = \frac{1}{8}a \hat{\mathbf{x}} + \frac{1}{8}a \hat{\mathbf{y}} - a \left(x_5 - \frac{1}{4}\right) \hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{25} &= \left(x_5 + \frac{3}{4}\right) \mathbf{a}_1 - x_5 \mathbf{a}_2 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_3 = \frac{3}{8}a \hat{\mathbf{x}} + a \left(x_5 + \frac{3}{4}\right) \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{26} &= -x_5 \mathbf{a}_1 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_2 - x_5 \mathbf{a}_3 = \frac{3}{8}a \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{27} &= -x_5 \mathbf{a}_1 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_2 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_3 = a \left(x_5 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{28} &= \left(x_5 + \frac{3}{4}\right) \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3 = -ax_5 \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{29} &= -x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_3 = \frac{3}{8}a \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{30} &= \left(x_5 + \frac{3}{4}\right) \mathbf{a}_1 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_2 - x_5 \mathbf{a}_3 = \frac{3}{8}a \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} + a \left(x_5 + \frac{3}{4}\right) \hat{\mathbf{z}} & (48f) & \text{Ga IV}
\end{aligned}$$

References

- [1] H. Y. Playford, A. C. Hannon, E. R. Barney, and R. I. Walton, *Structures of Uncharacterised Polymorphs of Gallium Oxide from Total Neutron Diffraction*, Chem. Euro. J. **19**, 2803–2813 (2013), doi:10.1002/chem.201203359.

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