

Al₁₀V Structure:

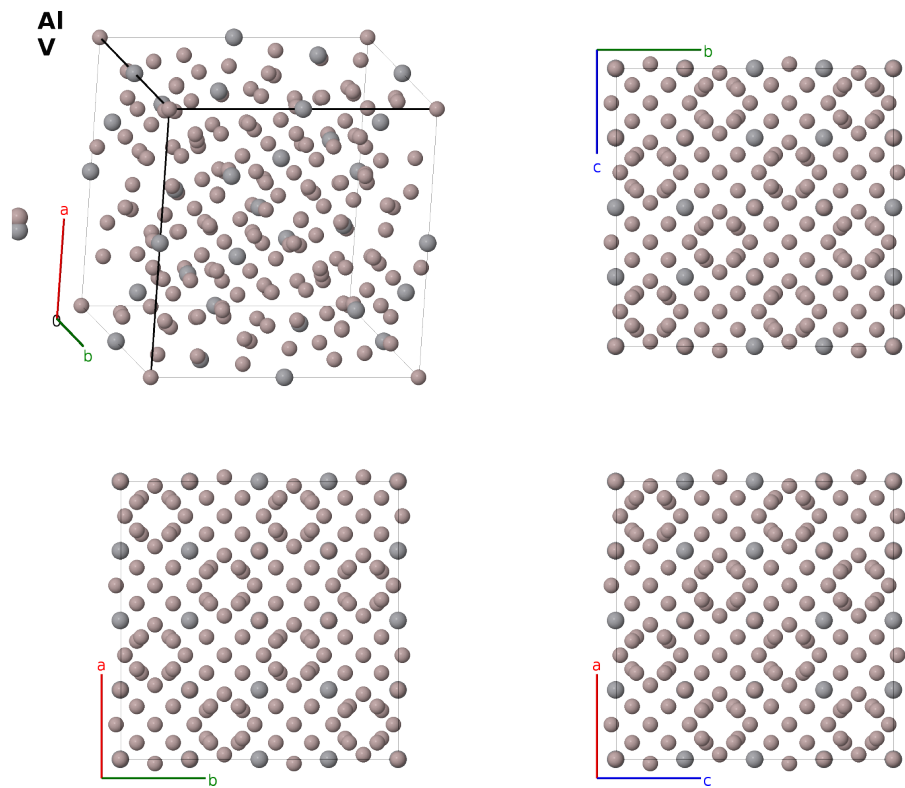
A10B_cF176_227_cfg_d-001

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- D. Hicks, M. J. Mehl, M. Esters, C. Osos, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/WWX6>

https://aflow.org/prototype-encyclopedia/A10B_cF176_227_cfg_d-001

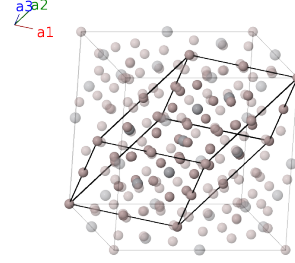


Prototype	Al ₁₀ V
AFLOW prototype label	A10B_cF176_227_cfg_d-001
ICSD	58202
CCDC	1622230
Pearson symbol	cF176
Space group number	227
Space group symbol	$Fd\bar{3}m$
AFLOW prototype command	<code>aflow --proto=A10B_cF176_227_cfg_d-001</code> <code>--params=a, x_3, x_4, z_4</code>

- (Brown, 1957) gives the structural information in setting 1 of space group $Fd\bar{3}m$ #227. We shifted the origin by $(a/8, a/8, a/8)$ to change this to the standard setting 2.

Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	=	0	=	0	(16c) Al I
$\mathbf{B}_2$	=	$\frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}}$	(16c) Al I
$\mathbf{B}_3$	=	$\frac{1}{2}\mathbf{a}_2$	=	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16c) Al I
$\mathbf{B}_4$	=	$\frac{1}{2}\mathbf{a}_1$	=	$\frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16c) Al I
$\mathbf{B}_5$	=	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}}$	(16d) V I
$\mathbf{B}_6$	=	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	=	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}}$	(16d) V I
$\mathbf{B}_7$	=	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16d) V I
$\mathbf{B}_8$	=	$\frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16d) V I
$\mathbf{B}_9$	=	$-(x_3 - \frac{1}{4})\mathbf{a}_1 + x_3\mathbf{a}_2 + x_3\mathbf{a}_3$	=	$ax_3\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{10}$	=	$x_3\mathbf{a}_1 - (x_3 - \frac{1}{4})\mathbf{a}_2 - (x_3 - \frac{1}{4})\mathbf{a}_3$	=	$-a(x_3 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{11}$	=	$x_3\mathbf{a}_1 - (x_3 - \frac{1}{4})\mathbf{a}_2 + x_3\mathbf{a}_3$	=	$\frac{1}{8}a\hat{\mathbf{x}} + ax_3\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{12}$	=	$-(x_3 - \frac{1}{4})\mathbf{a}_1 + x_3\mathbf{a}_2 - (x_3 - \frac{1}{4})\mathbf{a}_3$	=	$\frac{1}{8}a\hat{\mathbf{x}} - a(x_3 - \frac{1}{4})\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{13}$	=	$x_3\mathbf{a}_1 + x_3\mathbf{a}_2 - (x_3 - \frac{1}{4})\mathbf{a}_3$	=	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + ax_3\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{14}$	=	$-(x_3 - \frac{1}{4})\mathbf{a}_1 - (x_3 - \frac{1}{4})\mathbf{a}_2 + x_3\mathbf{a}_3$	=	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} - a(x_3 - \frac{1}{4})\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{15}$	=	$(x_3 + \frac{3}{4})\mathbf{a}_1 - x_3\mathbf{a}_2 + (x_3 + \frac{3}{4})\mathbf{a}_3$	=	$\frac{3}{8}a\hat{\mathbf{x}} + a(x_3 + \frac{3}{4})\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{16}$	=	$-x_3\mathbf{a}_1 + (x_3 + \frac{3}{4})\mathbf{a}_2 - x_3\mathbf{a}_3$	=	$\frac{3}{8}a\hat{\mathbf{x}} - ax_3\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{17}$	=	$-x_3\mathbf{a}_1 + (x_3 + \frac{3}{4})\mathbf{a}_2 + (x_3 + \frac{3}{4})\mathbf{a}_3$	=	$a(x_3 + \frac{3}{4})\hat{\mathbf{x}} + \frac{3}{8}a\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{18}$	=	$(x_3 + \frac{3}{4})\mathbf{a}_1 - x_3\mathbf{a}_2 - x_3\mathbf{a}_3$	=	$-ax_3\hat{\mathbf{x}} + \frac{3}{8}a\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{19}$	=	$-x_3\mathbf{a}_1 - x_3\mathbf{a}_2 + (x_3 + \frac{3}{4})\mathbf{a}_3$	=	$\frac{3}{8}a\hat{\mathbf{x}} + \frac{3}{8}a\hat{\mathbf{y}} - ax_3\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{20}$	=	$(x_3 + \frac{3}{4})\mathbf{a}_1 + (x_3 + \frac{3}{4})\mathbf{a}_2 - x_3\mathbf{a}_3$	=	$\frac{3}{8}a\hat{\mathbf{x}} + \frac{3}{8}a\hat{\mathbf{y}} + a(x_3 + \frac{3}{4})\hat{\mathbf{z}}$	(48f) Al II
$\mathbf{B}_{21}$	=	$z_4\mathbf{a}_1 + z_4\mathbf{a}_2 + (2x_4 - z_4)\mathbf{a}_3$	=	$ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + az_4\hat{\mathbf{z}}$	(96g) Al III
$\mathbf{B}_{22}$	=	$z_4\mathbf{a}_1 + z_4\mathbf{a}_2 - (2x_4 + z_4 - \frac{1}{2})\mathbf{a}_3$	=	$-a(x_4 - \frac{1}{4})\hat{\mathbf{x}} - a(x_4 - \frac{1}{4})\hat{\mathbf{y}} + az_4\hat{\mathbf{z}}$	(96g) Al III
$\mathbf{B}_{23}$	=	$(2x_4 - z_4)\mathbf{a}_1 - (2x_4 + z_4 - \frac{1}{2})\mathbf{a}_2 + z_4\mathbf{a}_3$	=	$-a(x_4 - \frac{1}{4})\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - a(z_4 - \frac{1}{4})\hat{\mathbf{z}}$	(96g) Al III

$$\begin{aligned}
\mathbf{B}_{24} &= \begin{pmatrix} -(2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_1 + \\ (2x_4 - z_4) \mathbf{a}_2 + z_4 \mathbf{a}_3 \end{pmatrix} = ax_4 \hat{\mathbf{x}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{y}} - a \left(z_4 - \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{25} &= (2x_4 - z_4) \mathbf{a}_1 + z_4 \mathbf{a}_2 + z_4 \mathbf{a}_3 = az_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{26} &= \begin{pmatrix} -(2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_1 + z_4 \mathbf{a}_2 + \\ z_4 \mathbf{a}_3 \end{pmatrix} = az_4 \hat{\mathbf{x}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{y}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{27} &= \begin{pmatrix} z_4 \mathbf{a}_1 + (2x_4 - z_4) \mathbf{a}_2 - \\ (2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a \left(z_4 - \frac{1}{4}\right) \hat{\mathbf{x}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{28} &= \begin{pmatrix} z_4 \mathbf{a}_1 - (2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_2 + \\ (2x_4 - z_4) \mathbf{a}_3 \end{pmatrix} = -a \left(z_4 - \frac{1}{4}\right) \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{29} &= z_4 \mathbf{a}_1 + (2x_4 - z_4) \mathbf{a}_2 + z_4 \mathbf{a}_3 = ax_4 \hat{\mathbf{x}} + az_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{30} &= z_4 \mathbf{a}_1 - (2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_2 + z_4 \mathbf{a}_3 = -a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{x}} + az_4 \hat{\mathbf{y}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{31} &= \begin{pmatrix} -(2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_1 + z_4 \mathbf{a}_2 + \\ (2x_4 - z_4) \mathbf{a}_3 \end{pmatrix} = ax_4 \hat{\mathbf{x}} - a \left(z_4 - \frac{1}{4}\right) \hat{\mathbf{y}} - a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{32} &= \begin{pmatrix} (2x_4 - z_4) \mathbf{a}_1 + z_4 \mathbf{a}_2 - \\ (2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{x}} - a \left(z_4 - \frac{1}{4}\right) \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{33} &= \begin{pmatrix} -z_4 \mathbf{a}_1 - z_4 \mathbf{a}_2 + \\ (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{y}} - az_4 \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{34} &= -z_4 \mathbf{a}_1 - z_4 \mathbf{a}_2 - (2x_4 - z_4) \mathbf{a}_3 = -ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - az_4 \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{35} &= \begin{pmatrix} -(2x_4 - z_4) \mathbf{a}_1 + \\ (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 - z_4 \mathbf{a}_3 \end{pmatrix} = a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + a \left(z_4 + \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{36} &= \begin{pmatrix} (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 - \\ (2x_4 - z_4) \mathbf{a}_2 - z_4 \mathbf{a}_3 \end{pmatrix} = -ax_4 \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{y}} + a \left(z_4 + \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{37} &= \begin{pmatrix} -(2x_4 - z_4) \mathbf{a}_1 - z_4 \mathbf{a}_2 + \\ (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{x}} + a \left(z_4 + \frac{1}{4}\right) \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{38} &= \begin{pmatrix} (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 - z_4 \mathbf{a}_2 - \\ (2x_4 - z_4) \mathbf{a}_3 \end{pmatrix} = -ax_4 \hat{\mathbf{x}} + a \left(z_4 + \frac{1}{4}\right) \hat{\mathbf{y}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{39} &= -z_4 \mathbf{a}_1 - (2x_4 - z_4) \mathbf{a}_2 - z_4 \mathbf{a}_3 = -ax_4 \hat{\mathbf{x}} - az_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{40} &= \begin{pmatrix} -z_4 \mathbf{a}_1 + (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 - \\ z_4 \mathbf{a}_3 \end{pmatrix} = a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{x}} - az_4 \hat{\mathbf{y}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{41} &= \begin{pmatrix} -z_4 \mathbf{a}_1 - (2x_4 - z_4) \mathbf{a}_2 + \\ (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a \left(z_4 + \frac{1}{4}\right) \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{42} &= \begin{pmatrix} -z_4 \mathbf{a}_1 + (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 - \\ (2x_4 - z_4) \mathbf{a}_3 \end{pmatrix} = a \left(z_4 + \frac{1}{4}\right) \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{43} &= (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 - z_4 \mathbf{a}_2 - z_4 \mathbf{a}_3 = -az_4 \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{y}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{z}} & (96g) & \text{Al III} \\
\mathbf{B}_{44} &= -(2x_4 - z_4) \mathbf{a}_1 - z_4 \mathbf{a}_2 - z_4 \mathbf{a}_3 = -az_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} & (96g) & \text{Al III}
\end{aligned}$$

References

- [1] P. J. Brown, *The Structure of $\alpha(V\text{-Al})$* , Acta Cryst. **10**, 133–135 (1957), doi:10.1107/S0365110X57000389.

Found in

- [1] F. Wang, Y.-L. Chiu, D. Eskin, W. Du, and P. R. Shearing, *A grain refinement mechanism of cast commercial purity aluminium by vanadium*, Mater. Charact **181**, 111468 (2021), doi:10.1016/j.matchar.2021.111468.

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