

Orthorhombic $\text{Sr}_4\text{Ru}_3\text{O}_{10}$ Structure: A10B3C4_oP68_55_2e2fgh2i_ade2f-001

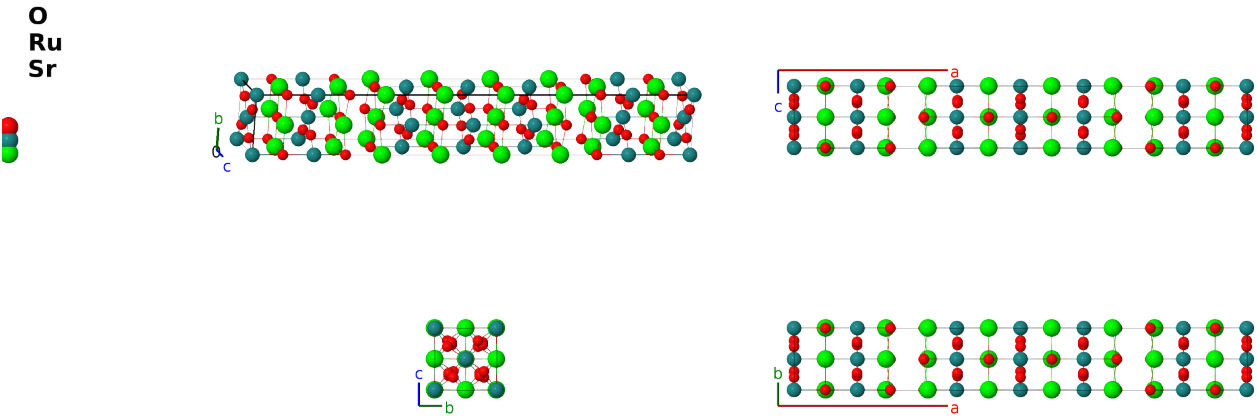
This structure previously used the label(s) **A10B3C4_oP68_55_2e2fgh2i_ade2f**. Calls to these addresses will be redirected here.

Cite this page as:

- H. Eckert, S. Divilov, M. J. Mehl, D. Hicks, A. C. Zettel, M. Esters, X. Campilongo, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*, Comput. Mater. Sci. **240**, 112988 (2024), doi: 10.1016/j.commatsci.2024.112988.
- D. Hicks, M. J. Mehl, M. Esters, C. Osos, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/PEKW>

https://aflow.org/prototype-encyclopedia/A10B3C4_oP68_55_2e2fgh2i_ade2f-001



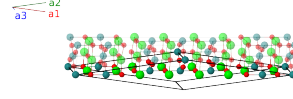
Prototype	$\text{O}_{10}\text{Ru}_3\text{Sr}_4$
AFLOW prototype label	A10B3C4_oP68_55_2e2fgh2i_ade2f-001
ICSD	96729
CCDC	1656068
Pearson symbol	oC68
Space group number	64
Space group symbol	$Cmce$
AFLOW prototype command	<code>aflow --proto=A10B3C4_oP68_55_2e2fgh2i_ade2f-001</code> <code>--params=a, b/a, c/a, x₂, x₃, x₄, x₅, x₆, y₇, z₇, x₈, y₈, z₈</code>

- This structure consists of triple-layer ruthenate structures separated by 2.37Å from each other. In the $Pbam$ #55 space group shown here there are two inequivalent stacks in the orthorhombic cell.
- This cell is very problematic. (Crawford, 2002) note that the x-ray scattering intensities are pseudo body-centered, but found that refining this structure in a body-centered cell with space group $Bbcm$ ($Cmca$ #64 in our standard orientation) led to non-positive definite thermal parameters. In that case there is only one triple-layer stack in the primitive cell, and the two stacks in the conventional orthorhombic cell are equivalent.

- If we use AFLOW with its default tolerance the structure also resolves into the smaller unit cell. The current cell can be recovered by using a smaller tolerance:
- aflow --proto=A10B3C4_oC68.64_2dfg.ad_2d:O:Ru:Sr
--params=a,b/a,c/a,x₂,z₃,z₄,z₅,z₆,z₇,z₈,z₉,z₁₀,z₁₁,z₁₂,x₁₃,y₁₃,x₁₄,y₁₄,x₁₅,y₁₅,z₁₅,x₁₆,y₁₆,z₁₆ --tolerance=0.001 .
- Note that the lattice constants in the CIF for ICSD 96729 do not agree with the lattice constants in (Crawford, 2002), although the atomic positions are the same.

Base-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	=	0	=	0	(4a) Ru I
$\mathbf{B}_2$	=	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4a) Ru I
$\mathbf{B}_3$	=	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2$	=	$ax_2 \hat{\mathbf{x}}$	(8d) O I
$\mathbf{B}_4$	=	$-\left(x_2 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_2 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-a \left(x_2 - \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) O I
$\mathbf{B}_5$	=	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2$	=	$-ax_2 \hat{\mathbf{x}}$	(8d) O I
$\mathbf{B}_6$	=	$\left(x_2 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_2 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$a \left(x_2 + \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) O I
$\mathbf{B}_7$	=	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2$	=	$ax_3 \hat{\mathbf{x}}$	(8d) O II
$\mathbf{B}_8$	=	$-\left(x_3 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_3 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-a \left(x_3 - \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) O II
$\mathbf{B}_9$	=	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2$	=	$-ax_3 \hat{\mathbf{x}}$	(8d) O II
$\mathbf{B}_{10}$	=	$\left(x_3 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_3 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$a \left(x_3 + \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) O II
$\mathbf{B}_{11}$	=	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2$	=	$ax_4 \hat{\mathbf{x}}$	(8d) Ru II
$\mathbf{B}_{12}$	=	$-\left(x_4 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_4 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-a \left(x_4 - \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) Ru II
$\mathbf{B}_{13}$	=	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2$	=	$-ax_4 \hat{\mathbf{x}}$	(8d) Ru II
$\mathbf{B}_{14}$	=	$\left(x_4 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_4 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$a \left(x_4 + \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) Ru II
$\mathbf{B}_{15}$	=	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2$	=	$ax_5 \hat{\mathbf{x}}$	(8d) Sr I
$\mathbf{B}_{16}$	=	$-\left(x_5 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_5 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-a \left(x_5 - \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) Sr I
$\mathbf{B}_{17}$	=	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2$	=	$-ax_5 \hat{\mathbf{x}}$	(8d) Sr I
$\mathbf{B}_{18}$	=	$\left(x_5 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_5 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$a \left(x_5 + \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) Sr I
$\mathbf{B}_{19}$	=	$x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2$	=	$ax_6 \hat{\mathbf{x}}$	(8d) Sr II
$\mathbf{B}_{20}$	=	$-\left(x_6 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_6 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-a \left(x_6 - \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) Sr II
$\mathbf{B}_{21}$	=	$-x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2$	=	$-ax_6 \hat{\mathbf{x}}$	(8d) Sr II
$\mathbf{B}_{22}$	=	$\left(x_6 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_6 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$a \left(x_6 + \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) Sr II
$\mathbf{B}_{23}$	=	$-y_7 \mathbf{a}_1 + y_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	=	$by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(8f) O III

$$\begin{aligned}
\mathbf{B}_{24} &= \begin{pmatrix} (y_7 + \frac{1}{2}) \mathbf{a}_1 - (y_7 - \frac{1}{2}) \mathbf{a}_2 + \\ (z_7 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = \frac{1}{2}a \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + c(z_7 + \frac{1}{2}) \hat{\mathbf{z}} & (8f) & \text{O III} \\
\mathbf{B}_{25} &= \begin{pmatrix} -(y_7 - \frac{1}{2}) \mathbf{a}_1 + (y_7 + \frac{1}{2}) \mathbf{a}_2 - \\ (z_7 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = \frac{1}{2}a \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - c(z_7 - \frac{1}{2}) \hat{\mathbf{z}} & (8f) & \text{O III} \\
\mathbf{B}_{26} &= y_7 \mathbf{a}_1 - y_7 \mathbf{a}_2 - z_7 \mathbf{a}_3 = -by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (8f) & \text{O III} \\
\mathbf{B}_{27} &= \begin{pmatrix} (x_8 - y_8) \mathbf{a}_1 + (x_8 + y_8) \mathbf{a}_2 + \\ z_8 \mathbf{a}_3 \end{pmatrix} = ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16g) & \text{O IV} \\
\mathbf{B}_{28} &= \begin{pmatrix} (-x_8 + y_8 + \frac{1}{2}) \mathbf{a}_1 - \\ (x_8 + y_8 - \frac{1}{2}) \mathbf{a}_2 + (z_8 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a(x_8 - \frac{1}{2}) \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + c(z_8 + \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{O IV} \\
\mathbf{B}_{29} &= \begin{pmatrix} -(x_8 + y_8 - \frac{1}{2}) \mathbf{a}_1 + \\ (-x_8 + y_8 + \frac{1}{2}) \mathbf{a}_2 - (z_8 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a(x_8 - \frac{1}{2}) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} - c(z_8 - \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{O IV} \\
\mathbf{B}_{30} &= \begin{pmatrix} (x_8 + y_8) \mathbf{a}_1 + (x_8 - y_8) \mathbf{a}_2 - \\ z_8 \mathbf{a}_3 \end{pmatrix} = ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16g) & \text{O IV} \\
\mathbf{B}_{31} &= \begin{pmatrix} -(x_8 - y_8) \mathbf{a}_1 - (x_8 + y_8) \mathbf{a}_2 - \\ z_8 \mathbf{a}_3 \end{pmatrix} = -ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16g) & \text{O IV} \\
\mathbf{B}_{32} &= \begin{pmatrix} (x_8 - y_8 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_8 + y_8 + \frac{1}{2}) \mathbf{a}_2 - (z_8 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a(x_8 + \frac{1}{2}) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} - c(z_8 - \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{O IV} \\
\mathbf{B}_{33} &= \begin{pmatrix} (x_8 + y_8 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_8 - y_8 + \frac{1}{2}) \mathbf{a}_2 + (z_8 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a(x_8 + \frac{1}{2}) \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + c(z_8 + \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{O IV} \\
\mathbf{B}_{34} &= \begin{pmatrix} -(x_8 + y_8) \mathbf{a}_1 - (x_8 - y_8) \mathbf{a}_2 + \\ z_8 \mathbf{a}_3 \end{pmatrix} = -ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16g) & \text{O IV}
\end{aligned}$$

References

- [1] M. K. Crawford, R. L. Harlow, W. Marshall, Z. Li, G. Cao, R. L. Lindstrom, Q. Huang, and J. W. Lynn, *Structure and magnetism of single crystal $\text{Sr}_4\text{Ru}_3\text{O}_{10}:\text{A}$ ferromagnetic triple-layer ruthenate*, Phys. Rev. B **65**, 214412 (2002), doi:10.1103/PhysRevB.65.214412.

First cited in

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